306201

PROTOCOLLO DI MISURA ZEISS UMESS

Scatola Frizione | CICLO CNC

DISEGNO No.	Indice	PROV.MAC	ZEISS	TIPO MISURA
K_TR_321___FASE1		Bz -	Cx ZEISS 1	TEST

OPERATORE	DATA	NUMERO PART.	PROGRAMMA	PALETTE	TIME
Santorsola	27. 7.2017	FULL LAYOUT			20:29:40

IND	NOMI / IDF	SY	VAL ATT	VAL NOM	TOL.S	TOL.I	DEV	MAG
	#BO_F_61_P	td	0.013	0.400				+
	#BO_PTO_D	D	9.997	9.000	0.300	0.000	0.997	0.697
	#BO_PTO_P	td	0.318	0.400				++++
	#BO_EL__D	D	11.842	12.000	0.300	-0.300	-0.158	---
	#PRE_CA11D	D	8.989	9.000	0.200	-0.200	-0.011	-
	#PRE_CA21D	D	8.997	9.000	0.200	-0.200	-0.003	-
	#PLA_P2	t	0.017	0.030				+++
	#PER__P2	t	0.068	0.100				+++
	#CON_CA1	td	0.093	0.100	0.100			++++
	#CON_CA2	td	0.077	0.100	0.100			++++
	#PER_FL_OD	t	0.027	0.100				++

OCD

PROTOCOLLO DI MISURA ZEISS UMESS

Scatola Frizione | CICLO CNC

DISEGNO No.	Indice	PROV.MAC	ZEISS	TIPO MISURA
K_TR_321___FASE1		Bz -	Cx ZEISS 1	MIS. PERIODICA

OPERATORE	DATA	NUMERO PART.	PROGRAMMA	PALETTE	TIME
Santorsola	7. 7.2017	FULL LAYOUT			12:47:31

TEMP. PEZZO 21.77

IND	NOMI / IDF	SY	VAL ATT	VAL NOM	TOL.S	TOL.I	DEV	MAG
	#GW_HP2__P	td	0.044	0.400				+
	#GW_DS1__R	R	46.032	46.000	0.150	-0.150	0.032	+
	#GW_DS1_AN X/Z	A1	161.705	162.000	0.150	-0.150	-0.295	-0.145
	#GW_DS1__P	td	0.478	0.300				0.178
	#GW_DS1__D	D	17.478	17.500	0.100	-0.100	-0.022	-
	#FL_DS1__Y	Y	3.990	4.000	0.100	-0.100	-0.010	-
	#GW_DS2__R	R	45.989	46.000	0.150	-0.150	-0.011	-
	#GW_DS2_AN X/Z	A1	53.752	54.000	0.150	-0.150	-0.248	-0.098
	#GW_DS2__P	td	0.399	0.300				0.099
	#GW_DS2__D	D	17.477	17.500	0.100	-0.100	-0.023	-
	#FL_DS2__Y	Y	3.989	4.000	0.100	-0.100	-0.011	-
	#GW_DS3__R	R	45.955	46.000	0.150	-0.150	-0.045	--
	#GW_DS3_AN X/Z	A1	305.717	-54.000	0.150	-0.150	-0.283	-0.133
	#GW_DS3__P	td	0.463	0.300				0.163
	#GW_DS3__D	D	17.478	17.500	0.100	-0.100	-0.022	-
	#FL_DS3__Y	Y	3.989	4.000	0.100	-0.100	-0.011	-
	#GW_CA11_P	td	0.351	0.400				++++
	#GW_CA12_P	td	0.389	0.400				++++
	#GW_CA13_Z	Z	122.972	123.000	0.200	-0.200	-0.028	-
	#GW_CA13_X	X	-32.686	-32.500	0.200	-0.200	-0.186	----
	#GW_CA13_P	td	0.376	0.400				++++
	#BO_CA13_Z	Z	123.005	123.000	0.050	-0.050	0.005	+
	#BO_CA13_X	X	-32.528	-32.500	0.050	-0.050	-0.028	---
	#BO_CA13_D	D	11.510	11.500	0.018	0.000	0.010	+
	#BO_CA13_P	td	0.057	0.100				+++
	#GW_CA14_P	td	0.395	0.400				++++

#BO_J_Z	Z	146.831	146.846	0.030	-0.030	-0.015	--
#BO_J_X	X	76.154	76.161	0.030	-0.030	-0.007	-
#BO_J_D	D	10.014	10.000	0.028	0.013	0.014	----
#BO_J_P	td	0.033	0.060				+++
#BO_R_Z	Z	-176.003	-176.000	0.030	-0.030	-0.003	-
#BO_R_X	X	-70.502	-70.500	0.030	-0.030	-0.002	-
#BO_R_D	D	10.014	10.000	0.028	0.013	0.014	----
#BO_R_P	td	0.007	0.060				+
#BO_J_RET	td	0.044	0.030				0.014
#BO_R_RET	td	0.003	0.030				+
#BO_D68__D	D	67.966	68.000	-0.014	-0.033	-0.034	-0.001
#BO_S_ROT	t	0.011	0.008				0.003
#P_18H7__Z	Z	104.555	104.550	0.050	-0.050	0.005	+
#P_18H7__X	X	-117.235	-117.257	0.050	-0.050	0.022	++
#P_18H7__D	D	18.006	18.000	0.018	0.000	0.006	--
#P_18H7__P	td	0.045	0.100				++
#BO_T1___Y	Y	25.954	26.000	0.200	-0.200	-0.046	-
#BO_T1___Z	Z	0.031	0.000	0.050	-0.050	0.031	+++
#BO_T1___D	D	21.044	21.050	0.100	-0.100	-0.006	-
#BO_T1___P	td	0.112	0.100				0.012
#FL_T1___X	X	-192.811	192.853	0.100	-0.100	-0.042	--
#CA1_3_CON	td	0.044	0.100				++
#CA2_3_CON	td	0.105	0.100				0.005
#ALT_Z1__Z	Z	4.390	4.000	0.800	-0.800	0.390	++
#CONO_Z1_X	X	-264.622	-264.750	0.150	-0.150	0.128	++++
#CONO_Z1_Y	Y	71.804	72.000	0.150	-0.150	-0.196	-0.046
#ANG_Z1	AC	60.028	60.000	0.100	-0.100	0.028	++
#CONO_Z1_Z	Z	145.048	144.911	0.150	-0.150	0.137	++++
#ALT_Z2__Z	Z	4.117	4.000	0.800	-0.800	0.117	+
#CONO_Z2_X	X	78.442	78.350	0.150	-0.150	0.092	+++
#CONO_Z2_Y	Y	55.592	55.500	0.150	-0.150	0.092	+++
#ANG_Z2	AC	58.050	60.000	0.100	-0.100	-1.950	-1.850
#CONO_Z2_Z	Z	170.960	171.110	0.150	-0.150	-0.150	-0.000
#ALT_Z3__Z	Z	3.994	4.000	0.800	-0.800	-0.006	-
#CONO_Z3_X	X	-122.704	-122.820	0.150	-0.150	0.116	++++
#CONO_Z3_Y	Y	92.760	92.800	0.150	-0.150	-0.040	--
#ANG_Z3	AC	60.057	60.000	0.100	-0.100	0.057	+++
#CONO_Z3_Z	Z	161.727	161.732	0.150	-0.150	-0.005	-

#Z3/Z2___X	|X |	-201.153|	201.170|	0.050|	-0.050|	-0.017|	--
#Z3/Z2___Y	|Y |	37.195|	37.300|	0.050|	-0.050|	-0.105|	-0.055
#Z3/Z2___P	|td|	0.270|	0.100|	|	|	|	0.170
#Z3/Z2___Z	|Z |	9.233|	9.378|	0.050|	-0.050|	-0.145|	-0.095
#T1_RET	|t |	0.074|	0.100|	|	|	|	+++ 82
#BO_J_RET	|td|	0.014|	0.030|	|	|	|	++ 6
#CA1_FL1_Z	|Z |	195.752|	195.800|	0.050|	-0.050|	-0.048|	---- 226
#CA1_FL2_Z	|Z |	52.903|	53.000|	0.100|	-0.100|	-0.097|	---- 227
#CA2_FL1_X	|X |	195.795|	195.800|	0.050|	-0.050|	-0.005|	- 226
#CA2_FL2_X	|X |	53.030|	53.000|	0.100|	-0.100|	0.030|	++ 227
#BO_F_61_P	|td|	0.034|	0.400|	|	|	|	+ 153
#BO_PTO__D	|D |	10.006|	9.000|	0.300|	0.000|	1.006|	0.706 285
#BO_PTO__P	|td|	0.329|	0.400|	|	|	|	++++ ?

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PROTOCOLLO STAMPATO DA NEW-GSSTAT IL 07/07/2017 15.09.07
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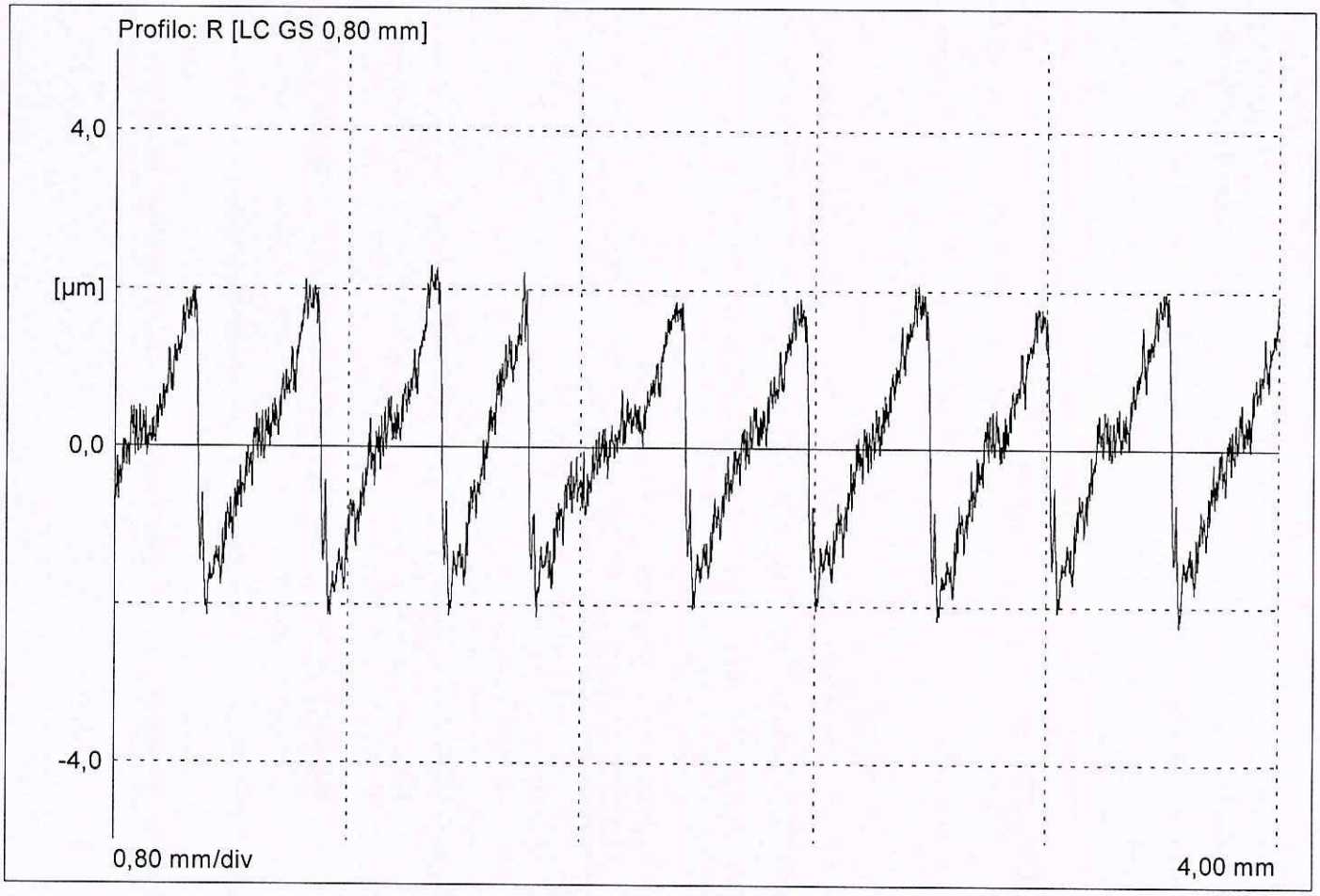
GETRAG

Via dei Ciclamini,4 Modugno (BA)

Sala Metrologica GPS5

Oggetto:	CH
Numero:	3321.10
Operatore:	TURNO A
Data, ora:	27/11/2017, 11:27
Nota:	SR5
Tastatore:	MFW-250 x 2.0 -50
MACCHINA:	MOA 416121 001



LT	5,60	mm
LM	4,00	mm
Z	5	
VB	±500,0	µm
Ra	0,9	µm
Rmax	4,4	µm
Rz	4,2	µm
R Sm	---	µm

PERTHOMETER CONCEPT

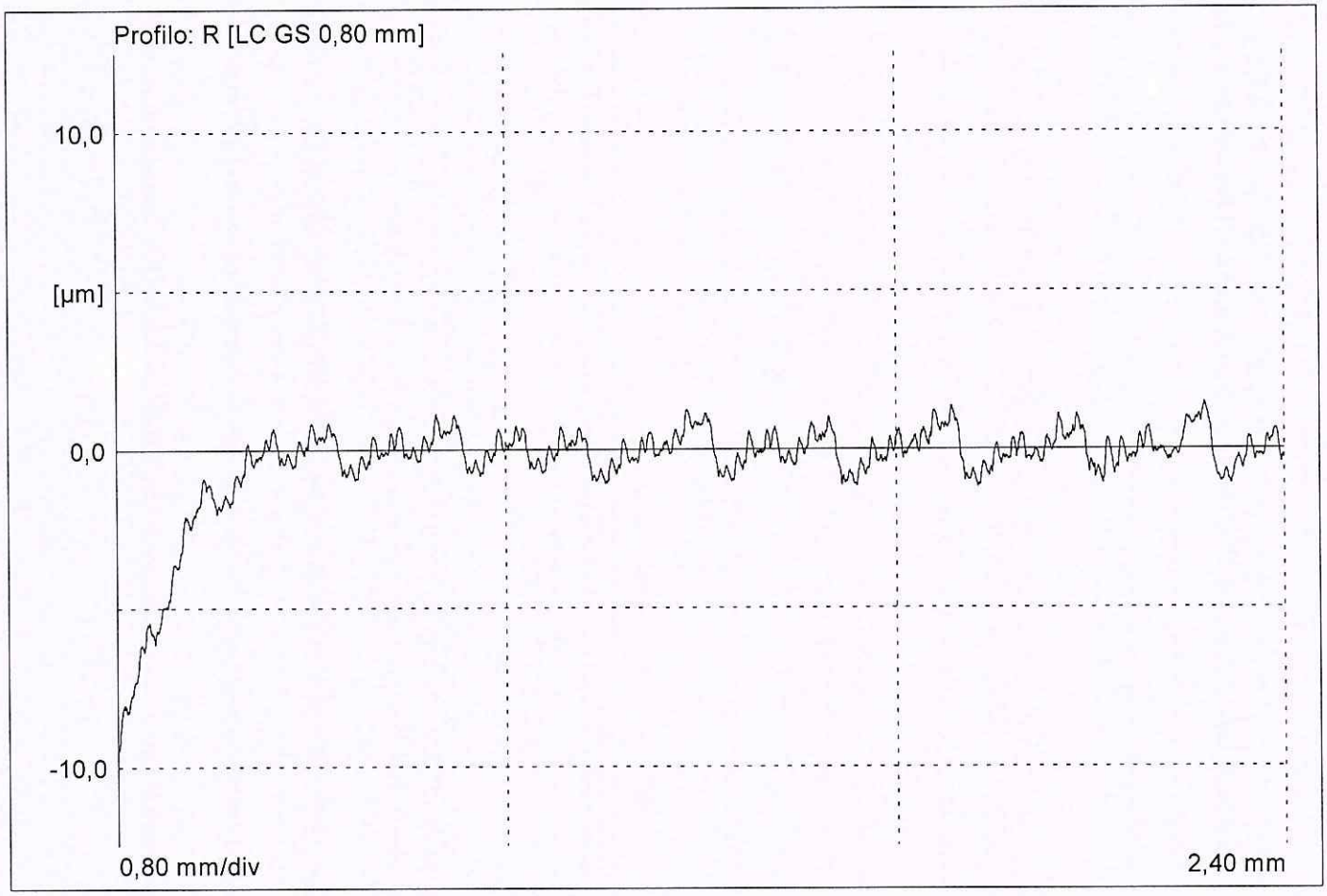
GETRAG

Via dei Ciclamini,4 Modugno (BA)

Sala Metrologica GPS5

Oggetto:	CH
Numero:	3321.10
Operatore:	TURNO A
Data, ora:	23/11/2017, 12:59
Nota:	RZ FORO DG2
Tastatore:	MFW-250 20

MACCHINA: MOA 416121 001



LT	4,00	mm
LM	2,40	mm
Z	3	
VB	±250,0	µm
Ra	0,82	µm
Rmax	10,69	µm
Rz	5,27	µm
R Sm	170,71	µm

PERTHOMETER CONCEPT

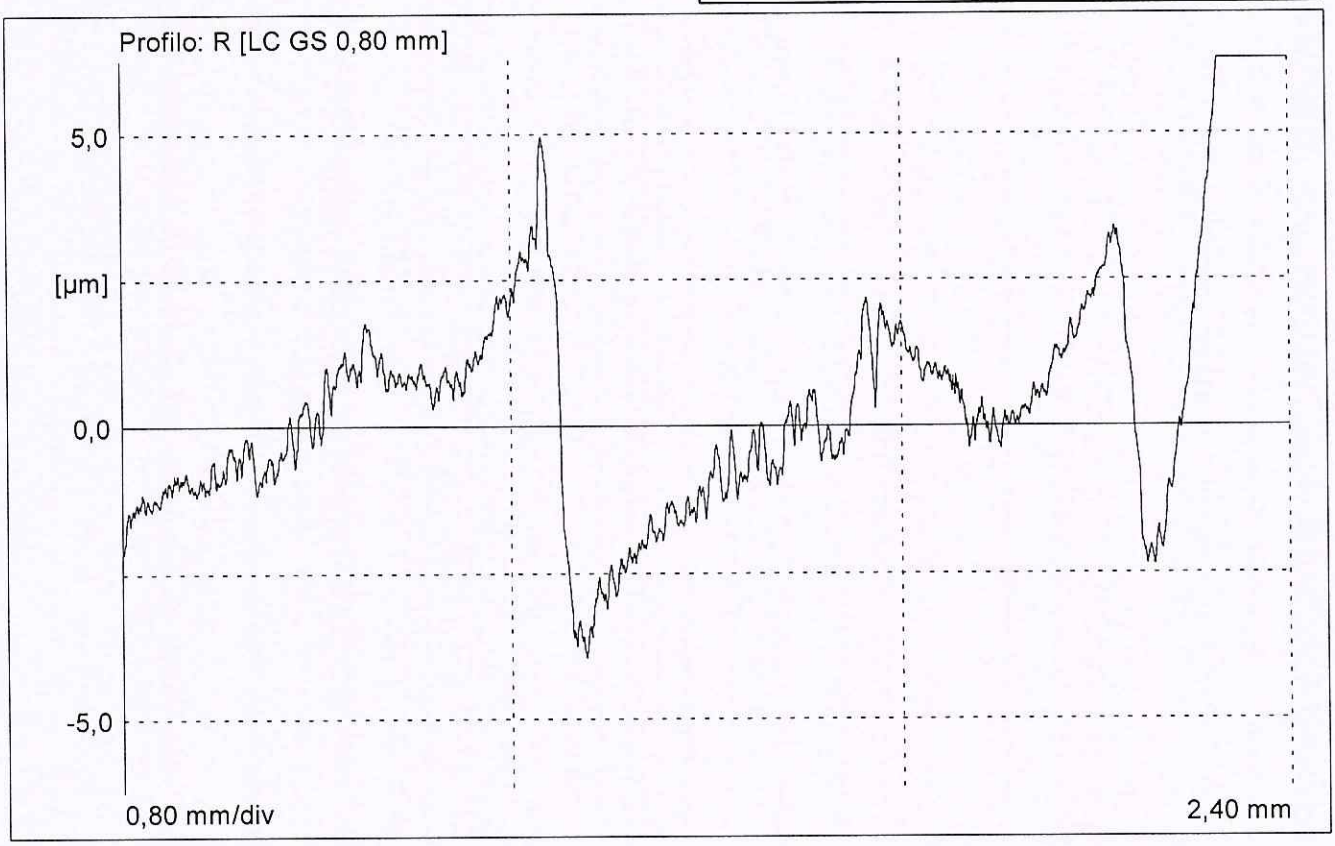
GETRAG

Via dei Ciclamini 4 Modugno Bari

Sala Metrologica GPS5

Oggetto:	CH
Numero:	3321.10
Operatore:	TURNO A
Data, ora:	23/11/2017, 13:08
Nota:	RZ FORO SR2
Tastatore:	MFW-250 20

MACCHINA: MOA 416121 001



LS	2,5	µm
LT	4,00	mm
LM	2,40	mm
Z	3	
VB	±250,0	µm
Ra	2,25	µm
Rmax	33,78	µm
Rz	15,70	µm
R Sm	870,75	µm

PERTHOMETER CONCEPT

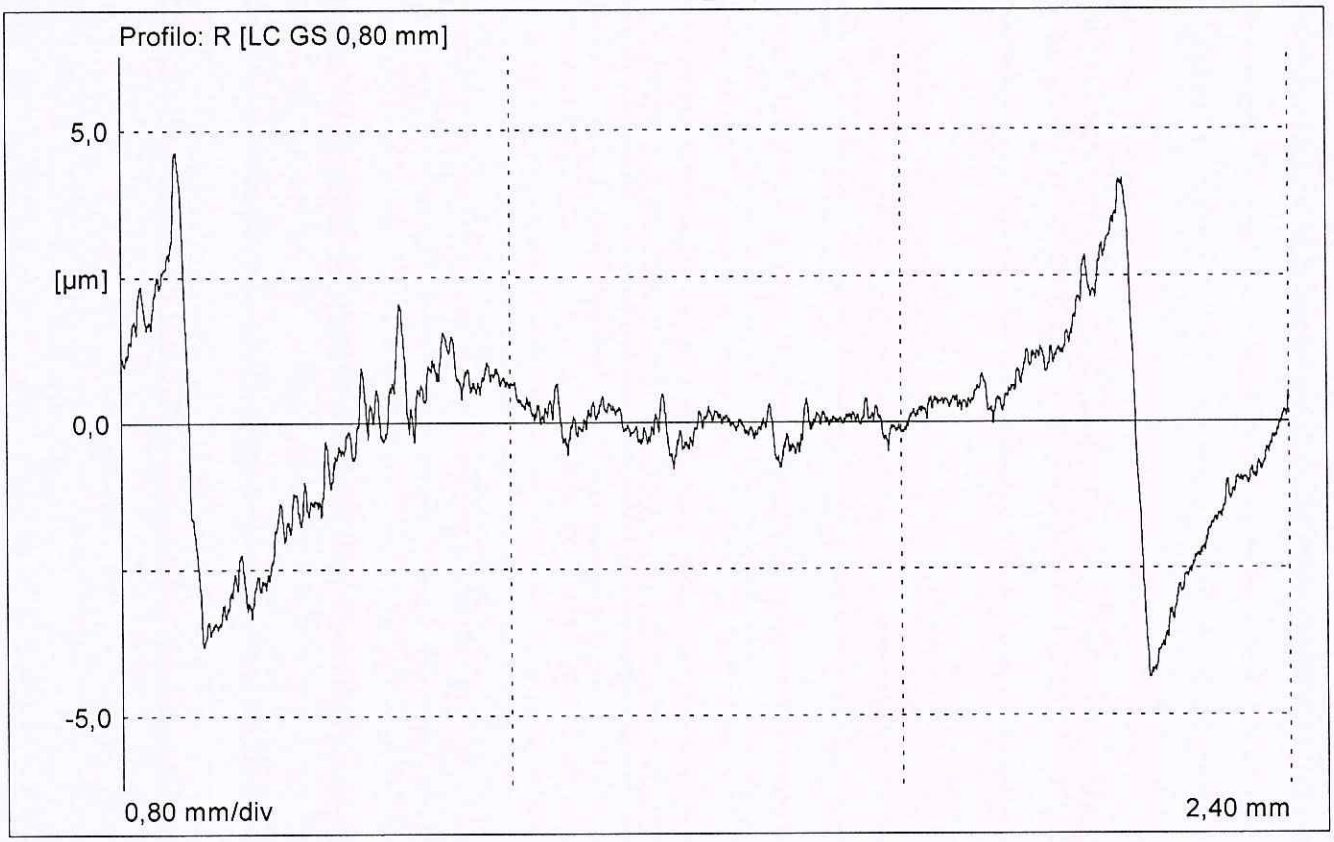
GETRAG

Via dei Ciclamini 4 Modugno Bari

Sala Metrologica GPS5

Oggetto:	CH
Numero:	3321.10
Operatore:	TURNO A
Data, ora:	23/11/2017, 13:05
Nota:	RZ FORO DG4
Tastatore:	MFW-250 20

MACCHINA: MOA 416121 001



LS	2,5	µm
LT	4,00	mm
LM	2,40	mm
Z	3	
VB	±250,0	µm
Ra	1,06	µm
Rmax	8,51	µm
Rz	6,15	µm
R Sm	1263,00	µm

PERTHOMETER CONCEPT

Misurazione
effettuata e validata da:
Badge 578

PROTOCOLLO DI MISURA ZEISS UMESS

Scatola Frizione | CICLO CNC

DISEGNO No.	Indice	PROV.MAC	ZEISS	TIPO MISURA
K_TR_321___FASE1		Bz -	Cx ZEISS 1	TEST

OPERATORE	DATA	NUMERO PART.	PROGRAMMA	PALETTE	TIME
Loconsole	13. 7.2017	FULL LAYOUT			12:13: 5

TEMP. PEZZO 22.37

IND	NOMI / IDF	SY	VAL ATT	VAL NOM	TOL.S	TOL.I	DEV	MAG	
	#FL_G_Y	Y	-179.778	179.800	0.040	-0.040	-0.022	---	1
	#FL_G_PAR	t	0.017	0.080				+	241
	#FL_H_PLAN	t	0.033	0.050				+++	2
	#H_PLA/100	t	0.027	0.030				++++	3
	#FL_E1_Y	Y	159.681	159.710	0.000	-0.060	-0.029	+	47
	#FL_E1_PAR	t	0.007	0.100				+	48
	#FL_E2_Y	Y	159.682	159.710	0.000	-0.060	-0.028	+	
	#FL_E2_PAR	t	0.006	0.100				+	
	#BO_K_Z	Z	56.567	56.574	0.050	-0.050	-0.007	-	
	#BO_K_X	X	151.306	151.310	0.050	-0.050	-0.004	-	
	#BO_K_D	D	12.883	12.887	0.014	-0.014	-0.004	--	49
	#BO_K_P	td	0.016	0.100				+	50
	#BO_K_PERP	td	0.004	0.040				+	131
	#BO_K1_D	D	11.273	11.200	0.250	-0.250	0.073	++	132
	#BO_K1_CON	td	0.477	0.500				++++	133
	#BO_M_Z	Z	-17.755	-17.751	0.050	-0.050	-0.004	-	
	#BO_M_X	X	-165.405	-165.423	0.050	-0.050	0.018	++	
	#BO_M_D	D	12.881	12.887	0.014	-0.014	-0.006	--	49
	#BO_M_P	td	0.036	0.100				++	50
	#BO_M_PERP	td	0.001	0.040				+	
	#GW_M_Z	Z	-17.625	-17.751	0.200	-0.200	0.126	+++	
	#GW_M_X	X	-165.403	-165.423	0.200	-0.200	0.020	+	
	#GW_M_P	td	0.255	0.400				+++	
	#GW_M_CON	td	0.259	0.300				++++	135
	#GW_M_PERP	td	0.025	0.300				+	136
	#ANG_K/M	A1	52.366	52.363	0.100	-0.100	0.003	+	51

#GW_G1_Z	|Z |	-133.785|	-133.776|	0.300|	-0.300|	-0.009|	-
#GW_G1_X	|X |	-99.461|	-99.500|	0.300|	-0.300|	0.039|	+
#GW_G1_P	|td|	0.079|	0.600|	|	|	|	+ 137
#GW_G1_RET	|td|	0.026|	0.200|	|	|	|	+ 138
#GR_G3_P	|td|	0.446|	0.800|	0.800|	|	|	?+++ 140
#GR_G4_P	|td|	0.529|	0.800|	1.100|	|	|	++ 140
#GR_G5_P	|td|	0.417|	0.800|	0.972|	|	|	++ 140
#GR_G7_P	|td|	0.766|	0.800|	0.910|	|	|	++++ 140
#GW_G9_Z	|Z |	-58.833|	-58.916|	0.300|	-0.300|	0.083|	++
#GW_G9_X	|X |	171.631|	171.643|	0.300|	-0.300|	-0.012|	-
#GW_G9_P	|td|	0.168|	0.600|	|	|	|	++ 141
#GW_G9_RET	|td|	0.022|	0.200|	|	|	|	+ 142
#GW_G10_Z	|Z |	-135.019|	-135.041|	0.300|	-0.300|	0.022|	+
#GW_G10_X	|X |	128.805|	128.745|	0.300|	-0.300|	0.060|	+
#GW_G10_P	|td|	0.128|	0.600|	|	|	|	+ 137
#GW_G10_RE	|td|	0.063|	0.200|	|	|	|	++ 138
#GW_G11_Z	|Z |	-186.903|	-186.964|	0.300|	-0.300|	0.061|	+
#GW_G11_X	|X |	-39.733|	-39.783|	0.300|	-0.300|	0.050|	+
#GW_G11_P	|td|	0.158|	0.600|	|	|	|	++ 137
#GW_G11_RE	|td|	0.052|	0.200|	|	|	|	++ 138
#BO_G6_Z	|Z |	160.719|	160.700|	0.050|	-0.050|	0.019|	++
#BO_G6_X	|X |	125.095|	125.100|	0.050|	-0.050|	-0.005|	-
#BO_G6_D	|D |	5.981|	5.979|	0.009|	-0.009|	0.002|	+ 52
#BO_G6_P	|td|	0.040|	0.100|	|	|	|	++ 53
#BO_G6_RET	|td|	0.012|	0.100|	|	|	|	+ 55
#BO_TR3__Z	|Z |	-136.810|	-136.854|	0.200|	-0.200|	0.044|	+
#BO_TR3__X	|X |	-207.891|	-207.975|	0.200|	-0.200|	0.084|	++
#BO_TR3__P	|td|	0.189|	0.400|	|	|	|	++ 154
#FL_TR3__Y	|Y |	4.731|	4.700|	0.100|	-0.100|	0.031|	++ 155
#BO_PT0__Z	|Z |	164.581|	164.658|	0.200|	-0.200|	-0.077|	--
#BO_PT0__X	|X |	115.208|	115.347|	0.200|	-0.200|	-0.139|	---
RIVEDERE #BO_PT0__P	|td|	0.317|	0.400|	|	|	|	++++ 156
#BO_EL___Z	|Z |	14.479|	14.428|	0.200|	-0.200|	0.051|	++
#BO_EL___X	|X |	173.156|	173.257|	0.200|	-0.200|	-0.101|	---
RIVEDERE #BO_EL___P	|td|	0.226|	0.400|	|	|	|	+++ 157
#BO_PT1__Z	|Z |	-39.138|	-39.190|	0.200|	-0.200|	0.052|	++
#BO_PT1__X	|X |	-192.112|	-192.153|	0.200|	-0.200|	0.041|	+
#BO_PT1__D	|D |	7.414|	7.430|	0.045|	-0.045|	-0.016|	-- 55

#BO_PT1__P	|td|	0.132|	0.400|	|	|	|	++ 56
#FL_PT1__Y	|Y |	-0.004|	0.000|	0.200|	-0.200|	-0.004|	-
#BO_PT2__Z	|Z |	-95.188|	-95.248|	0.200|	-0.200|	0.060|	++
#BO_PT2__X	|X |	-212.791|	-212.844|	0.200|	-0.200|	0.053|	++
#BO_PT2__D	|D |	7.408|	7.430|	0.045|	-0.045|	-0.022|	-- 55
#BO_PT2__P	|td|	0.160|	0.400|	|	|	|	++ 56
#FL_PT2__Y	|Y |	-0.001|	0.000|	0.200|	-0.200|	-0.001|	-
#GW_PT3__Z	|Z |	-50.022|	-50.004|	0.200|	-0.200|	-0.018|	-
#GW_PT3__X	|X |	-257.306|	-257.369|	0.200|	-0.200|	0.063|	++
#GW_PT3__P	|td|	0.132|	0.400|	|	|	|	++ 152
#FL_PT3__Y	|Y |	75.518|	75.500|	0.200|	-0.200|	0.018|	+ 154
#GW_HP1__Z	|Z |	-23.930|	-24.000|	0.200|	-0.200|	0.070|	++
#GW_HP1__X	|X |	-262.008|	-262.000|	0.200|	-0.200|	-0.008|	-
#GW_HP1__P	|td|	0.140|	0.400|	|	|	|	++
#FL_HP1__Y	|Y |	129.811|	129.800|	0.200|	-0.200|	0.011|	+ 324
#GW_HP2__Z	|Z |	86.561|	86.523|	0.200|	-0.200|	0.038|	+
#GW_HP2__X	|X |	-201.169|	-201.144|	0.200|	-0.200|	-0.025|	-
#GW_HP2__P	|td|	0.091|	0.400|	|	|	|	+ 57
#FL_HP2__Y	|Y |	129.816|	129.800|	0.200|	-0.200|	0.016|	+ 324
#ASOL_DIST	|Z |	10.050|	10.000|	0.100|	-0.100|	0.050|	+++
#ASOL_D__Z	|Z |	-0.003|	0.000|	0.050|	-0.050|	-0.003|	-
#ASOL_D__X	|X |	-42.495|	-42.500|	0.050|	-0.300|	0.005|	+++
#ASOL_D__D	|D |	10.016|	10.000|	0.100|	-0.100|	0.016|	+ 155
#ASOL_P(M)	|td|	0.011|	0.100|	0.216|	|	|	+ 156
#BO_D72__D	|D |	72.124|	72.100|	0.050|	-0.050|	0.024|	++ 157
#D72_CONC	|td|	0.052|	0.100|	|	|	|	+++ 158
#TR3_RET	|td|	0.047|	0.200|	|	|	|	+
#FLTR3_PAR	|t |	0.025|	0.200|	|	|	|	+
#LAM_P_64	|X |	6.529|	6.550|	0.150|	-0.150|	-0.021|	- 159
#LAM_P_11	|Z |	8.975|	9.000|	0.150|	-0.150|	-0.025|	- 160
#GW_DS1__R	|R |	45.912|	46.000|	0.150|	-0.150|	-0.088|	---
#GW_DS1_AN	X/Z|A1|	161.954|	162.000|	0.150|	-0.150|	-0.046|	--
#GW_DS1__P	|td|	0.190|	0.300|	|	|	|	+++ 161
#GW_DS1__D	|D |	17.498|	17.500|	0.100|	-0.100|	-0.002|	- 162
#CONC_17/1	|td|	0.035|	0.200|	|	|	|	+ 164
#FL_DS1__Y	|Y |	3.942|	4.000|	0.100|	-0.100|	-0.058|	---

#GW_DS2__R		R	46.072	46.000	0.150	-0.150	0.072	++
#GW_DS2_AN	X/Z	A1	53.984	54.000	0.150	-0.150	-0.016	-
#GW_DS2__P		td	0.146	0.300				++ 161
#GW_DS2__D		D	17.501	17.500	0.100	-0.100	0.001	+ 162
#CONC_17/2		td	0.074	0.200				++ 164
#FL_DS2__Y		Y	3.931	4.000	0.100	-0.100	-0.069	---
#GW_DS3__R		R	46.000	46.000	0.150	-0.150	0.000	+-
#GW_DS3_AN	X/Z	A1	306.171	-54.000	0.150	-0.150	0.171	0.021
#GW_DS3__P		td	0.274	0.300				++++ 161
#GW_DS3__D		D	17.499	17.500	0.100	-0.100	-0.001	- 162
#CONC_17/3		td	0.089	0.200				++ 164
#FL_DS3__Y		Y	3.926	4.000	0.100	-0.100	-0.074	---
#FL_D/G__Y		Y	161.410	161.400	0.000	-0.100	0.010	0.010
#GW_CA11_Z		Z	90.913	91.000	0.200	-0.200	-0.087	--
#GW_CA11_X		X	-59.998	-60.000	0.200	-0.200	0.002	+
#GW_CA11_P		td	0.174	0.400				++ 166
#FL_CA11_Y		Y	0.000	0.000	0.100	-0.100	0.000	+-
#GW_CA12_Z		Z	91.376	91.000	0.200	-0.200	0.376	0.176
#GW_CA12_X		X	59.965	60.000	0.200	-0.200	-0.035	-
#GW_CA12_P		td	0.756	0.400				0.356 166
#FL_CA12_Y		Y	-0.007	0.000	0.100	-0.100	-0.007	-
#GW_CA13_Z		Z	123.034	123.000	0.200	-0.200	0.034	+
#GW_CA13_X		X	-32.583	-32.500	0.200	-0.200	-0.083	--
#GW_CA13_P		td	0.178	0.400				++ 289
#BO_CA13_Z		Z	122.965	123.000	0.050	-0.050	-0.035	---
#BO_CA13_X		X	-32.501	-32.500	0.050	-0.050	-0.001	-
#BO_CA13_D		D	11.513	11.500	0.018	0.000	0.013	++ 60
#BO_CA13_P		td	0.070	0.100				+++ 61
#FL_CA13_Y		Y	4.086	4.100	0.200	-0.200	-0.014	-
#GW_CA14_Z		Z	123.175	123.000	0.200	-0.200	0.175	++++
#GW_CA14_X		X	32.442	32.500	0.200	-0.200	-0.058	--
#GW_CA14_P		td	0.369	0.400				++++ 166
#FL_CA14_Y		Y	-0.005	0.000	0.200	-0.200	-0.005	-
#BO_CA15_Z		Z	41.011	41.000	0.050	-0.050	0.011	+
#BO_CA15_X		X	0.008	0.000	0.050	-0.050	0.008	+
#BO_CA15_D		D	6.001	6.000	0.012	0.000	0.001	---- 63
#BO_CA15_P		td	0.028	0.100				++ 64
#CA15_RET		td	0.001	0.050				+ 65

#GW_CA21_Z	|Z |	60.077|	60.000|	0.200|	-0.200|	0.077|	++
#GW_CA21_X	|X |	92.749|	93.000|	0.200|	-0.200|	-0.251|	-0.051
#GW_CA21_P	|td|	0.526|	0.400|	|	|	|	0.126 (168)
#FL_CA21_Y	|Y |	-0.003|	0.000|	0.100|	-0.100|	-0.003|	-
#GW_CA22_Z	|Z |	-59.928|	-60.000|	0.200|	-0.200|	0.072|	++
#GW_CA22_X	|X |	93.255|	93.000|	0.200|	-0.200|	0.255|	0.055
#GW_CA22_P	|td|	0.530|	0.400|	|	|	|	0.130 (168)
#FL_CA22_Y	|Y |	-0.007|	0.000|	0.100|	-0.100|	-0.007|	-
#GW_CA23_Z	|Z |	32.662|	32.500|	0.200|	-0.200|	0.162|	++++
#GW_CA23_X	|X |	122.874|	123.000|	0.200|	-0.200|	-0.126|	---
#GW_CA23_P	|td|	0.411|	0.400|	|	|	|	0.011 (62)
#BO_CA23_Z	|Z |	32.522|	32.500|	0.050|	-0.050|	0.022|	++
#BO_CA23_X	|X |	122.998|	123.000|	0.050|	-0.050|	-0.002|	-
#BO_CA23_D	|D |	11.512|	11.500|	0.018|	0.000|	0.012|	++ (60)
#BO_CA23_P	|td|	0.045|	0.100|	|	|	|	++ (67)
#FL_CA23_Y	|Y |	4.179|	4.100|	0.200|	-0.200|	0.079|	++
#CA23_RET	|td|	0.003|	0.050|	|	|	|	+ (62)
#GW_CA24_Z	|Z |	-32.319|	-32.500|	0.200|	-0.200|	0.181|	++++
#GW_CA24_X	|X |	123.156|	123.000|	0.200|	-0.200|	0.156|	++++
#GW_CA24_P	|td|	0.478|	0.400|	|	|	|	0.078 (169)
#FL_CA24_Y	|Y |	-0.006|	0.000|	0.200|	-0.200|	-0.006|	-
#BO_CA25_Z	|Z |	0.007|	0.000|	0.050|	-0.050|	0.007|	+
#BO_CA25_X	|X |	41.029|	41.000|	0.050|	-0.050|	0.029|	+++
#BO_CA25_D	|D |	6.000|	6.000|	0.012|	0.000|	-0.000|	-0.000 (63)
#BO_CA25_P	|td|	0.059|	0.100|	|	|	|	+++ (64)
#CA25_RET	|td|	0.004|	0.050|	|	|	|	+ (65)
#BO_J_Z	|Z |	146.835|	146.846|	0.030|	-0.030|	-0.011|	--
#BO_J_X	|X |	76.165|	76.161|	0.030|	-0.030|	0.004|	+
#BO_J_D	|D |	10.015|	10.000|	0.028|	0.013|	0.015|	--- (5)
#BO_J_P	|td|	0.022|	0.060|	|	|	|	++ (5)
#BO_R_Z	|Z |	-175.988|	-176.000|	0.030|	-0.030|	0.012|	++
#BO_R_X	|X |	-70.487|	-70.500|	0.030|	-0.030|	0.013|	++
#BO_R_D	|D |	10.016|	10.000|	0.028|	0.013|	0.016|	--- (6)
#BO_R_P	|td|	0.036|	0.060|	|	|	|	+++ (5)
#BO_J_RET	|td|	0.007|	0.030|	|	|	|	+ (6)
#BO_R_RET	|td|	0.006|	0.030|	|	|	|	+ (6)
#BO_D68__D	|D |	67.970|	68.000|	-0.014|	-0.033|	-0.030|	--- (66)
#D68_RET	|td|	0.003|	0.030|	|	|	|	+ 172

#BO_D62__D	|D |	62.005|	62.000|	0.046|	0.000|	0.005|	---- 10
#D62_CONC	|td|	0.002|	0.050|	|	|	|	+ 173
#FL_D1___Y	|Y |	-8.491|	8.500|	0.030|	-0.030|	-0.009|	-- 67
#FL_D1_PAR	|t |	0.007|	0.030|	|	|	|	+ 68
#FL_D2___Y	|Y |	14.907|	14.900|	0.040|	-0.040|	0.007|	+ 16
#BO_L_Z	|Z |	-70.325|	-70.330|	0.025|	-0.025|	0.005|	+
#BO_L_X	|X |	-38.134|	-38.127|	0.025|	-0.025|	-0.007|	--
#BO_L_D	|D |	59.948|	60.000|	-0.035|	-0.054|	-0.052|	---- 7
#BO_L_P	|td|	0.017|	0.050|	|	|	|	++ 8
#BO_L_RET	|td|	0.004|	0.030|	|	|	|	+ 9
#BO_L_2__D	|D |	55.016|	55.000|	0.050|	-0.050|	0.016|	++ 175
#FL_L_Y	|Y |	-46.866|	46.800|	0.100|	-0.100|	0.066|	+++ 69
#FL_L_2_Y	|Y |	-28.332|	28.300|	0.100|	-0.100|	0.032|	++ 175
#BO_S_Z	|Z |	15.903|	15.906|	0.025|	-0.025|	-0.003|	-
#BO_S_X	|X |	-94.659|	-94.673|	0.025|	-0.025|	0.014|	+++
#BO_S_D	|D |	59.945|	60.000|	-0.035|	-0.054|	-0.055|	-0.001 7
#BO_S_P	|td|	0.029|	0.050|	|	|	|	+++ 5
#BO_S_RET	|td|	0.013|	0.030|	|	|	|	++ 9
#BO_S_2__D	|D |	55.017|	55.000|	0.050|	-0.050|	0.017|	++ 175
#FL_S_Y	|Y |	-46.861|	46.800|	0.100|	-0.100|	0.061|	+++ 69
#FL_S_2_Y	|Y |	-28.343|	28.300|	0.100|	-0.100|	0.043|	++ 175
#ANG1_S1	|A1|	15.249|	16.500|	1.000|	-1.000|	-1.251|	-0.251
#ANG2_S1	|A2|	45.074|	45.000|	0.500|	-0.500|	0.074|	+
#S1_D	|D |	6.113|	6.000|	0.300|	0.000|	0.113|	-
#S1_Z	|Z |	-5.241|	5.000|	0.100|	-0.100|	0.241|	0.141
#S1_X	|X |	-75.909|	75.000|	0.100|	-0.100|	0.909|	0.809
#BO_F_Z	|Z |	-89.596|	-89.601|	0.025|	-0.025|	0.005|	+
#BO_F_X	|X |	-165.271|	-165.274|	0.025|	-0.025|	0.003|	+
#BO_F_D	|D |	65.062|	65.000|	0.080|	0.061|	0.062|	---- 11
#BO_F_P	|td|	0.011|	0.050|	|	|	|	+ 12
#BO_F_RET	|td|	0.006|	0.030|	|	|	|	+ 13
#FL_F_Y	|Y |	-107.124|	107.120|	0.080|	-0.080|	0.004|	+ 14
#FL_F_PAR	|t |	0.020|	0.030|	|	|	|	+++ 70
#BO_F2_D	|D |	55.023|	55.000|	0.046|	0.000|	0.023|	+- 15
#BO_F2_CON	|td|	0.014|	0.050|	|	|	|	++ 71
#BO_F61_D	|D |	60.925|	61.000|	0.300|	-0.300|	-0.075|	-- 72

#FL_F61_Y	|Y |	-119.007|	119.100|	0.100|	-0.100|	-0.093|	----	17
#BO_L_ROT	|t |	0.007|	0.008|	|	|	|	++++	18
#BO_S_ROT	|t |	0.012|	0.008|	|	|	|	0.004	18
RIV #BO_D_ROT	|t |	0.006|	0.010|	|	|	|	+++	16
RIV #BO_F_ROT	|t |	0.006|	0.010|	|	|	|	+++	20
#CYL_D	|t |	0.005|	0.010|	|	|	|	++	17
#CYL_L	|t |	0.005|	0.010|	|	|	|	+++	19
#CYL_S	|t |	0.006|	0.010|	|	|	|	+++	19
#CYL_F	|t |	0.006|	0.010|	|	|	|	+++	21
#BO_F/L_PO	|R |	128.589|	128.600|	0.025|	-0.025|	-0.011|	--	22
#BO_F/S_PO	|R |	126.949|	126.950|	0.025|	-0.025|	-0.001|	-	23
#BO_D/S_PO	|R |	95.986|	96.000|	0.025|	-0.025|	-0.014|	---	24
#BO_D/L_PO	|R |	80.000|	80.000|	0.025|	-0.025|	0.000|	+-	25
#BO_D/F_PO	|R |	187.996|	188.000|	0.025|	-0.025|	-0.004|	-	26
#GW_01___Z	|Z |	-147.635|	-147.700|	0.200|	-0.200|	0.065|	++	
#GW_01___X	|X |	102.958|	103.000|	0.200|	-0.200|	-0.042|	-	
#GW_01___P	|td|	0.155|	0.400|	|	|	|	++	181
#GW_02___Z	|Z |	-113.485|	-113.500|	0.200|	-0.200|	0.015|	+	
#GW_02___X	|X |	146.274|	146.300|	0.200|	-0.200|	-0.026|	-	
#GW_02___P	|td|	0.061|	0.400|	|	|	|	+	181
#GW_03___Z	|Z |	-37.664|	-37.600|	0.200|	-0.200|	-0.064|	--	
#GW_03___X	|X |	164.087|	164.100|	0.200|	-0.200|	-0.013|	-	
#GW_03___P	|td|	0.131|	0.400|	|	|	|	++	181
#GW_04___Z	|Z |	21.475|	21.500|	0.200|	-0.200|	-0.025|	-	
#GW_04___X	|X |	169.013|	169.000|	0.200|	-0.200|	0.013|	+	
#GW_04___P	|td|	0.056|	0.400|	|	|	|	+	181
#GW_05___Z	|Z |	75.995|	76.000|	0.200|	-0.200|	-0.005|	-	
#GW_05___X	|X |	143.503|	143.500|	0.200|	-0.200|	0.003|	+	
#GW_05___P	|td|	0.011|	0.400|	|	|	|	+	181
#GW_06___Z	|Z |	128.885|	128.900|	0.200|	-0.200|	-0.015|	-	
#GW_06___X	|X |	109.784|	109.800|	0.200|	-0.200|	-0.016|	-	
#GW_06___P	|td|	0.044|	0.400|	|	|	|	+	181
#GW_07___Z	|Z |	154.178|	154.200|	0.200|	-0.200|	-0.022|	-	
#GW_07___X	|X |	60.031|	60.000|	0.200|	-0.200|	0.031|	+	
#GW_07___P	|td|	0.076|	0.400|	|	|	|	+	181
#GW_08___Z	|Z |	181.458|	181.500|	0.200|	-0.200|	-0.042|	-	

#GW_08___X	|X |	-13.077|	-13.100|	0.200|	-0.200|	0.023|	+
#GW_08___P	|td|	0.095|	0.400|	|	|	|	+ 181
#GW_09___Z	|Z |	162.497|	162.500|	0.200|	-0.200|	-0.003|	-
#GW_09___X	|X |	-67.961|	-68.000|	0.200|	-0.200|	0.039|	+
#GW_09___P	|td|	0.078|	0.400|	|	|	|	+ 183
#GW_10___Z	|Z |	138.074|	138.041|	0.200|	-0.200|	0.033|	+
#GW_10___X	|X |	-113.220|	-113.243|	0.200|	-0.200|	0.023|	+
#GW_10___P	|td|	0.081|	0.400|	|	|	|	+ 181
#GW_11___Z	|Z |	138.563|	138.526|	0.200|	-0.200|	0.037|	+
#GW_11___X	|X |	-166.151|	-166.242|	0.200|	-0.200|	0.091|	++
#GW_11___P	|td|	0.197|	0.400|	|	|	|	++ 191 ×
#GW_12___Z	|Z |	86.588|	86.523|	0.200|	-0.200|	0.065|	++
#GW_12___X	|X |	-201.086|	201.144|	0.200|	-0.200|	-0.058|	--
#GW_12___P	|td|	0.173|	0.400|	|	|	× |	++ 178
#GW_13___Z	|Z |	27.850|	27.757|	0.200|	-0.200|	0.093|	++
#GW_13___X	|X |	-231.543|	231.602|	0.200|	-0.200|	-0.059|	--
#GW_13___P	|td|	0.219|	0.400|	|	|	|	+++ 183
#GW_14___Z	|Z |	-23.936|	-24.000|	0.200|	-0.200|	0.064|	++
#GW_14___X	|X |	-261.946|	262.000|	0.200|	-0.200|	-0.054|	--
#GW_14___P	|td|	0.167|	0.400|	|	|	× |	++ 178
#GW_15___Z	|Z |	-83.524|	-83.600|	0.200|	-0.200|	0.076|	++
#GW_15___X	|X |	-281.643|	281.700|	0.200|	-0.200|	-0.057|	--
#GW_15___P	|td|	0.189|	0.400|	|	|	|	++ 181
#GW_16___Z	|Z |	-153.938|	-154.000|	0.200|	-0.200|	0.062|	++
#GW_16___X	|X |	-261.990|	262.000|	0.200|	-0.200|	-0.010|	-
#GW_16___P	|td|	0.126|	0.400|	|	|	|	++ 181
#DB_17___Z	|Z |	-196.176|	-196.200|	0.400|	-0.400|	0.024|	+
#DB_17___X	|X |	-212.265|	212.300|	0.400|	-0.400|	-0.035|	-
#DB_17___D	|D |	9.232|	9.000|	0.300|	0.000|	0.232|	+++ 185
#DB_17___P	|td|	0.085|	0.800|	|	|	|	+ 186
#DB_18___Z	|Z |	-204.770|	-204.800|	0.400|	-0.400|	0.030|	+
#DB_18___X	|X |	-147.692|	147.700|	0.400|	-0.400|	-0.008|	-
#DB_18___D	|D |	9.228|	9.000|	0.300|	0.000|	0.228|	+++ 185
#DB_18___P	|td|	0.062|	0.800|	|	|	|	+ 186
#GW_19___Z	|Z |	-179.727|	-179.800|	0.200|	-0.200|	0.073|	++
#GW_19___X	|X |	-90.553|	90.500|	0.200|	-0.200|	0.053|	++
#GW_19___P	|td|	0.180|	0.400|	|	|	|	++
#GW_20___Z	|Z |	-158.665|	-158.700|	0.200|	-0.200|	0.035|	+
#GW_20___X	|X |	-31.538|	31.500|	0.200|	-0.200|	0.038|	+
#GW_20___P	|td|	0.103|	0.400|	|	|	|	++

#GW_21___Z	|Z |	-152.541|	-152.600|	0.200|	-0.200|	0.059|	++
#GW_21___X	|X |	35.921|	36.000|	0.200|	-0.200|	-0.079|	--
#GW_21___P	|td|	0.197|	0.400|	|	|	|	++
#BO_DG1__Z	|Z |	87.727|	87.732|	0.025|	-0.025|	-0.005|	-
#BO_DG1__X	|X |	20.213|	20.223|	0.025|	-0.025|	-0.010|	--
#BO_DG1__D	|D |	10.031|	10.000|	0.040|	0.025|	0.031|	- 27
#BO_DG1__P	|td|	0.023|	0.050|	|	|	|	++ 28
#FL_DG1_1Y	|Y |	-2.671|	2.700|	0.050|	-0.050|	-0.029|	--- 187
#DG1_RET	|td|	0.005|	0.050|	|	|	|	+ 29
#BO_DG2__Z	|Z |	62.139|	62.138|	0.025|	-0.025|	0.001|	+
#BO_DG2__X	|X |	53.539|	53.523|	0.025|	-0.025|	0.016|	+++
#BO_DG2__D	|D |	8.030|	8.000|	0.040|	0.025|	0.030|	-- 30
#BO_DG2__P	|td|	0.032|	0.050|	|	|	|	++ 31
#FL_DG2_1Y	|Y |	-2.668|	2.700|	0.050|	-0.050|	-0.032|	--- 188
#DG2_RET	|td|	0.002|	0.050|	|	|	|	+ 32
#BO_DG3__Z	|Z |	4.545|	4.545|	0.025|	-0.025|	-0.000|	+-
#BO_DG3__X	|X |	83.793|	83.787|	0.025|	-0.025|	0.006|	+
#BO_DG3__D	|D |	8.028|	8.000|	0.040|	0.025|	0.028|	---
#BO_DG3__P	|td|	0.012|	0.050|	|	|	|	+
#FL_DG3_1Y	|Y |	-2.673|	2.700|	0.050|	-0.050|	-0.027|	---
#DG3_RET	|td|	0.006|	0.050|	|	|	|	+
#BO_DG4__Z	|Z |	-37.442|	-37.437|	0.025|	-0.025|	-0.005|	-
#BO_DG4__X	|X |	85.007|	84.997|	0.025|	-0.025|	0.010|	++
#BO_DG4__D	|D |	10.029|	10.000|	0.040|	0.025|	0.029|	-- 27
#BO_DG4__P	|td|	0.022|	0.050|	|	|	|	++ 28
#FL_DG4_1Y	|Y |	-2.673|	2.700|	0.050|	-0.050|	-0.027|	--- 187
#DG4_RET	|td|	0.012|	0.050|	|	|	|	+ 29
#BO_SD1__Z	|Z |	122.751|	122.758|	0.025|	-0.025|	-0.007|	--
#BO_SD1__X	|X |	-18.880|	-18.886|	0.025|	-0.025|	0.006|	+
#BO_SD1__D	|D |	15.983|	16.000|	0.000|	-0.018|	-0.017|	--- 33
#BO_SD1__P	|td|	0.019|	0.050|	|	|	|	++ 34
#FL_SD1_1Y	|Y |	19.332|	19.300|	0.050|	-0.050|	0.032|	+++ 190
#FL_SD1_2Y	|Y |	6.055|	6.100|	0.000|	-0.200|	-0.045|	+++ 191
#SD1_RET	|td|	0.002|	0.050|	|	|	|	+ 31
#BO_SD2__Z	|Z |	-89.525|	-89.538|	0.025|	-0.025|	0.013|	+++
#BO_SD2__X	|X |	91.470|	91.458|	0.025|	-0.025|	0.012|	++
#BO_SD2__D	|D |	15.983|	16.000|	0.000|	-0.018|	-0.017|	---- 33
#BO_SD2__P	|td|	0.036|	0.050|	|	|	|	+++ 34
#FL_SD2_1Y	|Y |	29.330|	29.300|	0.050|	-0.050|	0.030|	+++ 189

#SD2_RET	|td|	0.002|	0.050|	|	|	|	+ 35
#BO_SR2__Z	|Z |	-56.677|	-56.700|	0.050|	-0.050|	0.023|	++
#BO_SR2__X	|X |	42.739|	42.733|	0.050|	-0.050|	0.006|	+
#BO_SR2__D	|D |	13.007|	13.000|	0.018|	0.000|	0.007|	-- 36
#BO_SR2__P	|td|	0.047|	0.100|	|	|	|	++ 37
#FL_SR2_1Y	|Y |	0.572|	0.500|	0.500|	-0.500|	0.072|	+
#SR2_RET	|td|	0.009|	0.050|	|	|	|	+ 38
#BO_SR3__Z	|Z |	64.874|	64.857|	0.050|	-0.050|	0.017|	++
#BO_SR3__X	|X |	-28.870|	-28.887|	0.050|	-0.050|	0.017|	++
#BO_SR3__D	|D |	13.006|	13.000|	0.018|	0.000|	0.006|	-- 36
#BO_SR3__P	|td|	0.048|	0.100|	|	|	|	++ 37
#FL_SR3_1Y	|Y |	0.730|	0.500|	0.250|	-0.450|	0.230|	++++
#SR3_RET	|td|	0.003|	0.050|	|	|	|	+ 38
#BO_SR4__Z	|Z |	94.170|	94.176|	0.050|	-0.050|	-0.006|	-
#BO_SR4__X	|X |	-70.211|	-70.200|	0.050|	-0.050|	-0.011|	-
#BO_SR4__D	|D |	10.009|	10.000|	0.015|	0.000|	0.009|	+ 39
#BO_SR4__P	|td|	0.025|	0.100|	|	|	|	+ 40
#FL_SR4_1Y	|Y |	14.118|	14.000|	0.250|	-0.450|	0.118|	+++ 193
#SR4_RET	|td|	0.004|	0.050|	|	|	|	+ 41
#BO_SR5__Z	|Z |	-106.815|	-106.831|	0.050|	-0.050|	0.016|	++
#BO_SR5__X	|X |	35.315|	35.302|	0.050|	-0.050|	0.013|	++
#BO_SR5__D	|D |	10.007|	10.000|	0.015|	0.000|	0.007|	- 38
#BO_SR5__P	|td|	0.042|	0.100|	|	|	|	++ 40
#FL_SR5_1Y	|Y |	23.915|	24.000|	0.600|	-0.600|	-0.085|	- 192
#SR5_RET	|td|	0.003|	0.050|	|	|	|	+ 41
#GW_D1___Z	|Z |	-34.092|	-34.106|	0.200|	-0.200|	0.014|	+
#GW_D1___X	|X |	20.915|	20.900|	0.200|	-0.200|	0.015|	+
#GW_D1___P	|td|	0.041|	0.400|	|	|	|	+ 196
#GW_D2___Z	|Z |	-1.036|	-1.047|	0.200|	-0.200|	0.011|	+
#GW_D2___X	|X |	-39.979|	-39.986|	0.200|	-0.200|	0.007|	+
#GW_D2___P	|td|	0.026|	0.400|	|	|	|	+ 196
#GW_D3___Z	|Z |	33.362|	33.355|	0.200|	-0.200|	0.007|	+
#GW_D3___X	|X |	22.099|	22.077|	0.200|	-0.200|	0.022|	+
#GW_D3___P	|td|	0.046|	0.400|	|	|	|	+ 196
#P_18H7__Z	|Z |	104.565|	104.550|	0.050|	-0.050|	0.015|	++
#P_18H7__X	|X |	-117.243|	-117.257|	0.050|	-0.050|	0.014|	++
#P_18H7__D	|D |	18.007|	18.000|	0.018|	0.000|	0.007|	- 42
#P_18H7__P	|td|	0.040|	0.100|	|	|	|	++ 43
#FL18H7__Y	|Y |	-49.531|	49.560|	0.050|	-0.050|	-0.029|	--- 74

#P_18H9__Z	|Z |	104.554|	104.550|	0.100|	-0.100|	0.004|	+
#P_18H9__X	|X |	-117.257|	-117.257|	0.100|	-0.100|	-0.000|	+-
#P_18H9__D	|D |	18.014|	18.000|	0.043|	0.000|	0.014|	-- 75
#P_18H9__P	|td|	0.008|	0.200|	|	|	|	+ 76
#BO_P1___Z	|Z |	41.028|	41.011|	0.050|	-0.050|	0.017|	++
#BO_P1___X	|X |	-196.956|	-196.986|	0.050|	-0.050|	0.030|	+++
#BO_P1___D	|D |	12.036|	12.000|	0.050|	0.032|	0.036|	--- 196
#BO_P1___P	|td|	0.070|	0.100|	|	|	|	+++ 197
#FL_P1___Y	|Y |	9.370|	9.340|	0.050|	-0.050|	0.030|	+++ 198
#P_21R7__D	|D |	20.963|	21.000|	-0.020|	-0.041|	-0.037|	--- 199
#21R7_CONC	|td|	0.007|	0.100|	|	|	|	+ 200
#BO_P2___Y	|Y |	-30.187|	-30.210|	0.100|	-0.100|	0.023|	+
#BO_P2___Z	|Z |	0.033|	0.000|	0.100|	-0.100|	0.033|	++
#BO_P2___D	|D |	19.980|	20.000|	-0.007|	-0.028|	-0.020|	- 47
#BO_P2___P	|td|	0.080|	0.200|	|	|	|	++ 48
#GW_P2___Y	|Y |	-30.196|	-30.210|	0.200|	-0.200|	0.014|	+
#GW_P2___Z	|Z |	-0.114|	0.000|	0.200|	-0.200|	-0.114|	---
#GW_P2___P	|td|	0.231|	0.400|	|	|	|	+++ 201
#FL_P2___X	|X |	-93.593|	93.600|	0.100|	-0.100|	-0.007|	- 29
#BO_T1___Y	|Y |	25.997|	26.000|	0.200|	-0.200|	-0.003|	-
#BO_T1___Z	|Z |	-0.001|	0.000|	0.050|	-0.050|	-0.001|	-
#BO_T1___D	|D |	21.070|	21.050|	0.100|	-0.100|	0.020|	+ 44
#BO_T1___P	|td|	0.006|	0.100|	|	|	|	+ 45
#FL_T1___X	|X |	-192.798|	192.853|	0.100|	-0.100|	-0.055|	--- 80
#GW_T3___Y	|Y |	0.022|	0.000|	0.200|	-0.200|	0.022|	+
#GW_T3___Z	|Z |	-18.970|	-19.000|	0.200|	-0.200|	0.030|	+
#GW_T3___P	|td|	0.074|	0.400|	|	|	|	+ 203
#GW_T3_RET	|td|	0.148|	0.300|	|	|	|	++ 204
#T1_PLAN	|t |	0.010|	0.300|	|	|	|	+ 81
#GW_W1___X	|X |	-90.992|	-91.053|	0.200|	-0.200|	0.061|	++
#GW_W1___Y	|Y |	77.997|	78.000|	0.200|	-0.200|	-0.003|	-
#GW_W1___P	|td|	0.122|	0.400|	|	|	|	++ 206
#FL_W1___Z	|Z |	153.201|	153.224|	0.200|	-0.200|	-0.023|	- 208
#GW_W2___X	|X |	7.980|	7.921|	0.200|	-0.200|	0.059|	++
#GW_W2___Y	|Y |	74.589|	74.580|	0.200|	-0.200|	0.009|	+
#GW_W2___P	|td|	0.120|	0.400|	|	|	|	++ 209
#FL_W2___Z	|Z |	172.619|	172.719|	0.200|	-0.200|	-0.100|	--- 210
#GW_W6___X	|X |	-72.923|	-73.000|	0.200|	-0.200|	0.077|	++
#GW_W6___Y	|Y |	156.791|	156.800|	0.200|	-0.200|	-0.009|	-

#GW_W6___P	|td|	0.155|	0.400|	|	|	|	++ 212
#FL_W6___Z	|Z |	173.109|	173.000|	0.200|	-0.200|	0.109|	+++ 213
#GW_W3___X	|X |	120.048|	119.994|	0.200|	-0.200|	0.054|	++
#GW_W3___Y	|Y |	114.737|	114.780|	0.200|	-0.200|	-0.043|	-
#GW_W3___P	|td|	0.139|	0.400|	|	|	|	++ 215
#FL_W3___Z	|Z |	126.799|	126.998|	0.650|	-0.650|	-0.199|	-- 216
#BO_V____X	|X |	-54.938|	-55.000|	0.150|	-0.150|	0.062|	++
#BO_V____Y	|Y |	138.282|	138.300|	0.150|	-0.150|	-0.018|	-
#BO_V____D	|D |	5.995|	5.995|	0.033|	-0.033|	0.000|	+- 83
#BO_V____P	|td|	0.125|	0.300|	|	|	|	++ 84
#BO_PS1__X	|X |	34.961|	35.000|	0.050|	-0.050|	-0.039|	----
#BO_PS1__Y	|Y |	-41.457|	-41.460|	0.050|	-0.050|	0.003|	+
#BO_PS1__D	|D |	9.504|	9.500|	0.050|	-0.050|	0.004|	+ 85
#BO_PS1__P	|td|	0.079|	0.100|	|	|	|	++++ 86
#BO_PS2__X	|X |	-35.030|	-35.000|	0.050|	-0.050|	-0.030|	---
#BO_PS2__Y	|Y |	-41.448|	-41.460|	0.050|	-0.050|	0.012|	+
#BO_PS2__D	|D |	9.499|	9.500|	0.050|	-0.050|	-0.001|	- 85
#BO_PS2__P	|td|	0.064|	0.100|	|	|	|	+++ 86
#GW_PS1__X	|X |	34.943|	35.000|	0.200|	-0.200|	-0.057|	--
#GW_PS1__Y	|Y |	-41.443|	-41.460|	0.200|	-0.200|	0.017|	+
#GW_PS1__P	|td|	0.119|	0.400|	|	|	|	++ 218
#GW_PS2__X	|X |	-35.056|	-35.000|	0.200|	-0.200|	-0.056|	--
#GW_PS2__Y	|Y |	-41.435|	-41.460|	0.200|	-0.200|	0.025|	+
#GW_PS2__P	|td|	0.122|	0.400|	|	|	|	++ 218
#FL_PS1__Z	|Z |	39.427|	39.500|	0.100|	-0.100|	-0.073|	--- 220
#FL_PS2__Z	|Z |	39.495|	39.500|	0.100|	-0.100|	-0.005|	- 220
#FL_PS_PLA	|t |	0.004|	0.030|	|	|	|	+ 87
#FL_PS_INC	|tx|	0.221|	0.200|	|	|	|	0.021 88
#FL_PS_PAR	|t |	0.035|	0.100|	|	|	|	++ 89
#BO_CA1__X	|X |	-0.011|	0.000|	0.130|	-0.130|	-0.011|	-
#BO_CA1__Y	|Y |	-11.477|	-11.500|	0.130|	-0.130|	0.023|	+
#BO_CA1__D	|D |	24.124|	24.100|	0.050|	0.000|	0.024|	- 90
#BO_CA1__P	|td|	0.051|	0.260|	|	|	|	+ 91
#CA1_ROT	|t |	0.006|	0.015|	|	|	|	++ 92
#BO_CA1_2D	|D |	50.893|	50.900|	0.050|	-0.050|	-0.007|	- 93
#BO_CA1_3D	|D |	56.998|	57.000|	0.050|	-0.050|	-0.002|	- 94
#CA1_3_CON	|td|	0.089|	0.100|	|	|	|	++++ 95
#BO_CA16_X	|X |	23.288|	23.405|	0.100|	-0.100|	-0.117|	-0.017 ~~222~~

#BO_CA16_Y	|Y |	23.412|	23.405|	0.100|	-0.100|	0.007|	+
#BO_CA16_D	|D |	5.498|	5.500|	0.100|	-0.100|	-0.002|	- 221
#BO_CA16_P	|td|	0.235|	0.200|	|	|	|	0.035 222
#CA16_RET	|td|	0.032|	0.150|	|	|	|	+ 223
#BO_CA17_X	|X |	23.256|	23.405|	0.100|	-0.100|	-0.149|	-0.049
#BO_CA17_Y	|Y |	-23.409|	-23.405|	0.100|	-0.100|	-0.004|	-
#BO_CA17_D	|D |	5.498|	5.500|	0.100|	-0.100|	-0.002|	- 221
#BO_CA17_P	|td|	0.298|	0.200|	|	|	|	0.098 222
#CA17_RET	|td|	0.025|	0.150|	|	|	|	+ 223
#BO_CA18_X	|X |	-23.530|	-23.405|	0.100|	-0.100|	-0.125|	-0.025
#BO_CA18_Y	|Y |	-23.399|	-23.405|	0.100|	-0.100|	0.006|	+
#BO_CA18_D	|D |	5.498|	5.500|	0.100|	-0.100|	-0.002|	- 221
#BO_CA18_P	|td|	0.251|	0.200|	|	|	|	0.051 222
#CA18_RET	|td|	0.018|	0.150|	|	|	|	+ 223
#BO_CA19_X	|X |	-23.514|	-23.405|	0.100|	-0.100|	-0.109|	-0.009
#BO_CA19_Y	|Y |	23.389|	23.405|	0.100|	-0.100|	-0.016|	-
#BO_CA19_D	|D |	5.499|	5.500|	0.100|	-0.100|	-0.001|	- 221
#BO_CA19_P	|td|	0.220|	0.200|	|	|	|	0.020
#CA19_RET	|td|	0.021|	0.150|	|	|	|	+
#GW_CA16_X	|X |	23.330|	23.405|	0.200|	-0.200|	-0.075|	--
#GW_CA16_Y	|Y |	23.430|	23.405|	0.200|	-0.200|	0.025|	+
#GW_CA16_P	|td|	0.159|	0.400|	|	|	|	++ 225
#GW_CA17_X	|X |	23.292|	23.405|	0.200|	-0.200|	-0.113|	---
#GW_CA17_Y	|Y |	-23.410|	-23.405|	0.200|	-0.200|	-0.005|	-
#GW_CA17_P	|td|	0.227|	0.400|	|	|	|	+++ 225
#GW_CA18_X	|X |	-23.499|	-23.405|	0.200|	-0.200|	-0.094|	--
#GW_CA18_Y	|Y |	-23.393|	-23.405|	0.200|	-0.200|	0.012|	+
#GW_CA18_P	|td|	0.190|	0.400|	|	|	|	++ 225
#GW_CA19_X	|X |	-23.482|	-23.405|	0.200|	-0.200|	-0.077|	--
#GW_CA19_Y	|Y |	23.401|	23.405|	0.200|	-0.200|	-0.004|	-
#GW_CA19_P	|td|	0.155|	0.400|	|	|	|	++ 225
#FL_CA1_1Z	|Z |	195.768|	195.800|	0.050|	-0.050|	-0.032|	--- 226
#FL_CA1_2Z	|Z |	53.087|	53.000|	0.100|	-0.100|	0.087|	++++ 227
#FL_CA1PLA	|t |	0.002|	0.050|	|	|	|	+ 228
#FL_CA1RET	|t |	0.106|	0.100|	|	|	|	0.006 229
#GW_W4___Y	|Y |	148.248|	148.350|	0.200|	-0.200|	-0.102|	---
#GW_W4___Z	|Z |	75.696|	75.748|	0.200|	-0.200|	-0.052|	--
#GW_W4___P	|td|	0.228|	0.400|	|	|	|	+++ 230
#FL_W4___X	|X |	160.411|	160.230|	0.400|	-0.400|	0.181|	++ 231

#BO_CA2__Y	|Y |	-11.510	-11.500	0.130	-0.130	-0.010	-
#BO_CA2__Z	|Z |	0.060	0.000	0.130	-0.130	0.060	++
#BO_CA2__D	|D |	24.123	24.100	0.050	0.000	0.023	-
#BO_CA2__P	|td|	0.121	0.260				++
#CA2_ROT	|t |	0.010	0.015				+++
#BO_CA2_2D	|D |	50.893	50.900	0.050	-0.050	-0.007	-
#BO_CA2_3D	|D |	56.997	57.000	0.050	-0.050	-0.003	-
#CA2_3_CON	|td|	0.098	0.100				++++ 95
#BO_CA26_Y	|Y |	23.390	23.405	0.100	-0.100	-0.015	-
#BO_CA26_Z	|Z |	23.484	23.405	0.100	-0.100	0.079	++++
#BO_CA26_D	|D |	5.503	5.500	0.100	-0.100	0.003	+ 221
#BO_CA26_P	|td|	0.161	0.200				++++
#CA26_RET	|td|	0.019	0.150				+
#BO_CA27_Y	|Y |	-23.399	-23.405	0.100	-0.100	0.006	+
#BO_CA27_Z	|Z |	23.496	23.405	0.100	-0.100	0.091	++++
#BO_CA27_D	|D |	5.503	5.500	0.100	-0.100	0.003	+ 221
#BO_CA27_P	|td|	0.183	0.200				++++
#CA27_RET	|td|	0.010	0.150				+
#BO_CA28_Y	|Y |	-23.395	-23.405	0.100	-0.100	0.010	+
#BO_CA28_Z	|Z |	-23.302	-23.405	0.100	-0.100	0.103	0.003
#BO_CA28_D	|D |	5.504	5.500	0.100	-0.100	0.004	+ 221
#BO_CA28_P	|td|	0.207	0.200				0.007
#CA28_RET	|td|	0.018	0.150				+
#BO_CA29_Y	|Y |	23.392	23.405	0.100	-0.100	-0.013	-
#BO_CA29_Z	|Z |	-23.291	-23.405	0.100	-0.100	0.114	0.014
#BO_CA29_D	|D |	5.504	5.500	0.100	-0.100	0.004	+ 221
#BO_CA29_P	|td|	0.229	0.200				0.029
#CA29_RET	|td|	0.015	0.150				+
#GW_CA26_Y	|Y |	23.407	23.405	0.200	-0.200	0.002	+
#GW_CA26_Z	|Z |	23.471	23.405	0.200	-0.200	0.066	++
#GW_CA26_P	|td|	0.132	0.400				++
#GW_CA27_Y	|Y |	-23.395	-23.405	0.200	-0.200	0.010	+
#GW_CA27_Z	|Z |	23.496	23.405	0.200	-0.200	0.091	++
#GW_CA27_P	|td|	0.183	0.400				++
#GW_CA28_Y	|Y |	-23.403	-23.405	0.200	-0.200	0.002	+
#GW_CA28_Z	|Z |	-23.306	-23.405	0.200	-0.200	0.099	++
#GW_CA28_P	|td|	0.197	0.400				++
#GW_CA29_Y	|Y |	23.394	23.405	0.200	-0.200	-0.011	-
#GW_CA29_Z	|Z |	-23.315	-23.405	0.200	-0.200	0.090	++

#GW_CA29_P	|td|	0.181|	0.400|	|	|	|	++
#FL_CA2_1X	|X |	195.762|	195.800|	0.050|	-0.050|	-0.038|	---- 226
#FL_CA2_2X	|X |	53.002|	53.000|	0.100|	-0.100|	0.002|	+ 227
#FL_CA2PLA	|t |	0.001|	0.050|	|	|	|	+ 228
#FL_CA2RET	|t |	0.027|	0.100|	|	|	|	++ 229
#GW_TR1__X	|X |	-247.768|	-247.709|	0.200|	-0.200|	-0.059|	--
#GW_TR1__Y	|Y |	16.380|	16.400|	0.200|	-0.200|	-0.020|	-
#GW_TR1__P	|td|	0.125|	0.400|	|	|	|	++
#FL_TR1__Z	|Z |	-143.008|	143.020|	0.100|	-0.100|	-0.012|	- 231
#GW_TR2__X	|X |	-147.785|	-147.705|	0.200|	-0.200|	-0.080|	--
#GW_TR2__Y	|Y |	16.410|	16.400|	0.200|	-0.200|	0.010|	+
#GW_TR2__P	|td|	0.161|	0.400|	|	|	|	++
#FL_TR2__Z	|Z |	-154.233|	154.270|	0.100|	-0.100|	-0.037|	-- 232
#ALT_Z1__Z	|Z |	4.118|	4.000|	0.800|	-0.800|	0.118|	+ 128
#CONO_Z1_X	|X |	-264.790|	-264.750|	0.150|	-0.150|	-0.040|	--
#CONO_Z1_Y	|Y |	71.958|	72.000|	0.150|	-0.150|	-0.042|	--
#ANG_Z1	|AC|	59.959|	60.000|	0.100|	-0.100|	-0.041|	-- 125
#CONO_Z1_Z	|Z |	145.059|	144.911|	0.150|	-0.150|	0.148|	++++ 122
#ALT_Z2__Z	|Z |	4.064|	4.000|	0.800|	-0.800|	0.064|	+ 129
#CONO_Z2_X	|X |	78.232|	78.350|	0.150|	-0.150|	-0.118|	----
#CONO_Z2_Y	|Y |	55.435|	55.500|	0.150|	-0.150|	-0.065|	--
#ANG_Z2	|AC|	59.197|	60.000|	0.100|	-0.100|	-0.803|	-0.703 126
#CONO_Z2_Z	|Z |	170.981|	171.110|	0.150|	-0.150|	-0.129|	---- 123
#ALT_Z3__Z	|Z |	4.059|	4.000|	0.800|	-0.800|	0.059|	+ 130
#CONO_Z3_X	|X |	-122.783|	-122.820|	0.150|	-0.150|	0.037|	+
#CONO_Z3_Y	|Y |	92.763|	92.800|	0.150|	-0.150|	-0.037|	-
#ANG_Z3	|AC|	59.998|	60.000|	0.100|	-0.100|	-0.002|	- 127
#CONO_Z3_Z	|Z |	161.604|	161.732|	0.150|	-0.150|	-0.128|	---- 124
#Z3/Z2___X	|X |	-201.021|	201.170|	0.050|	-0.050|	-0.149|	-0.099
#Z3/Z2___Y	|Y |	37.333|	37.300|	0.050|	-0.050|	0.033|	+++
#Z3/Z2___P	|td|	0.370|	0.100|	|	|	|	0.270
#Z3/Z2___Z	|Z |	9.377|	9.378|	0.050|	-0.050|	-0.001|	-
#GW_U_M18X	|X |	-176.224|	-176.187|	0.200|	-0.200|	-0.037|	-
#GW_U_M18Y	|Y |	-23.003|	-23.000|	0.200|	-0.200|	-0.003|	-
#GW_U_M18P	|td|	0.075|	0.400|	|	|	|	+ 233
#FL_U_M18Z	|Z |	-121.350|	121.364|	0.200|	-0.200|	-0.014|	- 234

236

#FL_U_PLAN	|t |	0.006|	0.030|	|	|	|	+
#TR1_RET	|td|	0.066|	0.200|	|	|	|	++
#TR2_RET	|td|	0.037|	0.200|	|	|	|	+
#BO_J/A2_Z	|Z |	146.715|	146.846|	0.150|	-0.150|	-0.131|	----
#BO_J/A2_X	|X |	75.909|	76.161|	0.150|	-0.150|	-0.252|	-0.102
#BO_J/A2_P	|td|	0.568|	0.300|	|	|	|	0.268
#BO_R/A2_Z	|Z |	-176.178|	-176.000|	0.150|	-0.150|	-0.178|	-0.028
#BO_R/A2_X	|X |	-70.586|	-70.500|	0.150|	-0.150|	-0.086|	---
#BO_R/A2_P	|td|	0.395|	0.300|	|	|	|	0.095
#BO_D/GR_Z	|Z |	-0.154|	0.000|	0.150|	-0.150|	-0.154|	-0.004
#BO_D/GR_X	|X |	-0.190|	0.000|	0.150|	-0.150|	-0.190|	-0.040
#BO_D/GR_P	|td|	0.488|	0.300|	|	|	|	0.188
#SIMM_H	|ty|	0.267|	0.600|	|	|	|	++
#PAR_H/CP	|t |	0.123|	0.300|	|	|	|	++

****
PROTOCOLLO STAMPATO DA NEW-GSSTAT IL 13/07/2017 13.29.39
****

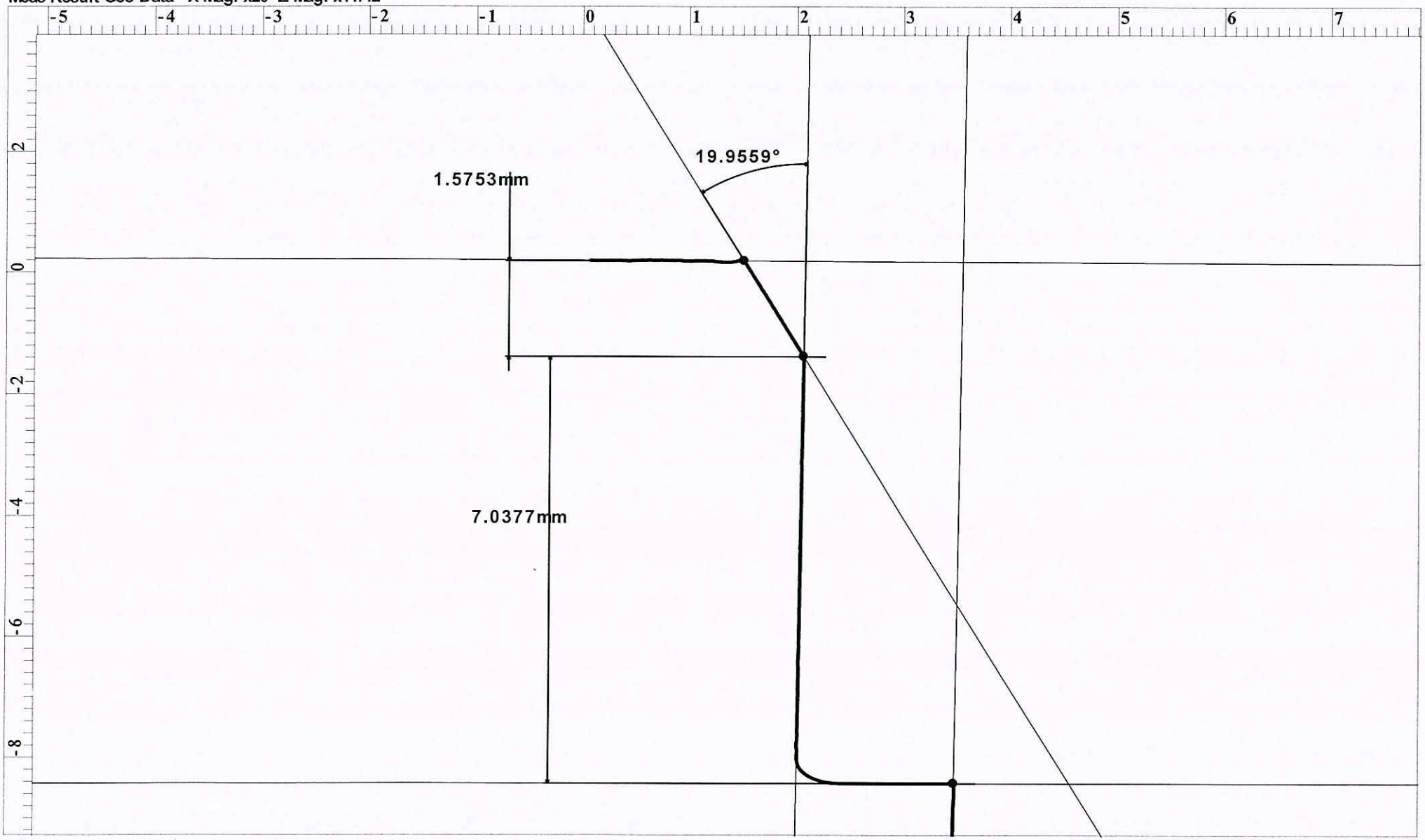
n° riga control plan	330/540	2884/3044	2594	2894/3064	2904/3074	3564
Elenco delle caratteristiche da controllare	Profondità "J"/ "R" (15+/-0.1)	Profondità fori S/L Ø35 da H (misurare su pista 51 -0.2)	Distanza fl. H fl. grezze CP1-CP2-CP3 (2+/-0.25)	Profondità fori S/L Ø55 da H (misurare su pista 49+/ -0.2)	Profondità foro S/L Ø51.3 da H (51.3+/- 0.25)	Profondità foro SD1 da fl. H (16.1 -0.2)
3624/3744/3684/3804	3694/3814	3954	4014/4134	4074	3334	4824
Altezza flangia DG1/DG4 - H Altezza flangia DG2/DG3 - H (2.7 +/-0.05)	Profondità fori DG2/DG3 fl.H (10.65+0.2)	Profondità foro SR_4 da fl.H (2.8+0.2)	Profondità fori SR_2/SR_3 da fl. H (11.3+0.2)	Profondità foro SR_5 da H (7.2-0.2)	Distanze: HP1 - G HP2 - G (129.8 +/- 0.2)	Profondità PT2 (22.8 +/- 0.2)
4644	4724	4474	2634	2736	2744/2746	4384
CA13 - CA23 altezza precamera (4.1 +/-0.2)	Profondità di nocciolo CA15_CA25 (10+/-0.2)	Profondità asola foro "D" (161.61+/-0.1)	Rugosità Flangia H (in 4 punti opposti sulla flangia) RZ-8-16 /Rmax 25, presenza di incrocio	Presenza gola di scarico F su Ø65 (accertarsi solo della presenza della stessa)	Rugosità F(55H8) Rz (10-16) Rmax(25)	Profondità foro G6 (8+/-0.2)

3484	3634/3754
Profondità foro SD2 da fl. H (6.1 -0.2) 181 6.06	266 Profondità fori DG1/DG4 fl. H (12.05+0.2) 17.06 / 17,06
4194	2237/2314
Profondità foro P1 (20.5+/-0.25) 272 20,38	275 K A3.31 Profondità fori K-M (ø12.887) (13.32+/-0.3) in 13,77
2514	4244
Rugosità D(62H8) Rz (10-16) Rmax(25)	Altezza foro P da Fl 18H7 a battuta 21R7 (9.5 +/- 0.1) 277 9,60

FORO P

28/11/17 11:37:02

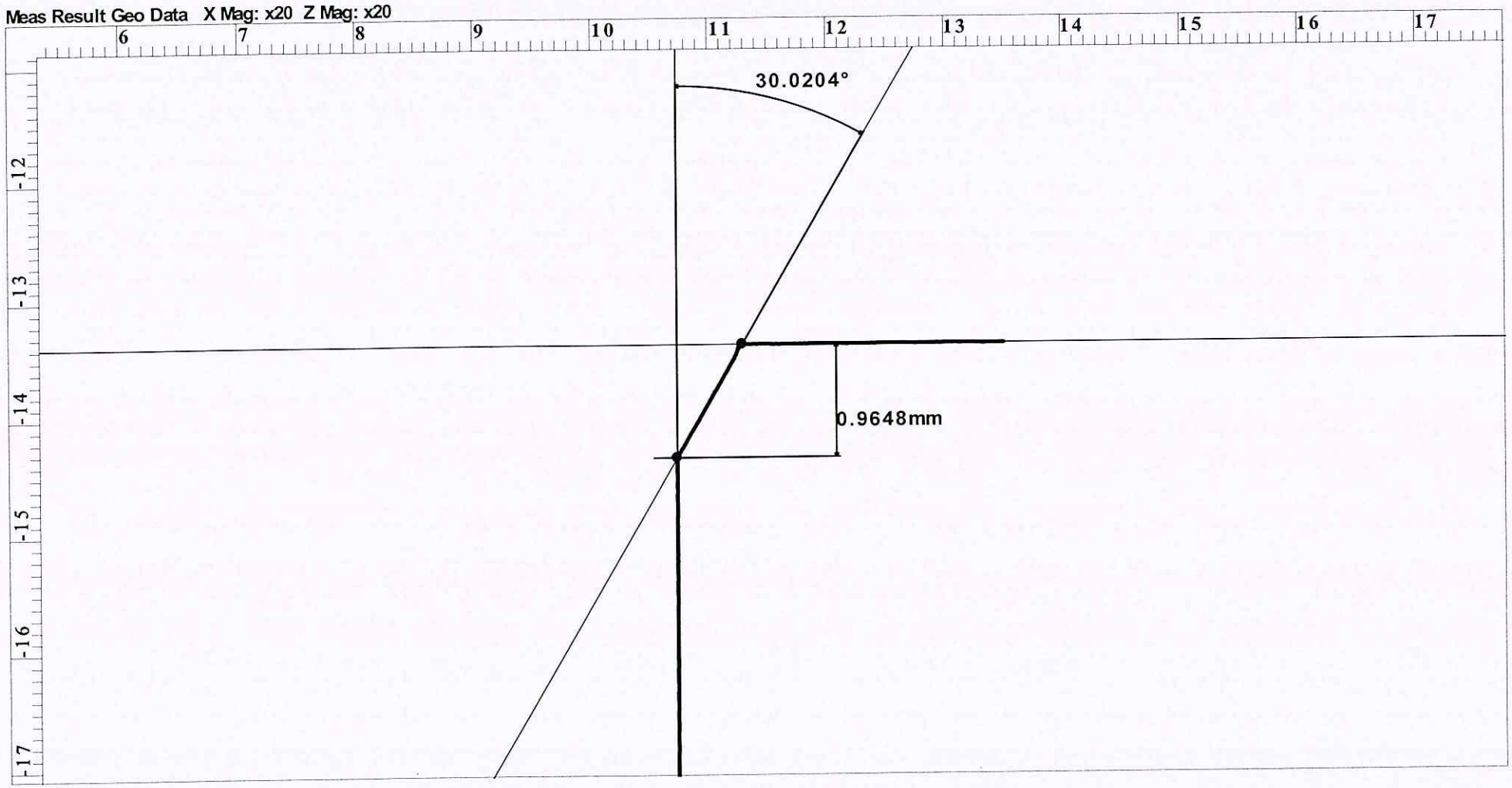
Meas Result Geo Data X Mag: x20 Z Mag: x11.42



1/45

FORO CA23

25/11/17 11:46:56

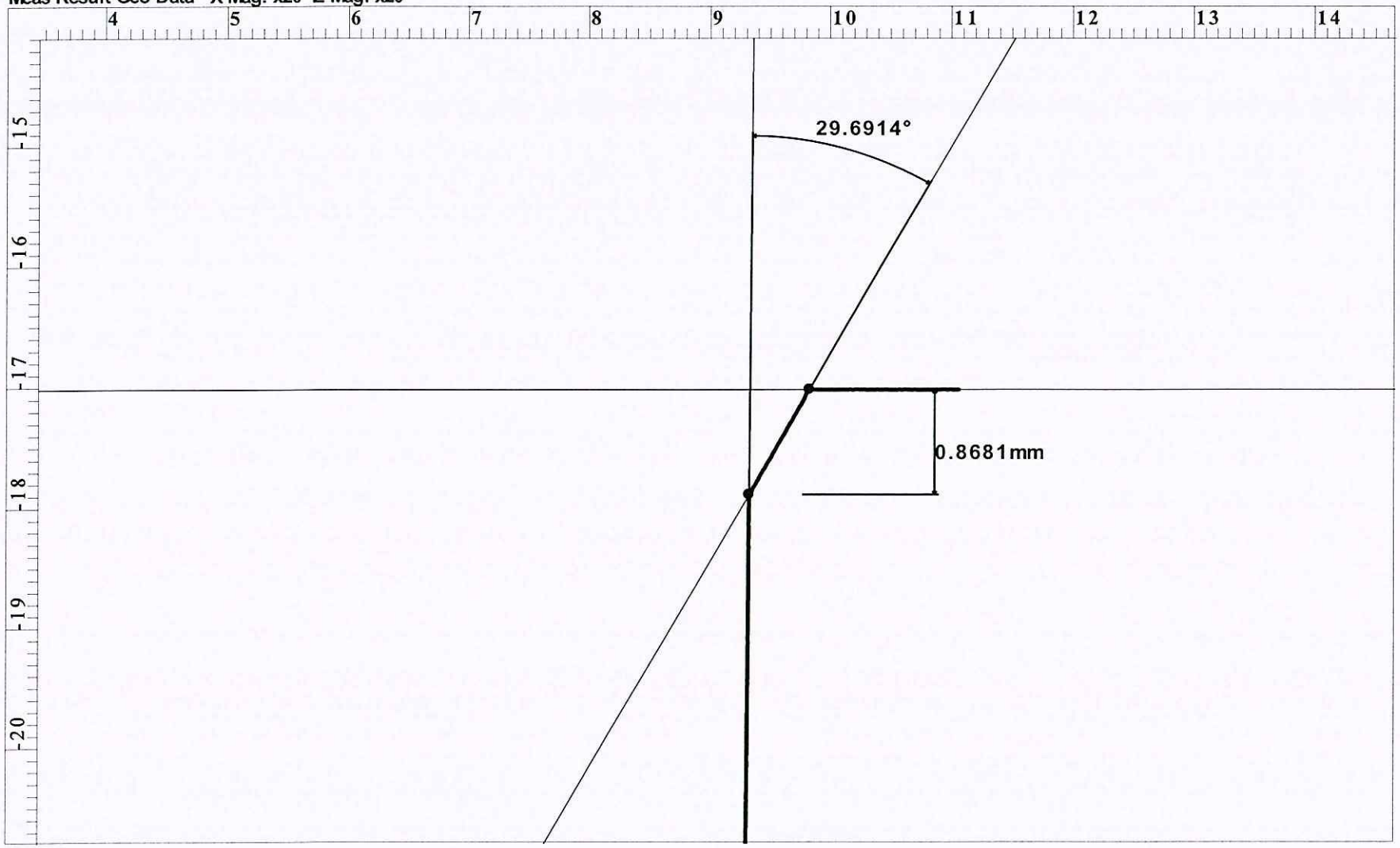


INS

FORO CA13

25/11/17 11:37:26

Meas Result Geo Data X Mag: x20 Z Mag: x20

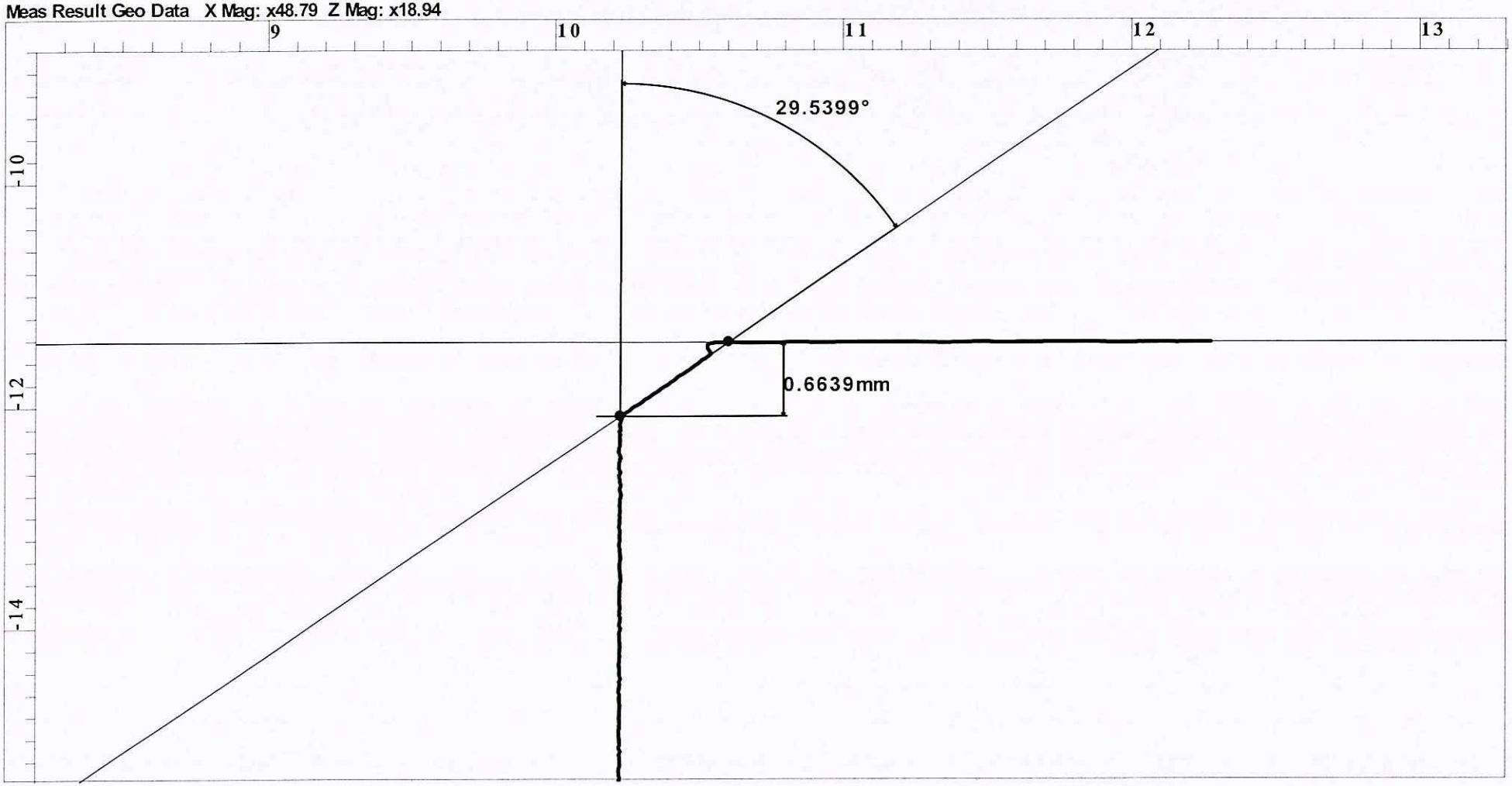


INS

FORO G6

25/11/17 11:26:48

Meas Result Geo Data X Mag: x48.79 Z Mag: x18.94

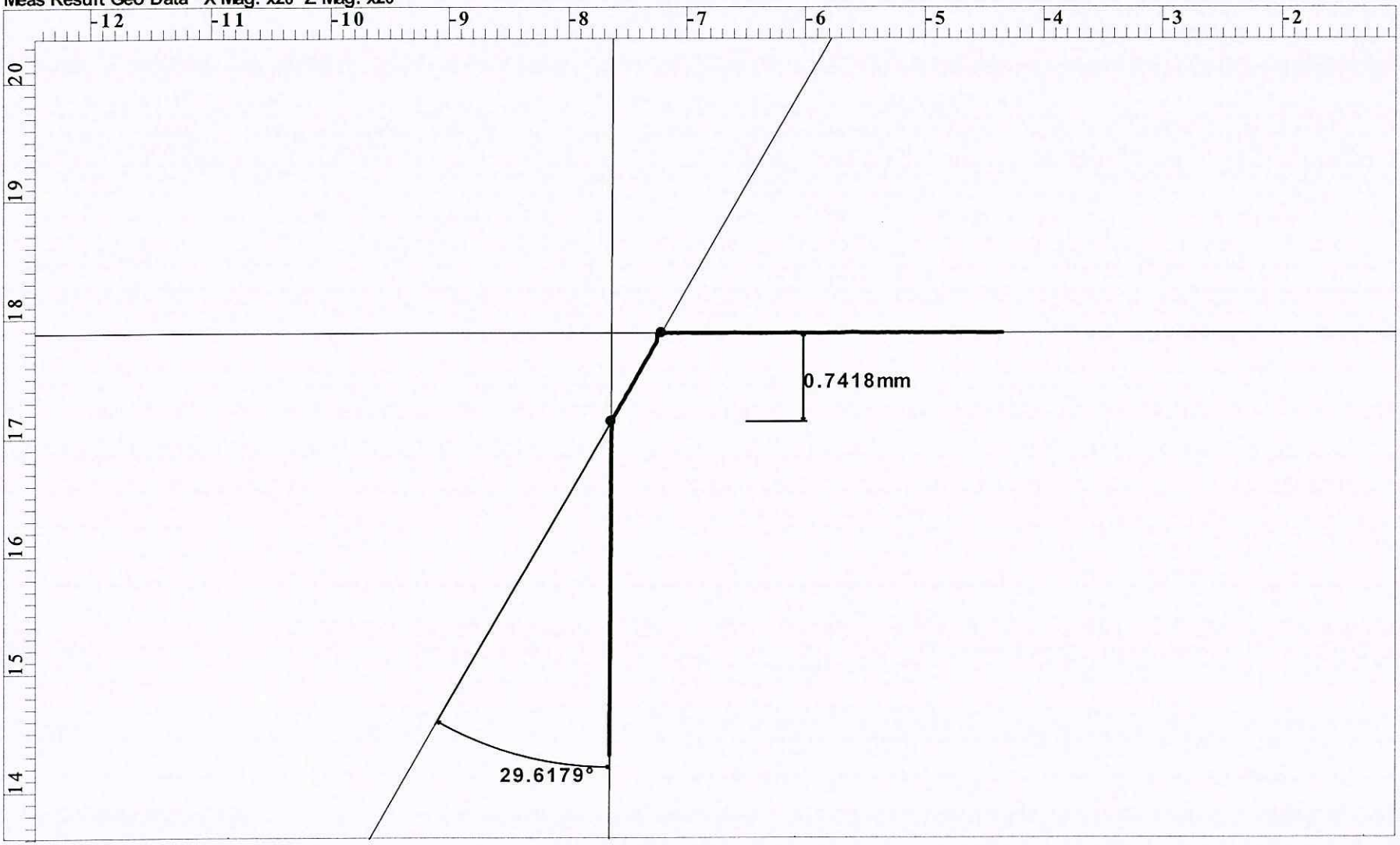


1HS

FORO CA15

25/11/17 11:11:59

Meas Result Geo Data X Mag: x20 Z Mag: x20

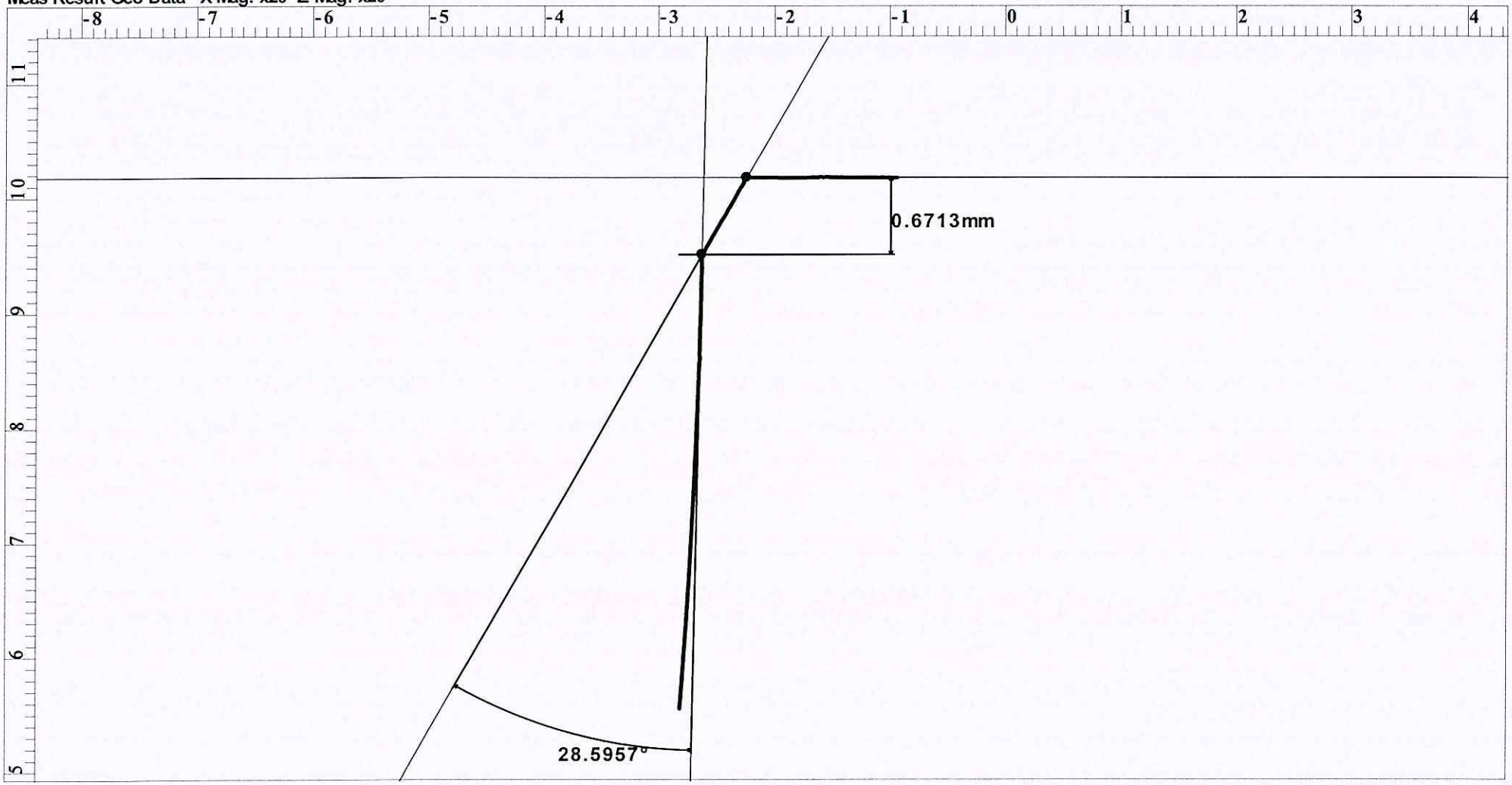


1HS

FORO CA25

25/11/17 11:17:54

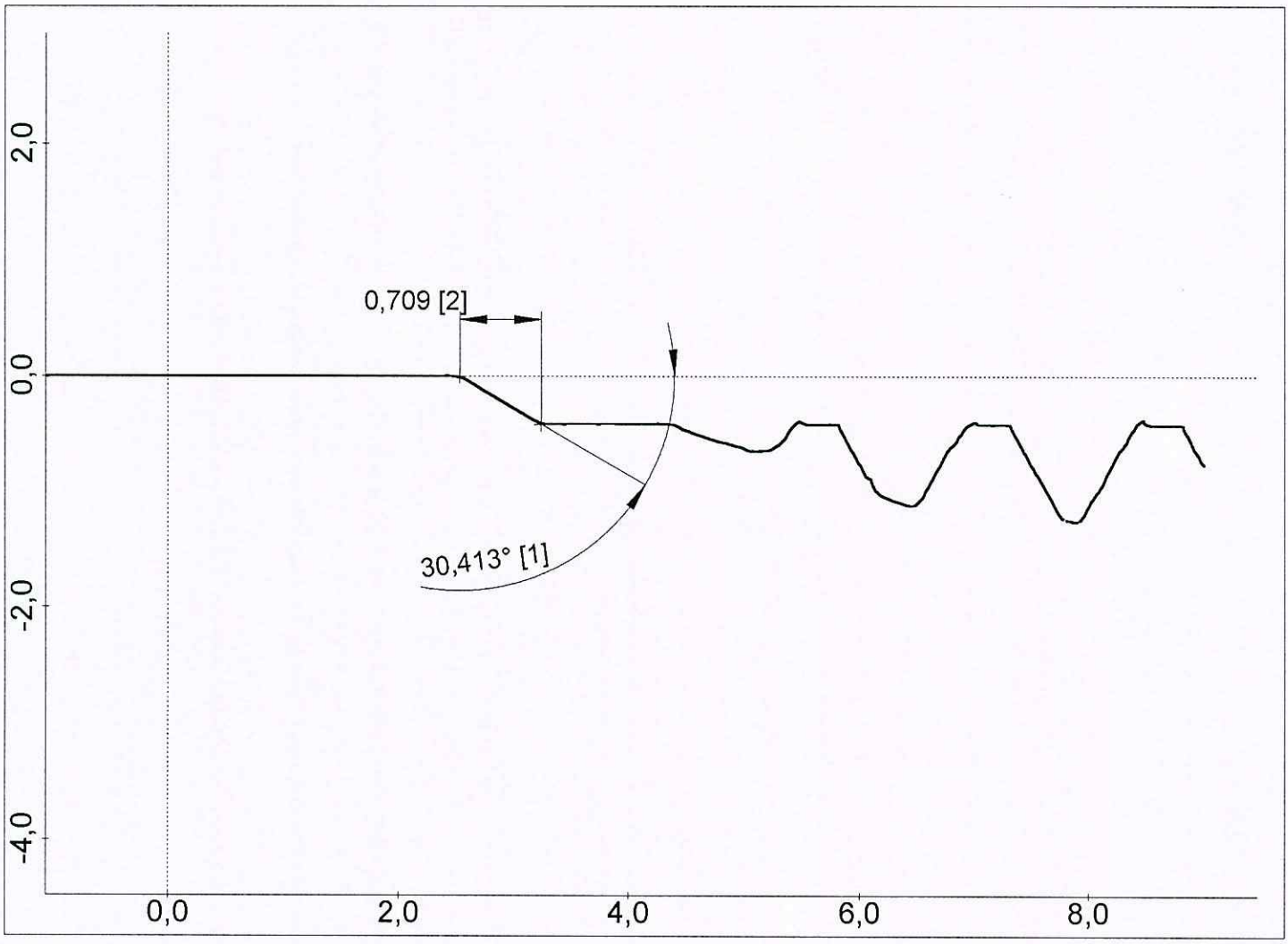
Meas Result Geo Data X Mag: x20 Z Mag: x20



GETRAG

Via dei Ciclamini 4, Modugno (BA)

Oggetto:	CH
Numero:	3321.10
Operatore:	TURNO A
Data, ora:	27.11.2017, 11:40
Nota:	FORO P
Tastatore:	PCV 175-M / 9032212
Macchina:	MOA 416120 002



PERTHOMETER CONCEPT

Area Riservata alla Produzione

Valutazione Profilo

OK ☐

NOK ☐

N°BADGE ODP RICEVENTE

1x15

FORO EL

25/11/17 12:06:38

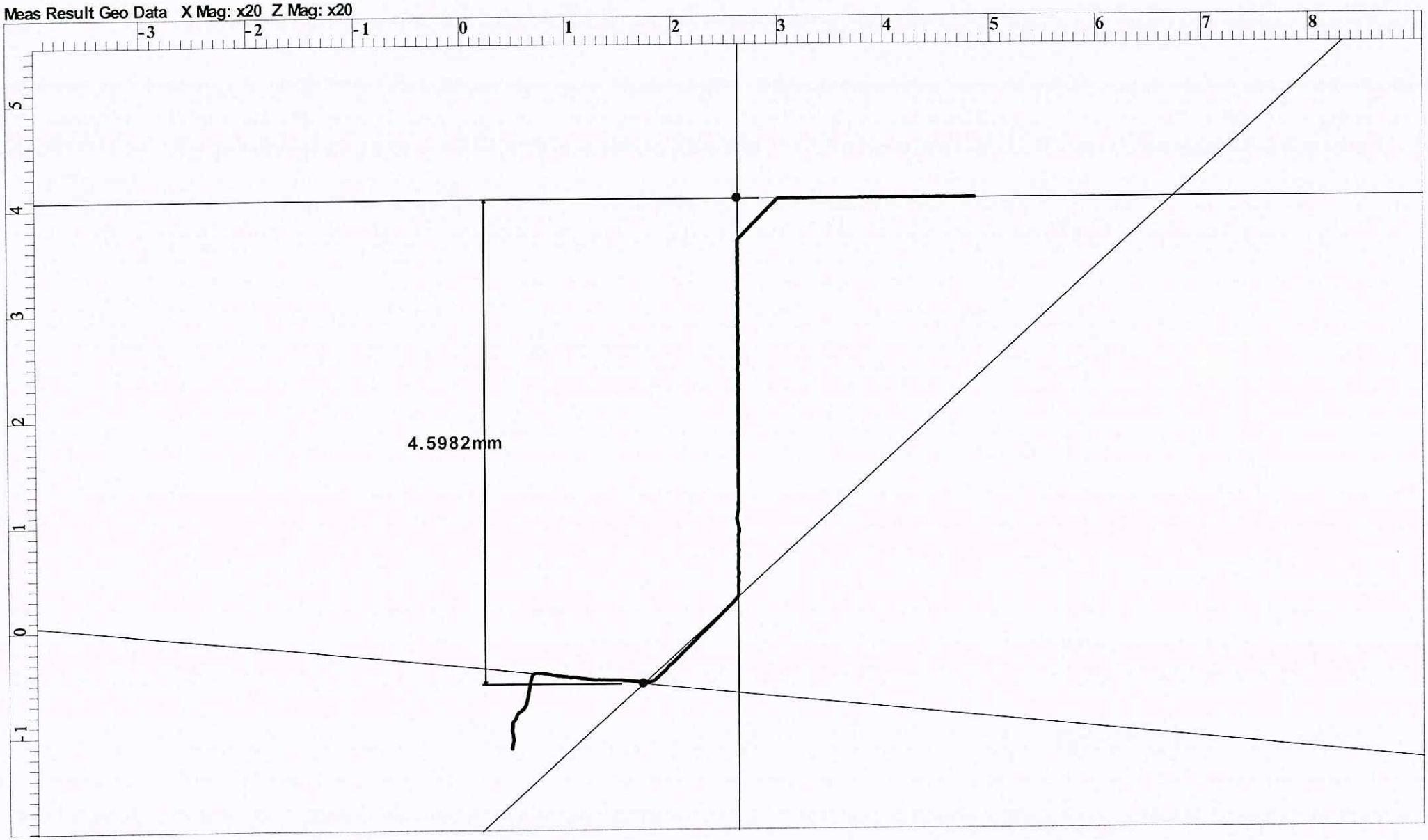
Meas Result Geo Data X Mag: x10 Z Mag: x10

INJ

25/11/17 12:30:17

FORO TRS1

Meas Result Geo Data X Mag: x20 Z Mag: x20

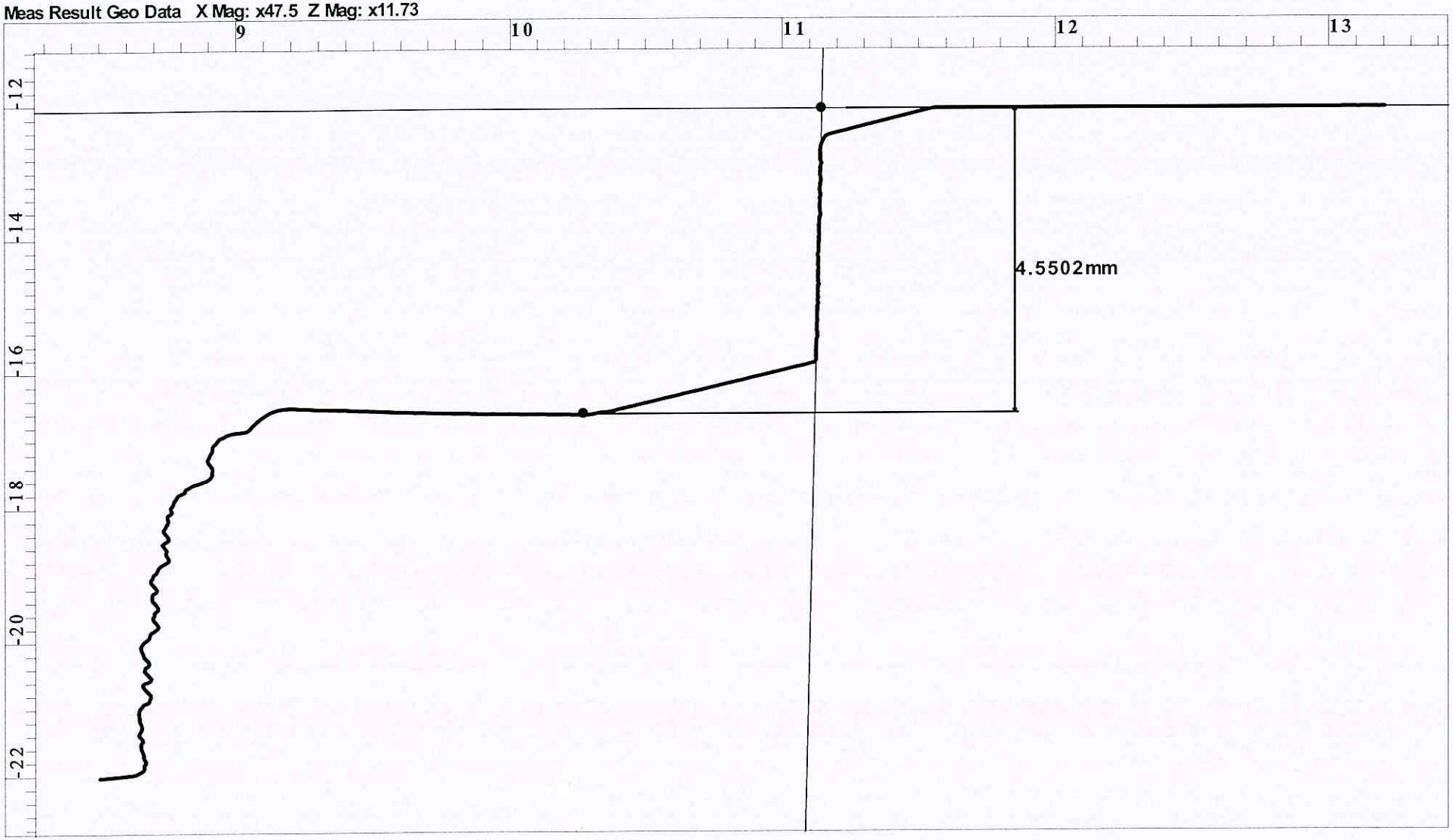


NLS

FORO TRS2

25/11/17 12:25:26

Meas Result Geo Data X Mag: x47.5 Z Mag: x11.73

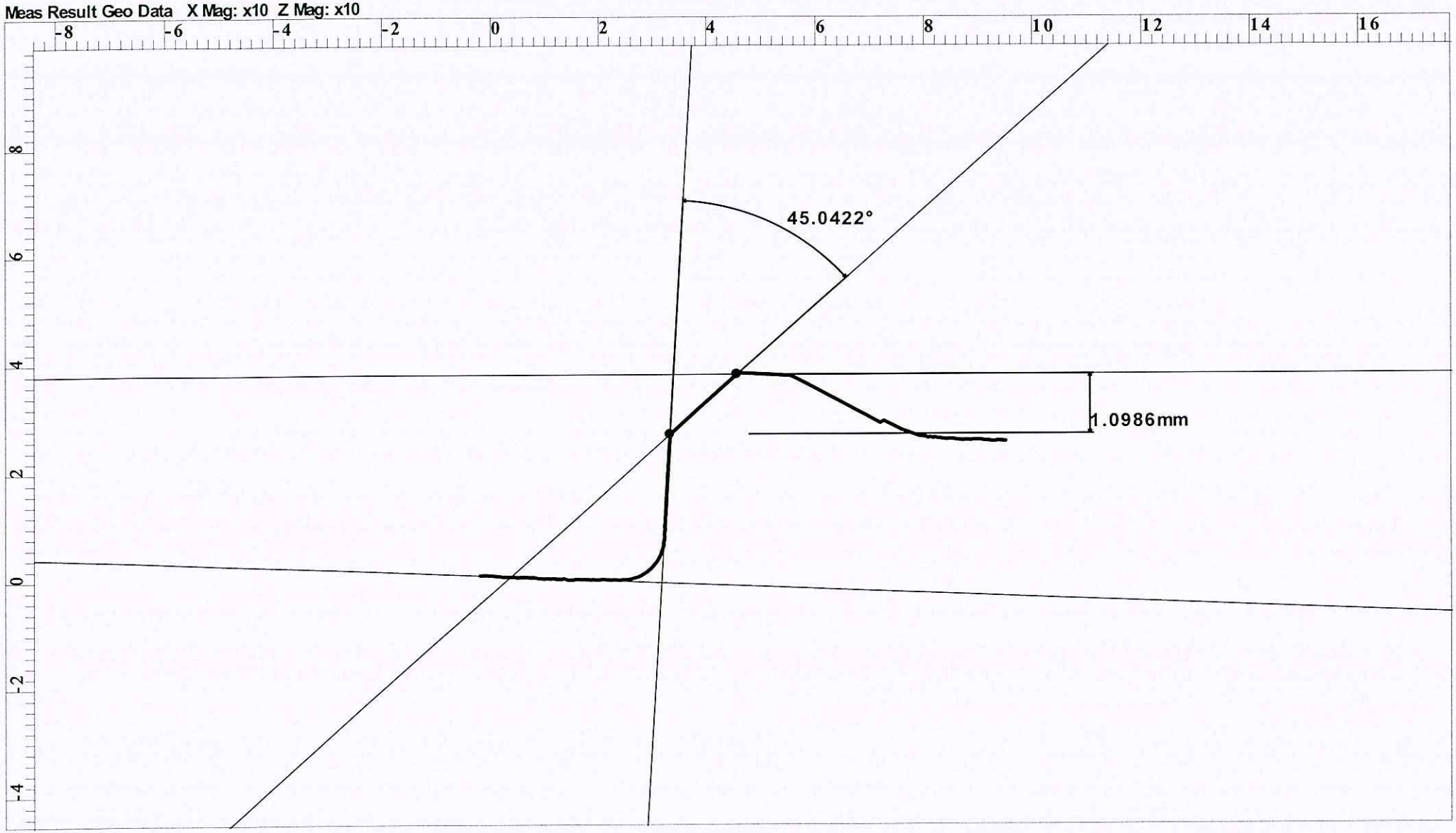


INS

FORO GTS3

25/11/17 10:47:30

Meas Result Geo Data X Mag: x10 Z Mag: x10

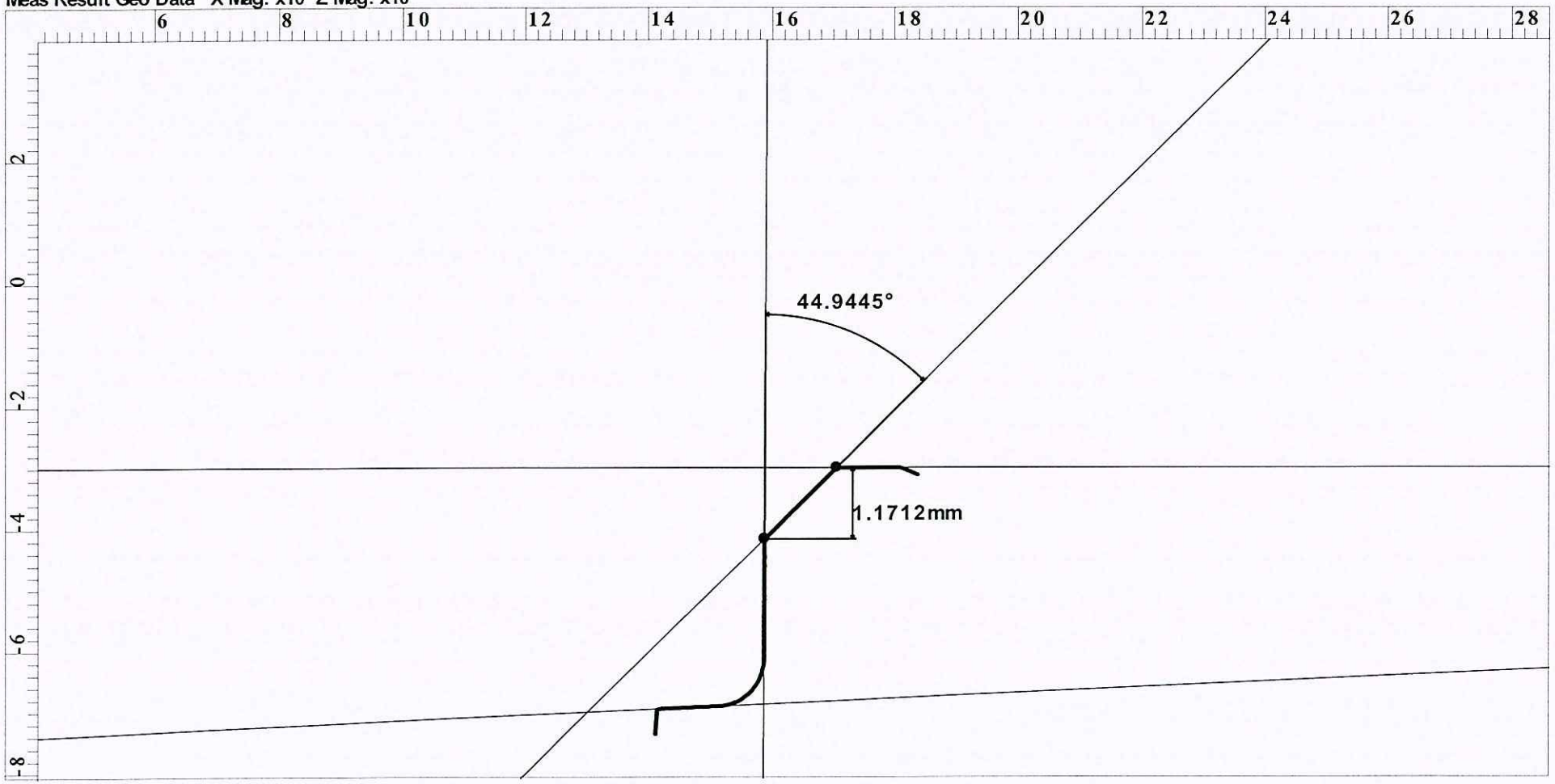


INS

FORO GTS2

25/11/17 10:52:59

Meas Result Geo Data X Mag: x10 Z Mag: x10

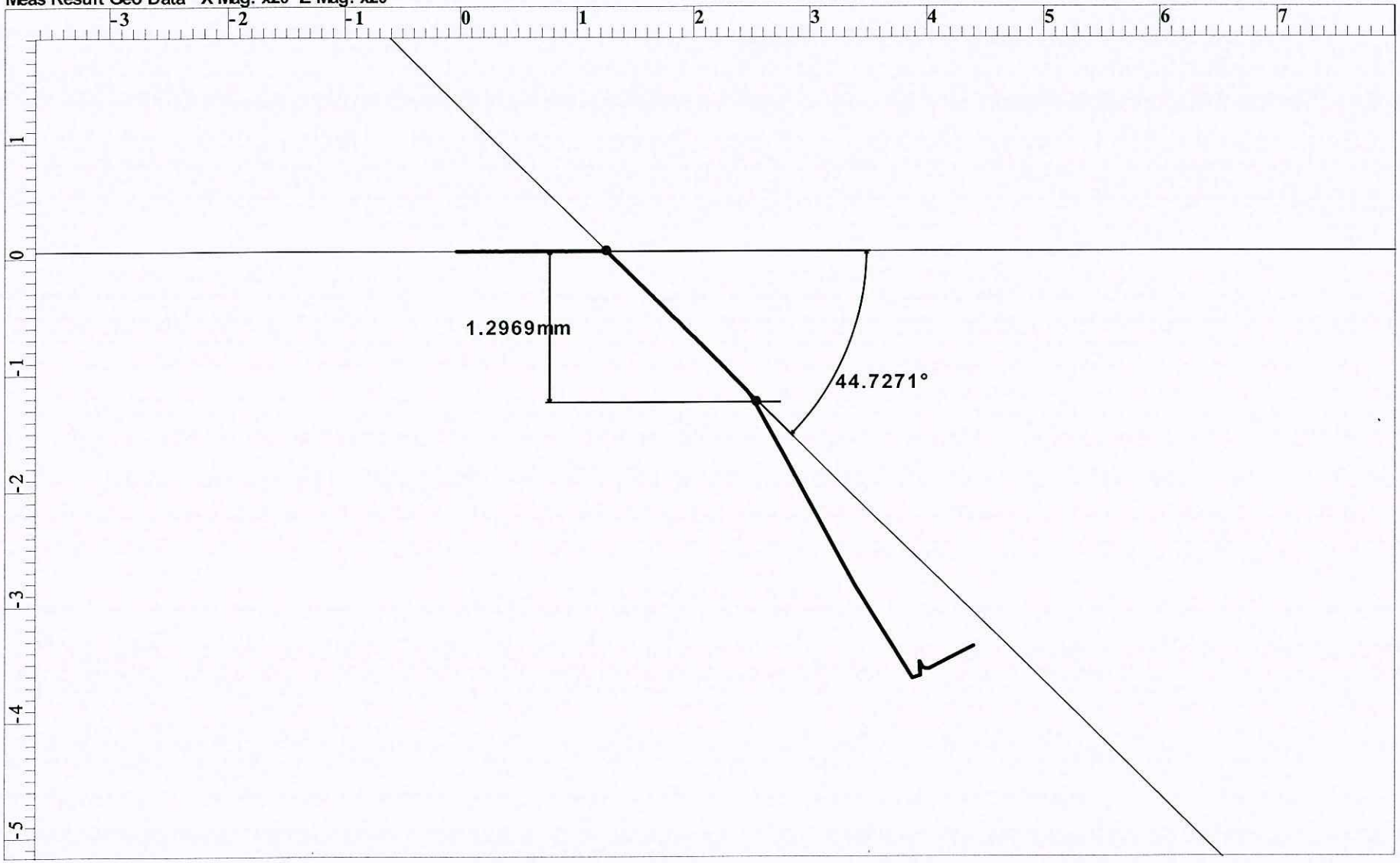


INS

FORO GTS1

25/11/17 11:00:31

Meas Result Geo Data X Mag: x20 Z Mag: x20

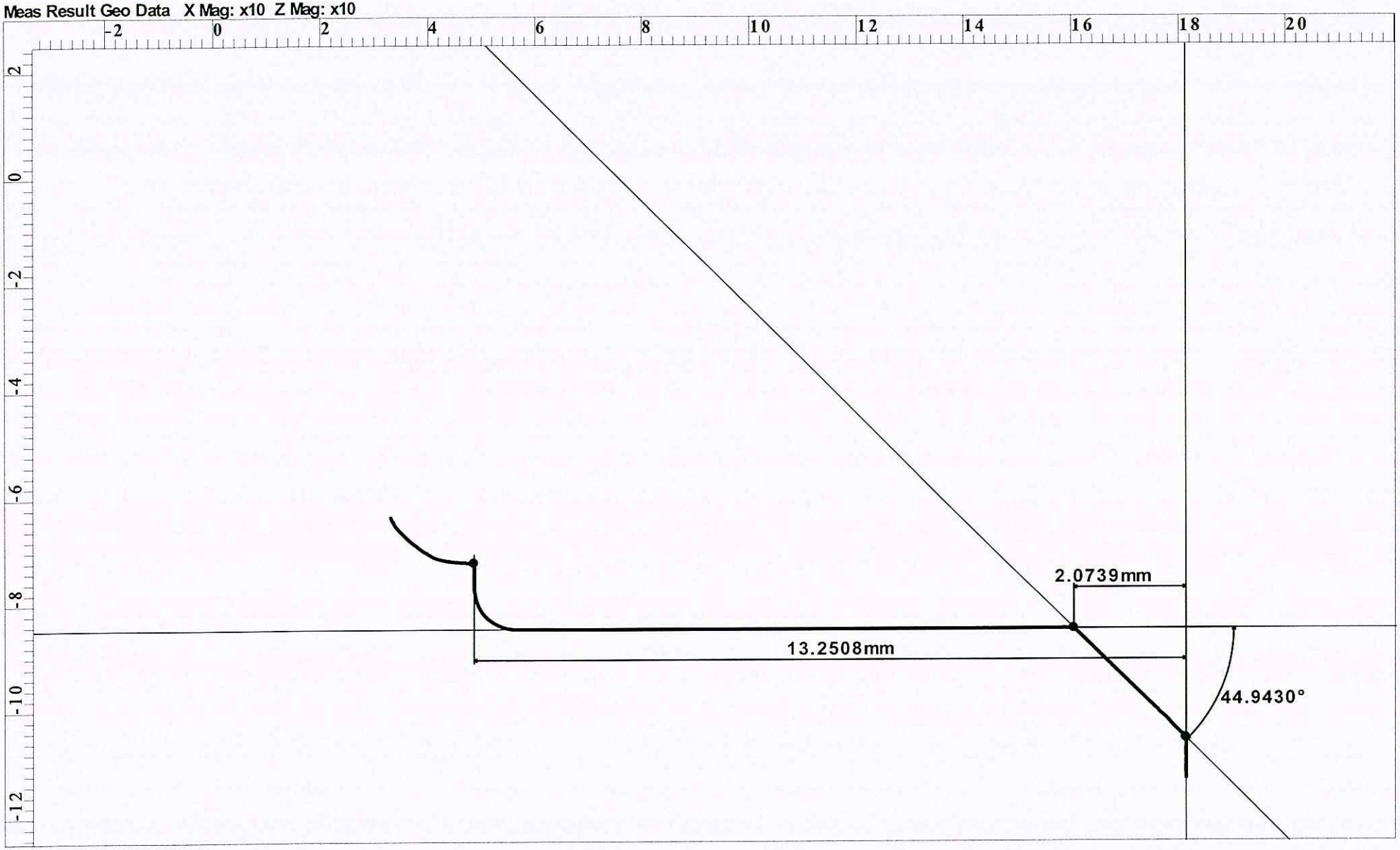


1 of 5

FORO SD2

25/11/17 10:31:06

Meas Result Geo Data X Mag: x10 Z Mag: x10

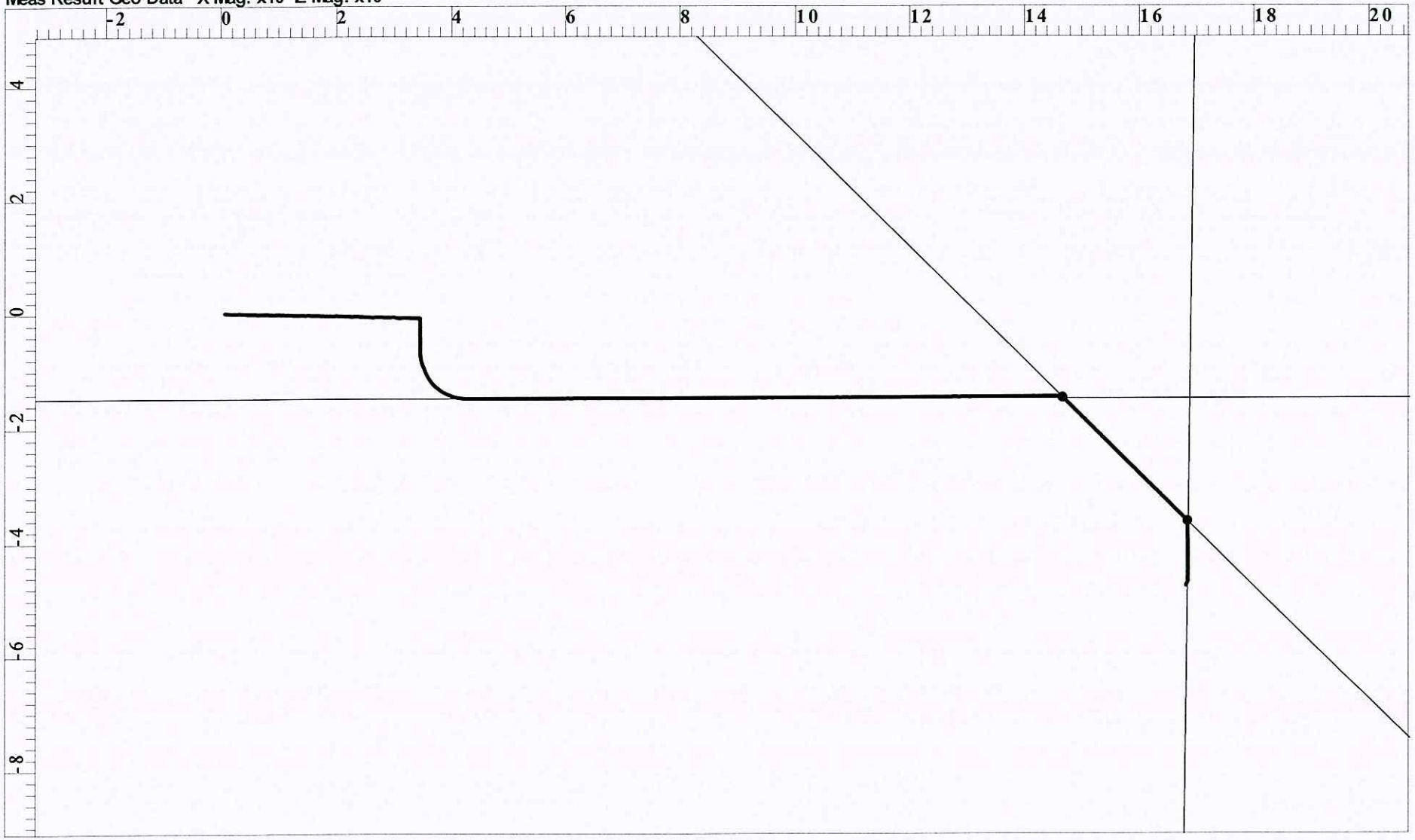


1/N S

FORO SD1

25/11/17 10:32:18

Meas Result Geo Data X Mag: x10 Z Mag: x10

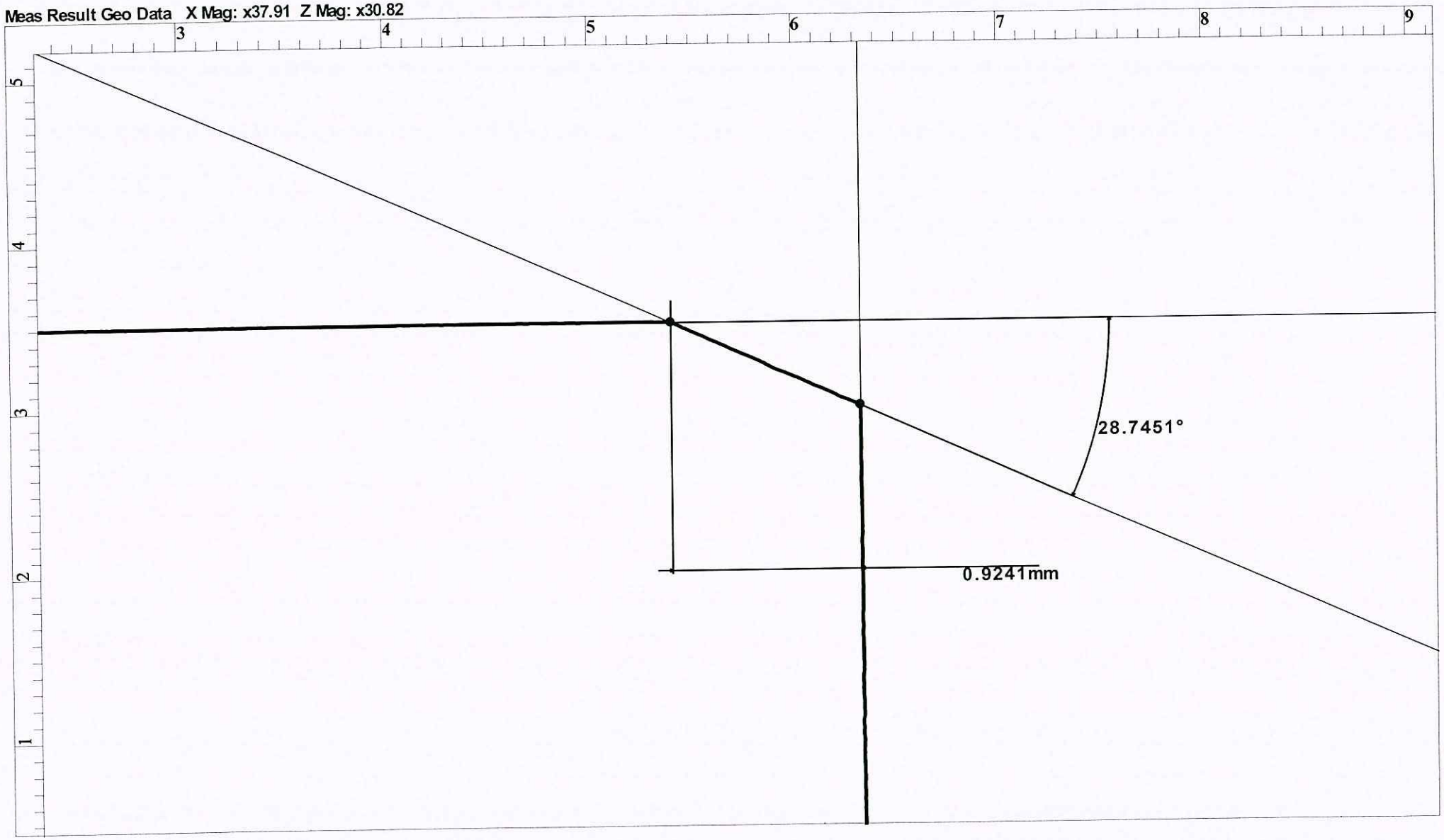


OK

FORO P

23/11/17 09:44:22

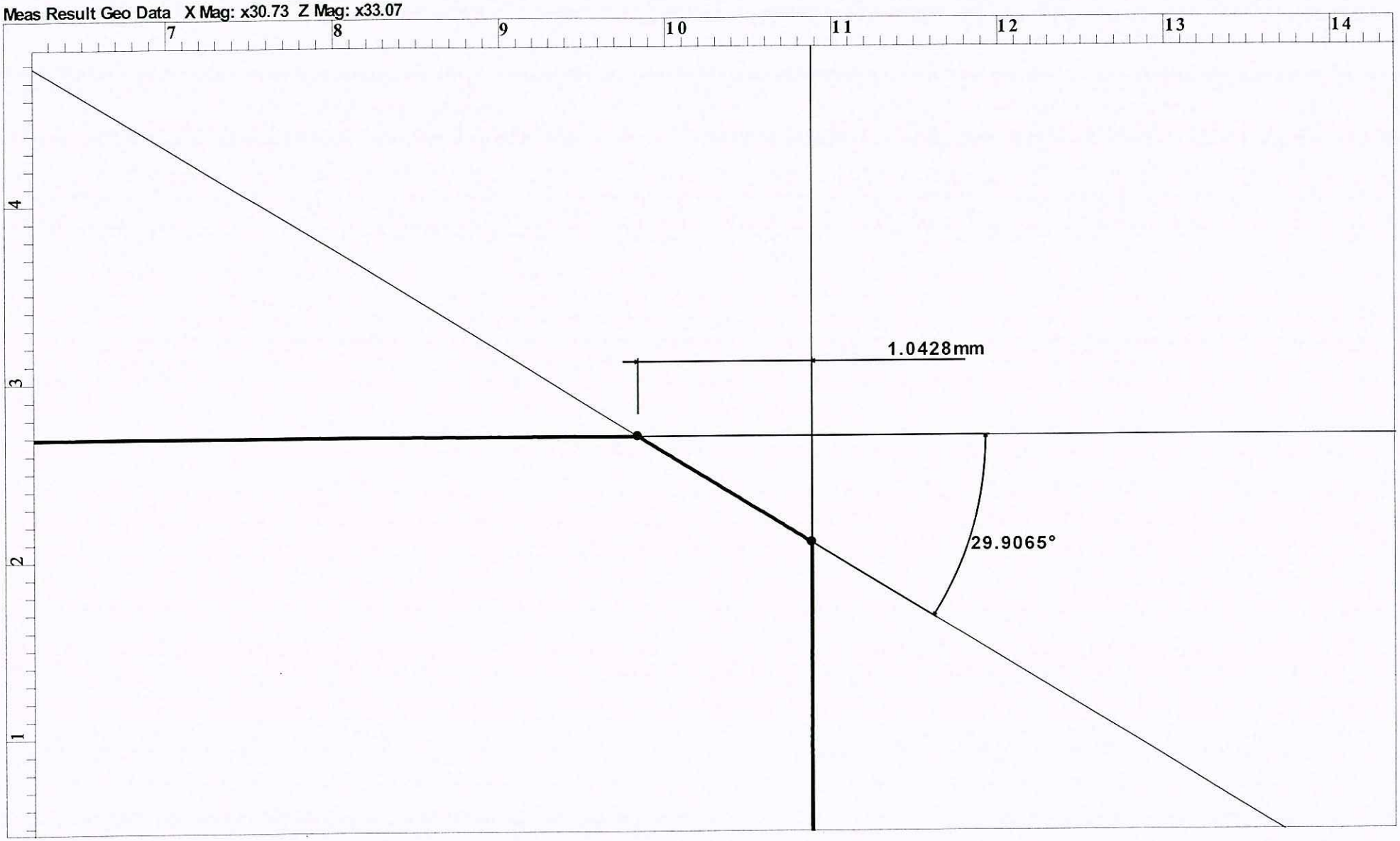
Meas Result Geo Data X Mag: x37.91 Z Mag: x30.82



FORO P1

23/11/17 09:51:45

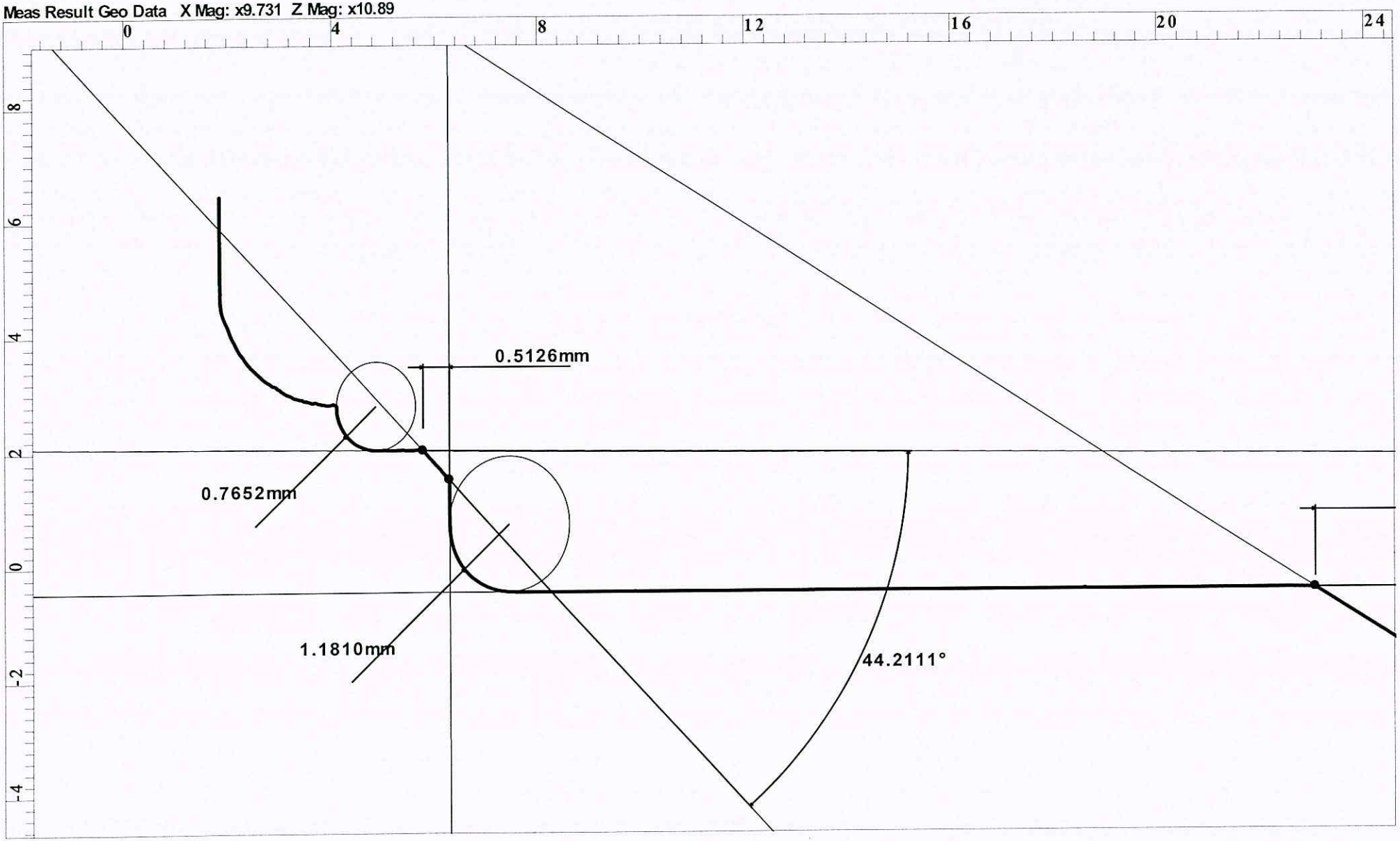
Meas Result Geo Data X Mag: x30.73 Z Mag: x33.07



FORO S1

23/11/17 09:31:09 OK

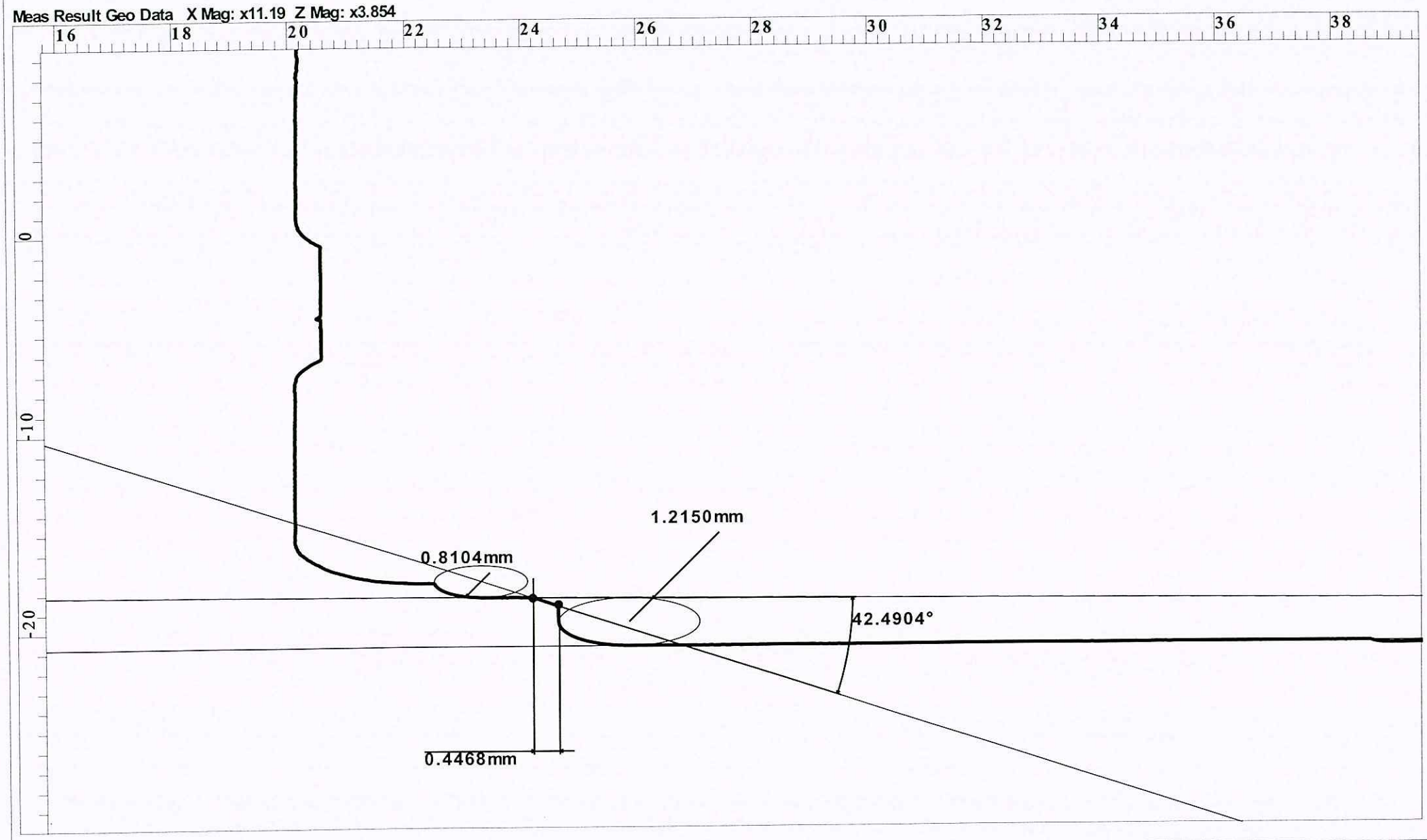
Meas Result Geo Data X Mag: x9.731 Z Mag: x10.89



FORO L1

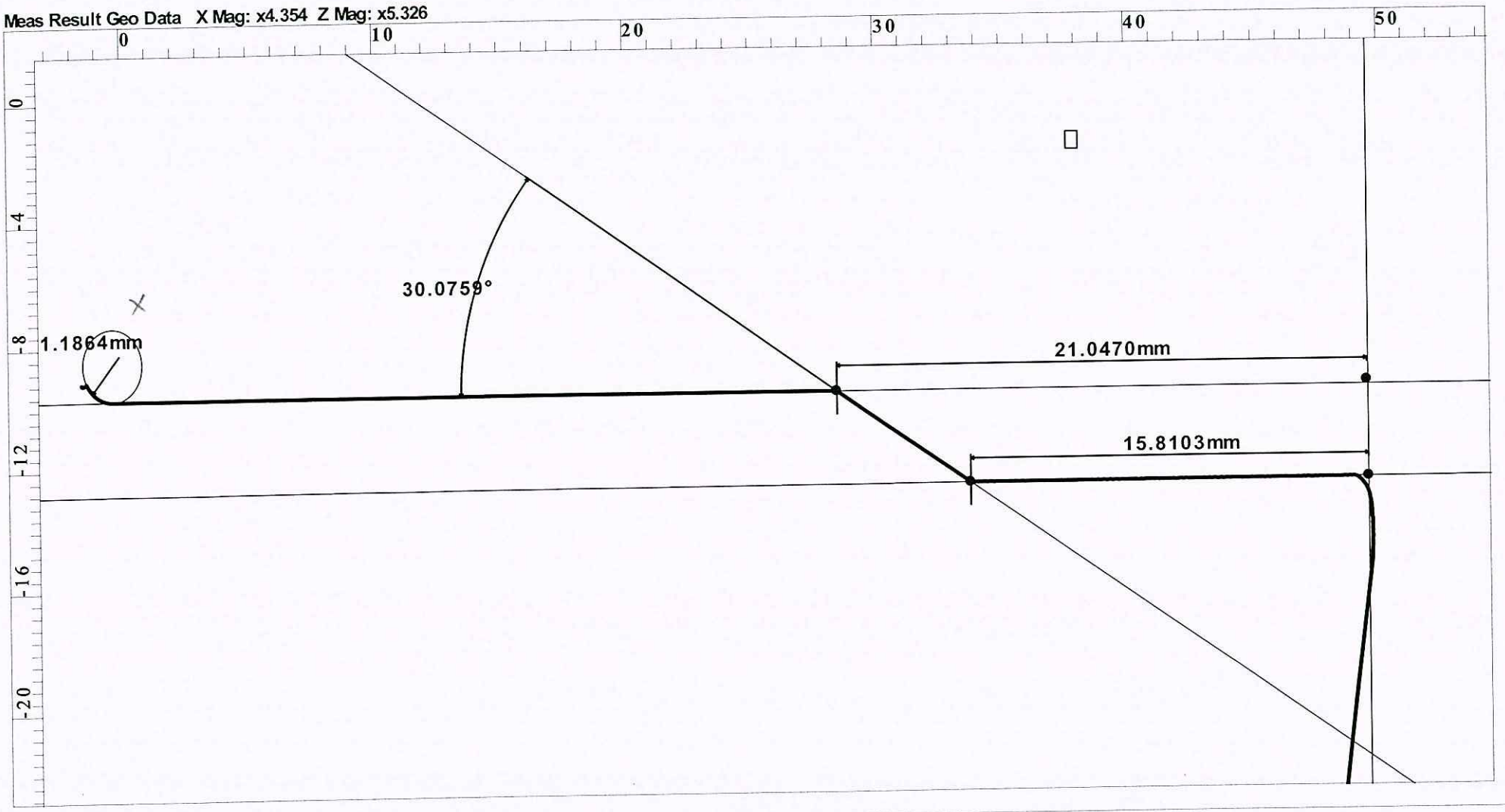
23/11/17 09:24:08 OK

Meas Result Geo Data X Mag: x11.19 Z Mag: x3.854



raggio su grezzo CA1

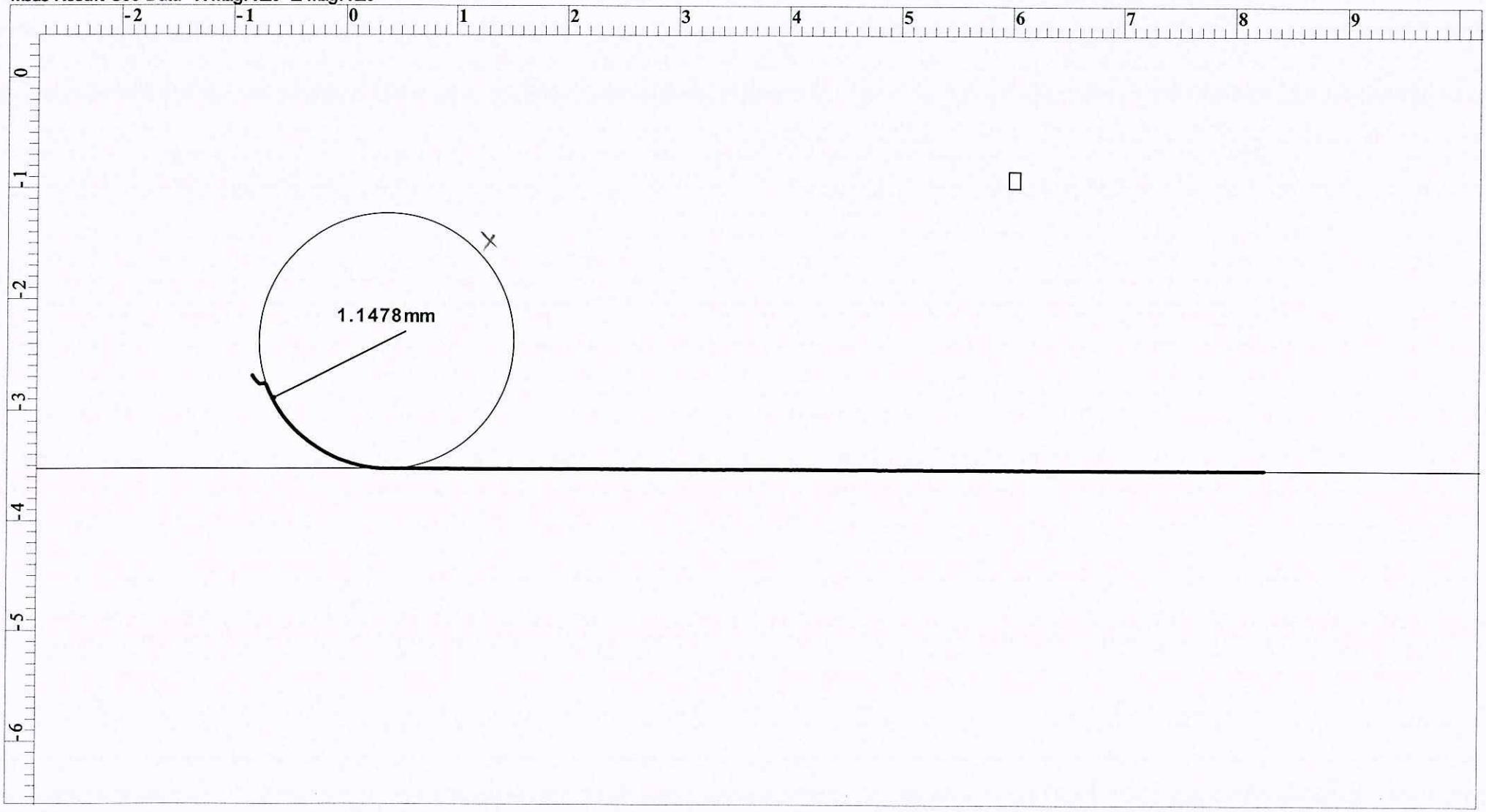
22/11/17 11:46:04



raggio su grezzo CA2

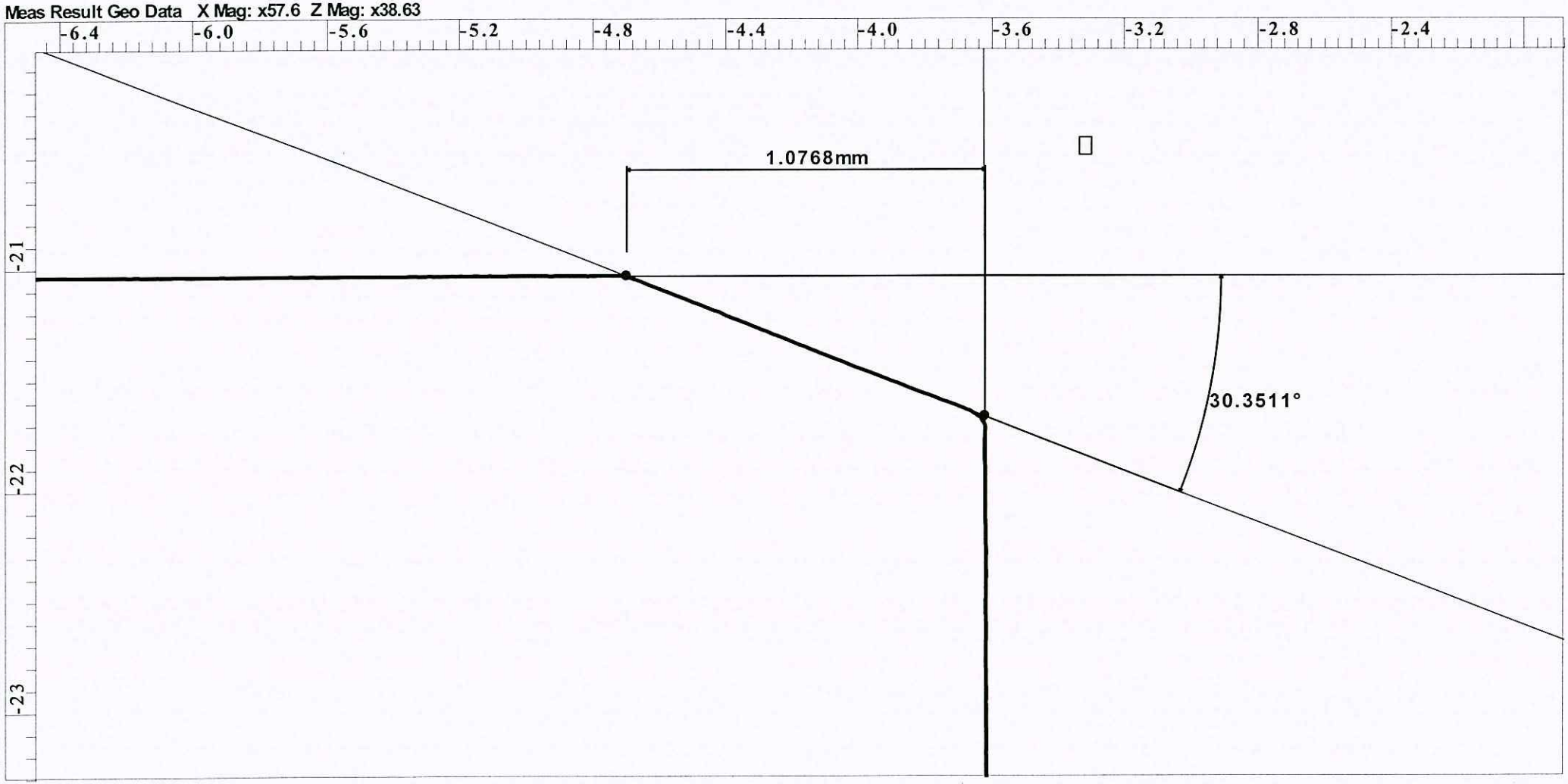
22/11/17 11:20:31

Meas Result Geo Data X Mag: x20 Z Mag: x20



smusso Dg4 **22/11/17 12:01:32**

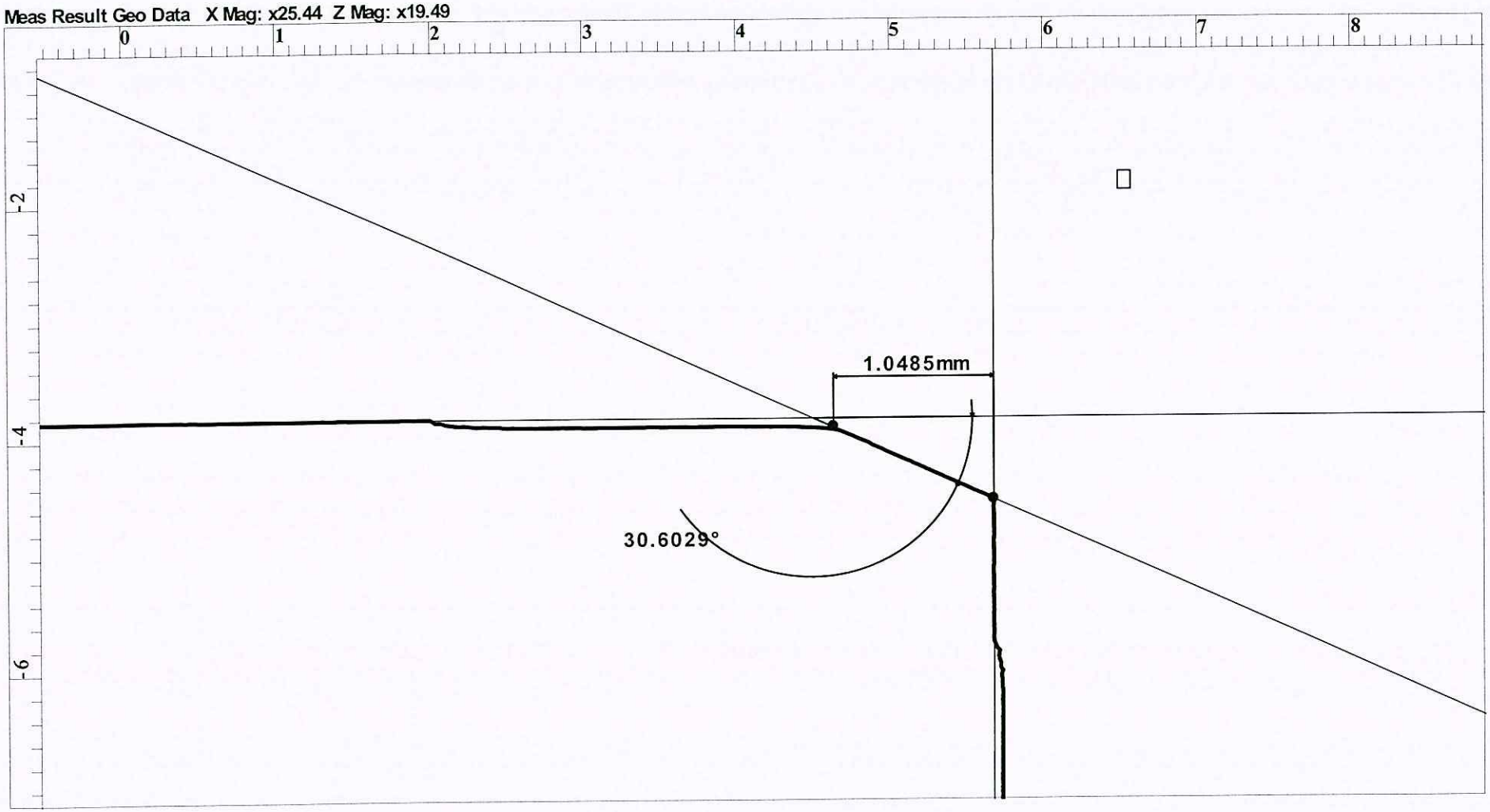
Meas Result Geo Data X Mag: x57.6 Z Mag: x38.63



22/11/17 12:04:34

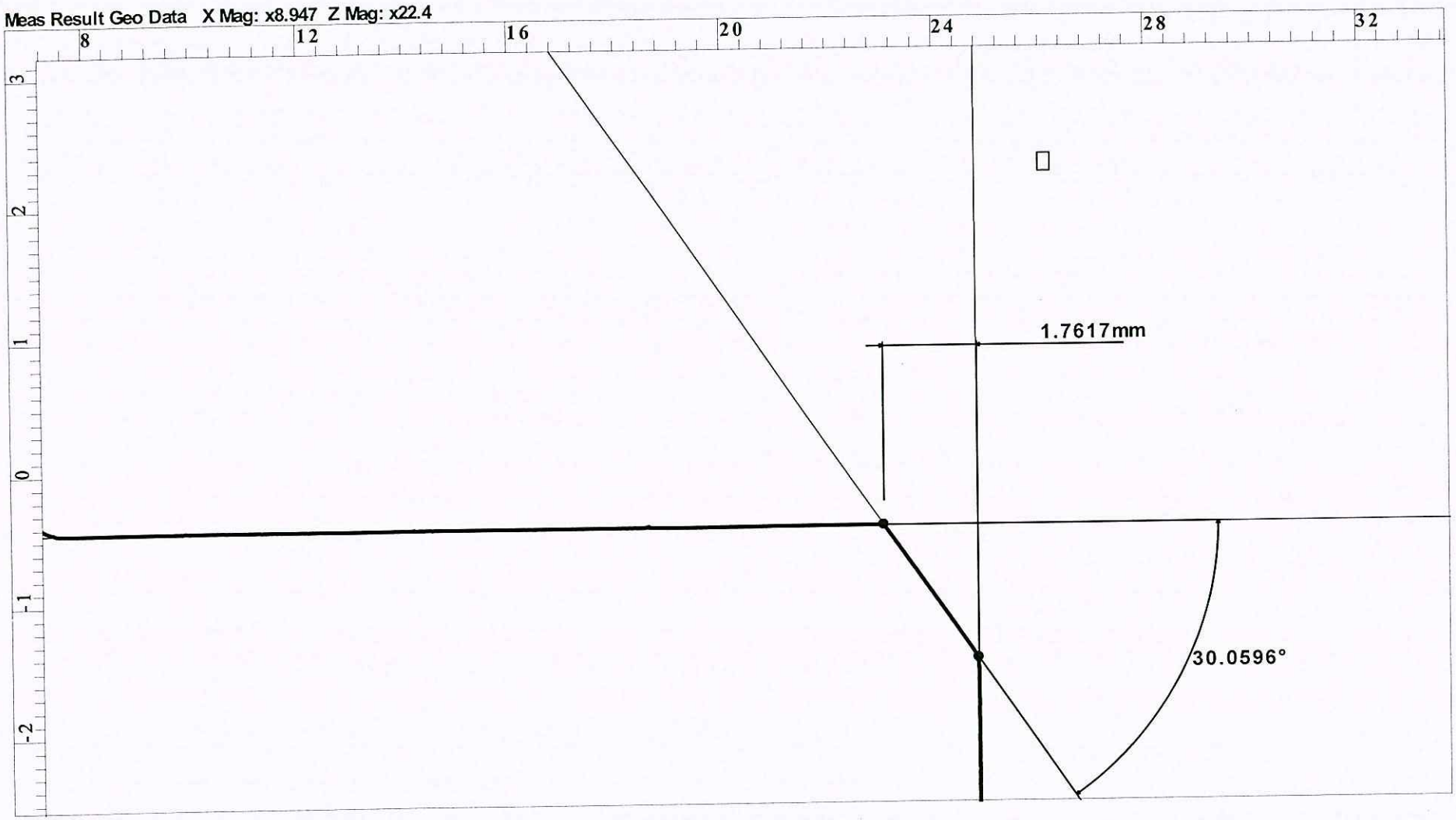
smusso Dg2

Meas Result Geo Data X Mag: x25.44 Z Mag: x19.49



SMUSSO FORO S

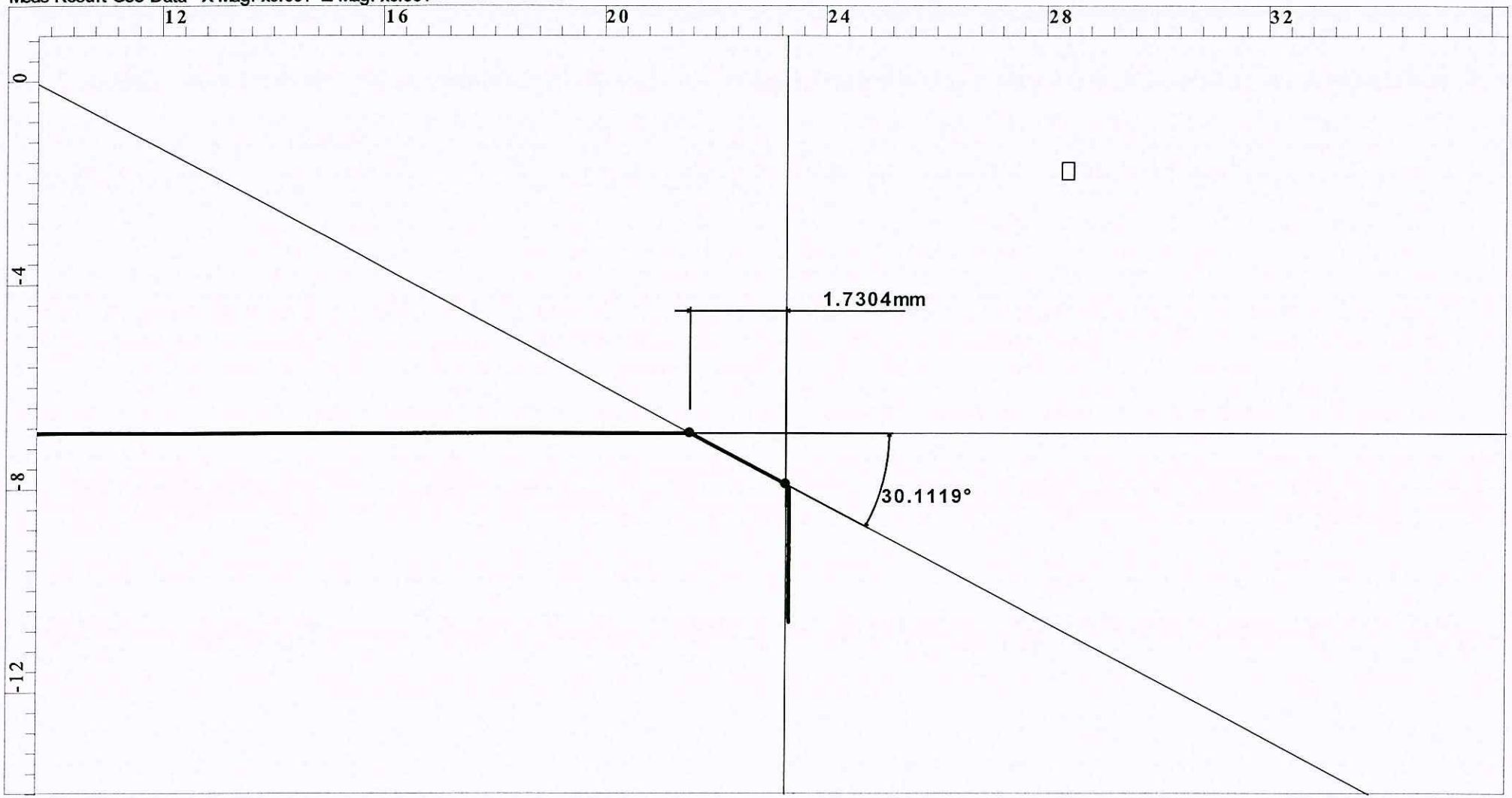
22/11/17 12:35:31



SMUSSO FORO L

22/11/17 12:40:47

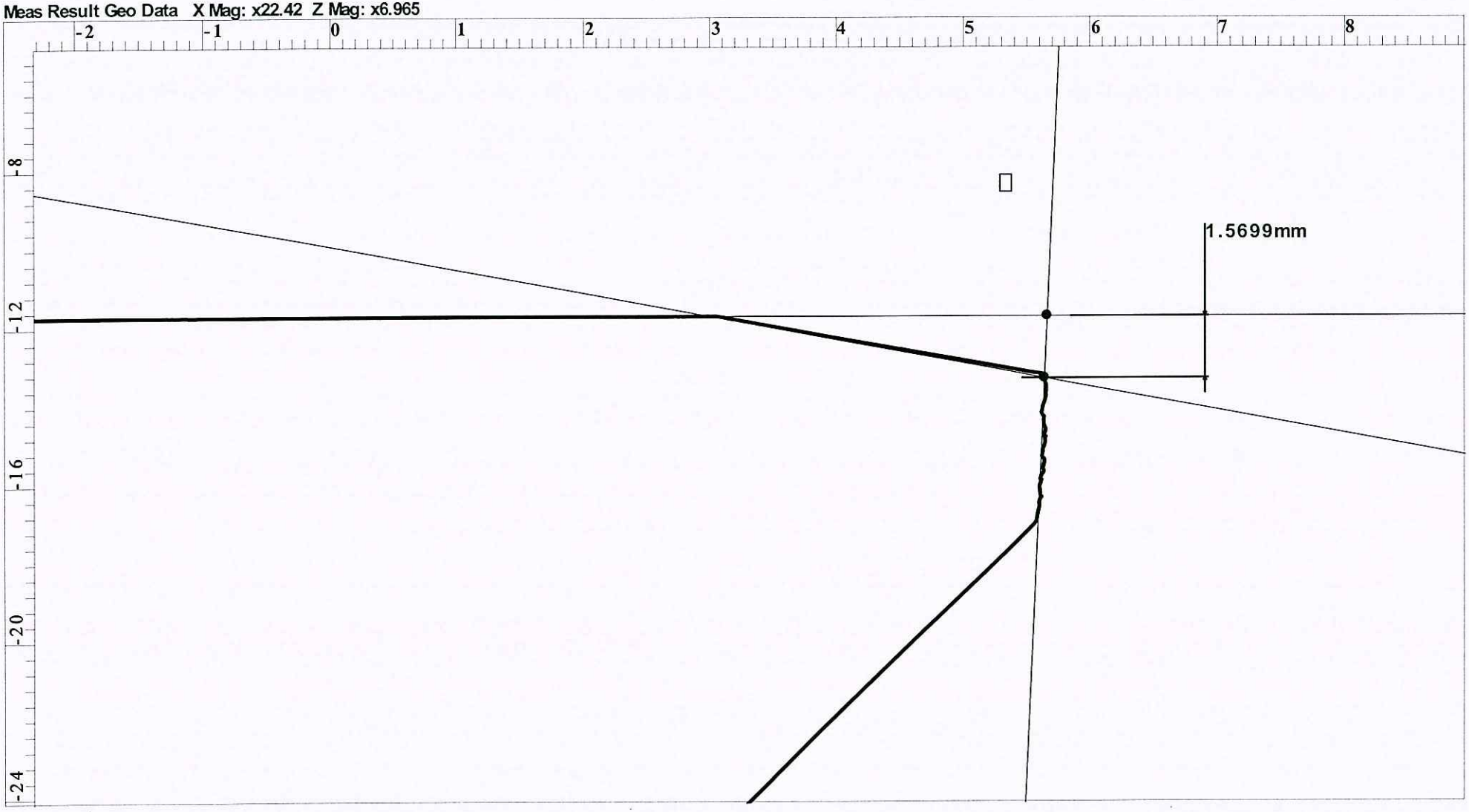
Meas Result Geo Data X Mag: x9.661 Z Mag: x8.951



FORO F Ø67

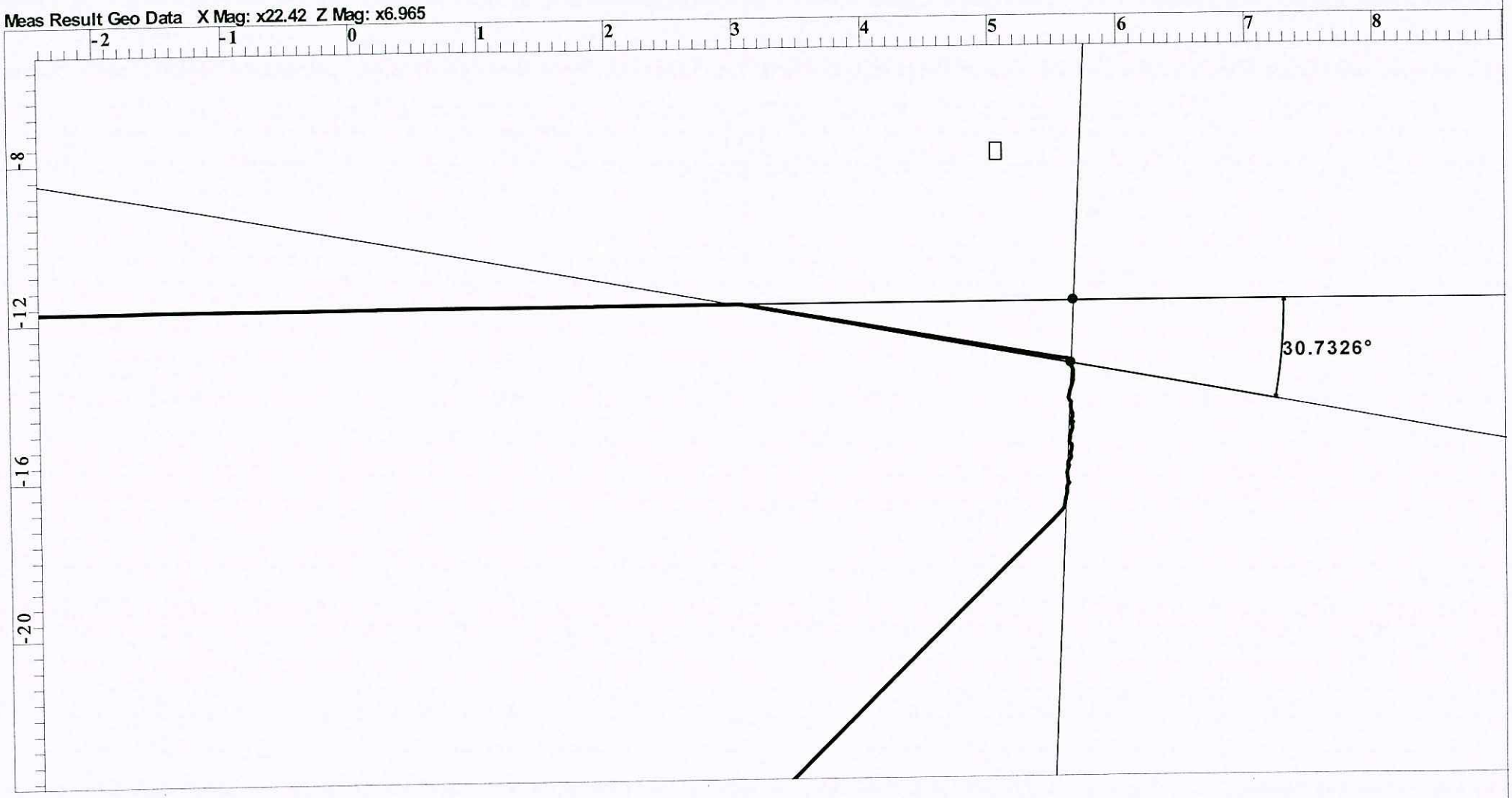
22/11/17 13:03:02

Meas Result Geo Data X Mag: x22.42 Z Mag: x6.965



FORO F Ø67

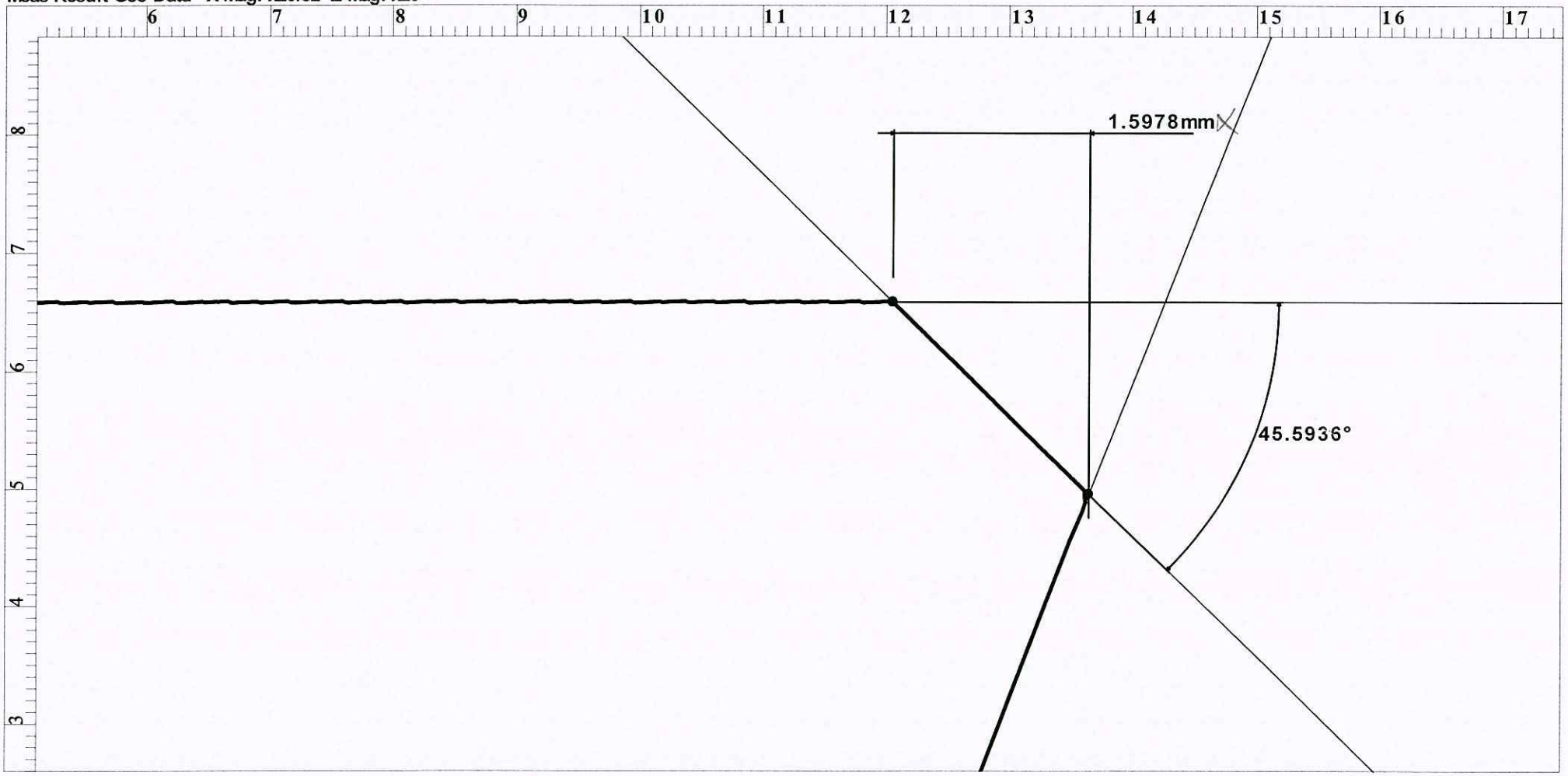
22/11/17 13:05:08



SMUSSO A 45° CA1

23/11/17 10:12:23

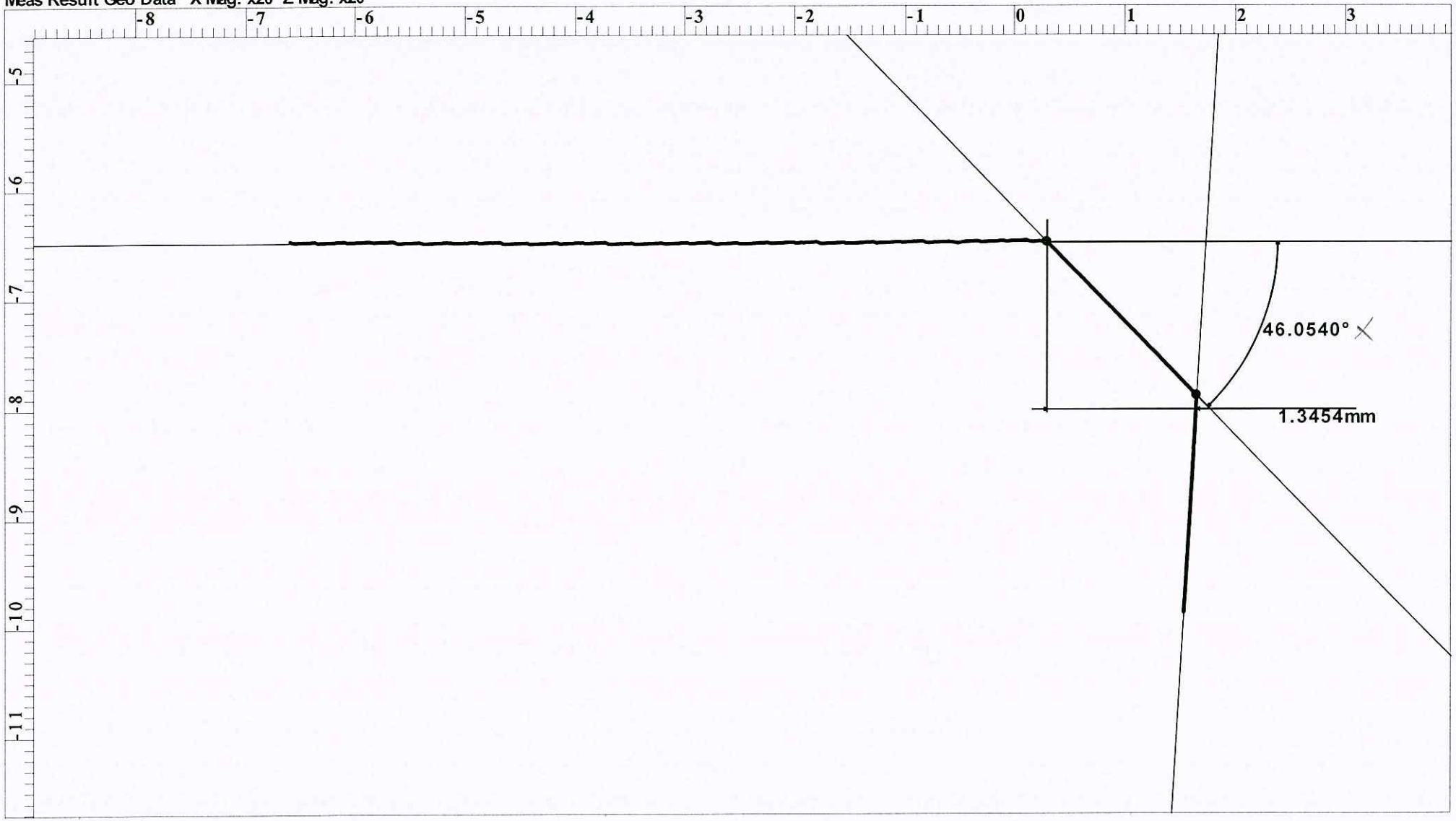
Meas Result Geo Data X Mag: x20.82 Z Mag: x20



SMUSSO A 45° CA2

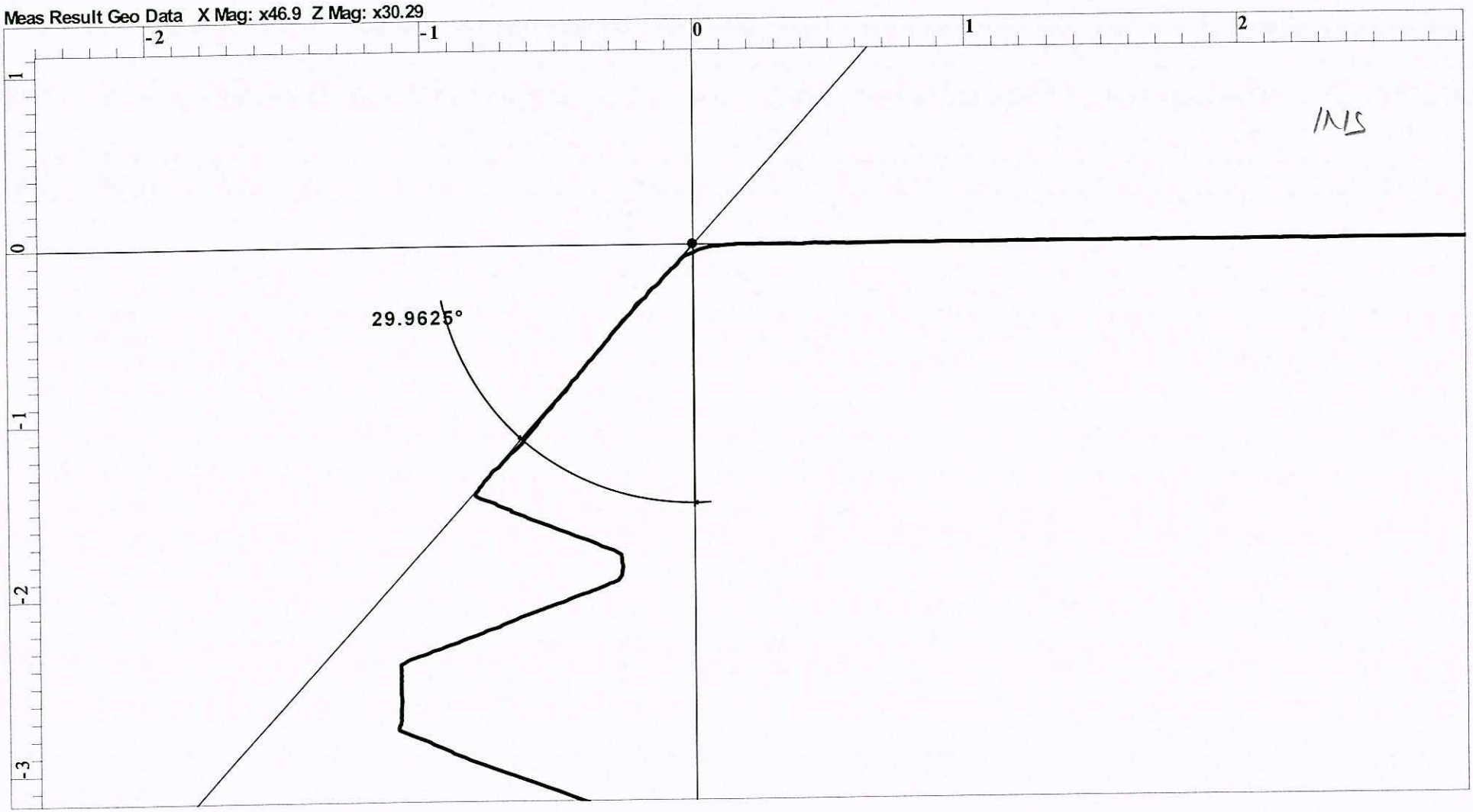
23/11/17 10:02:23

Meas Result Geo Data X Mag: x20 Z Mag: x20



SMUSSO OD

23/11/17 10:34:12

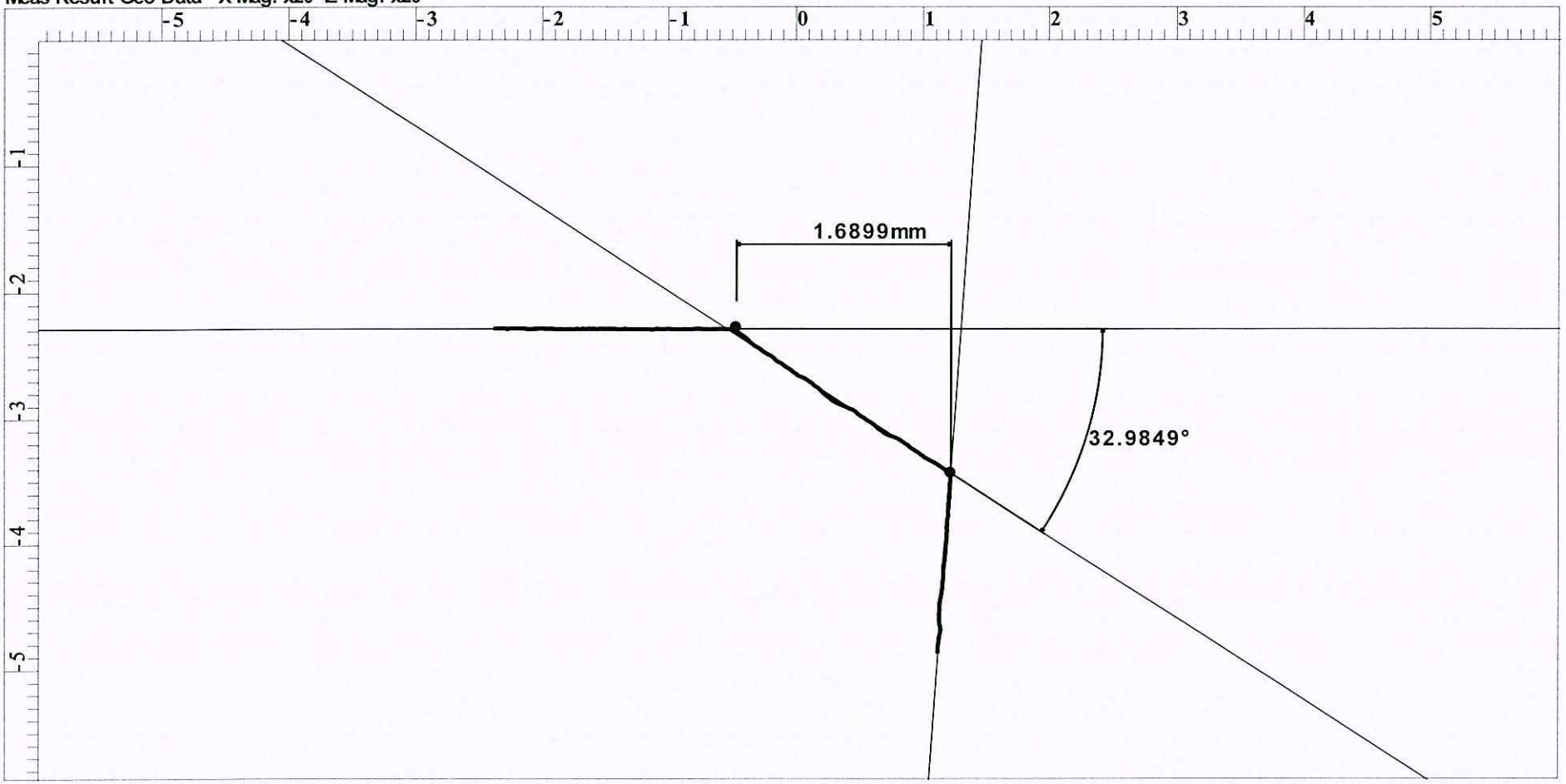


FORO V

INS

23/11/17 11:12:13

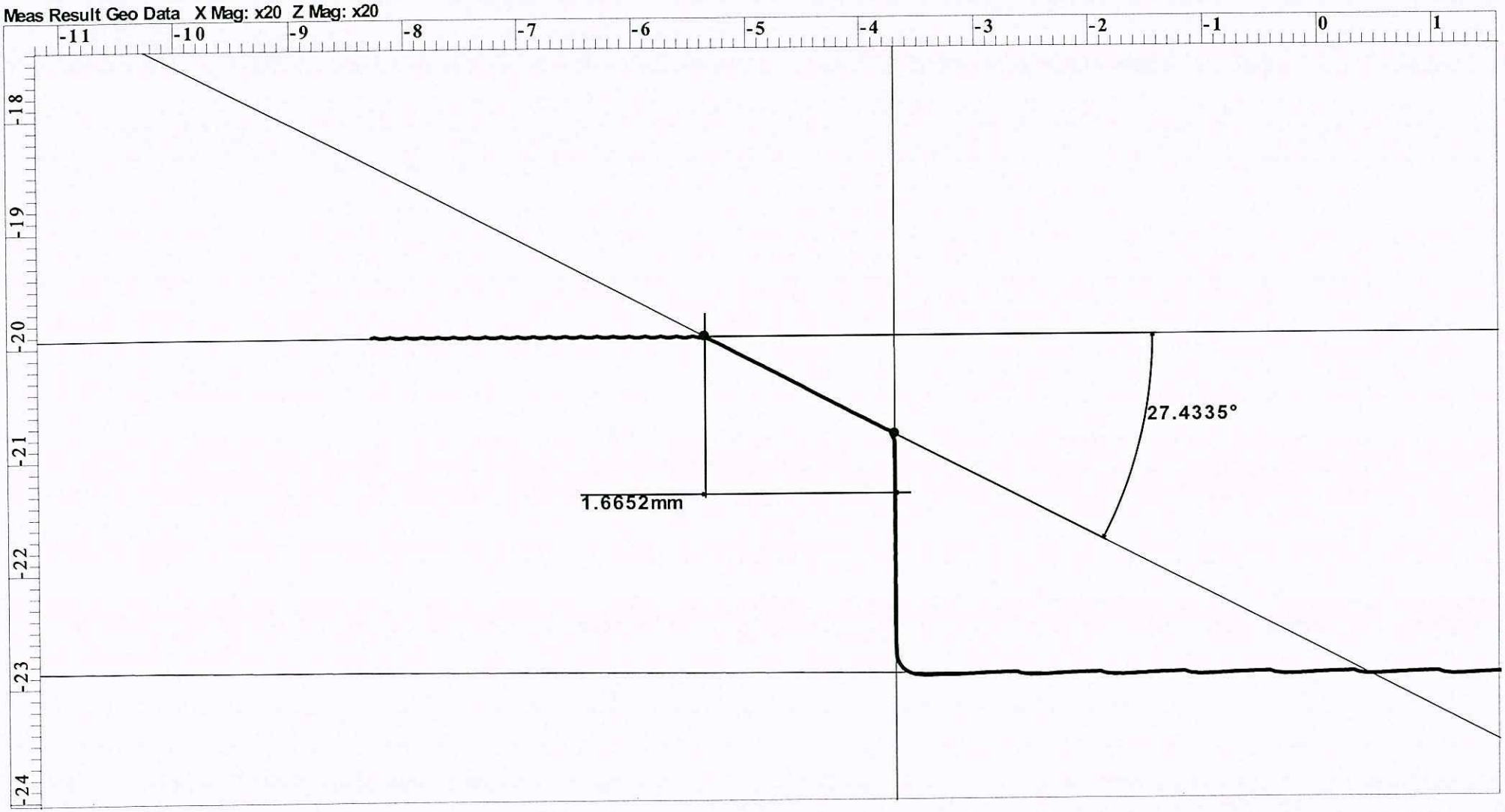
Meas Result Geo Data X Mag: x20 Z Mag: x20



INS

SMUSSO FORO FØ55

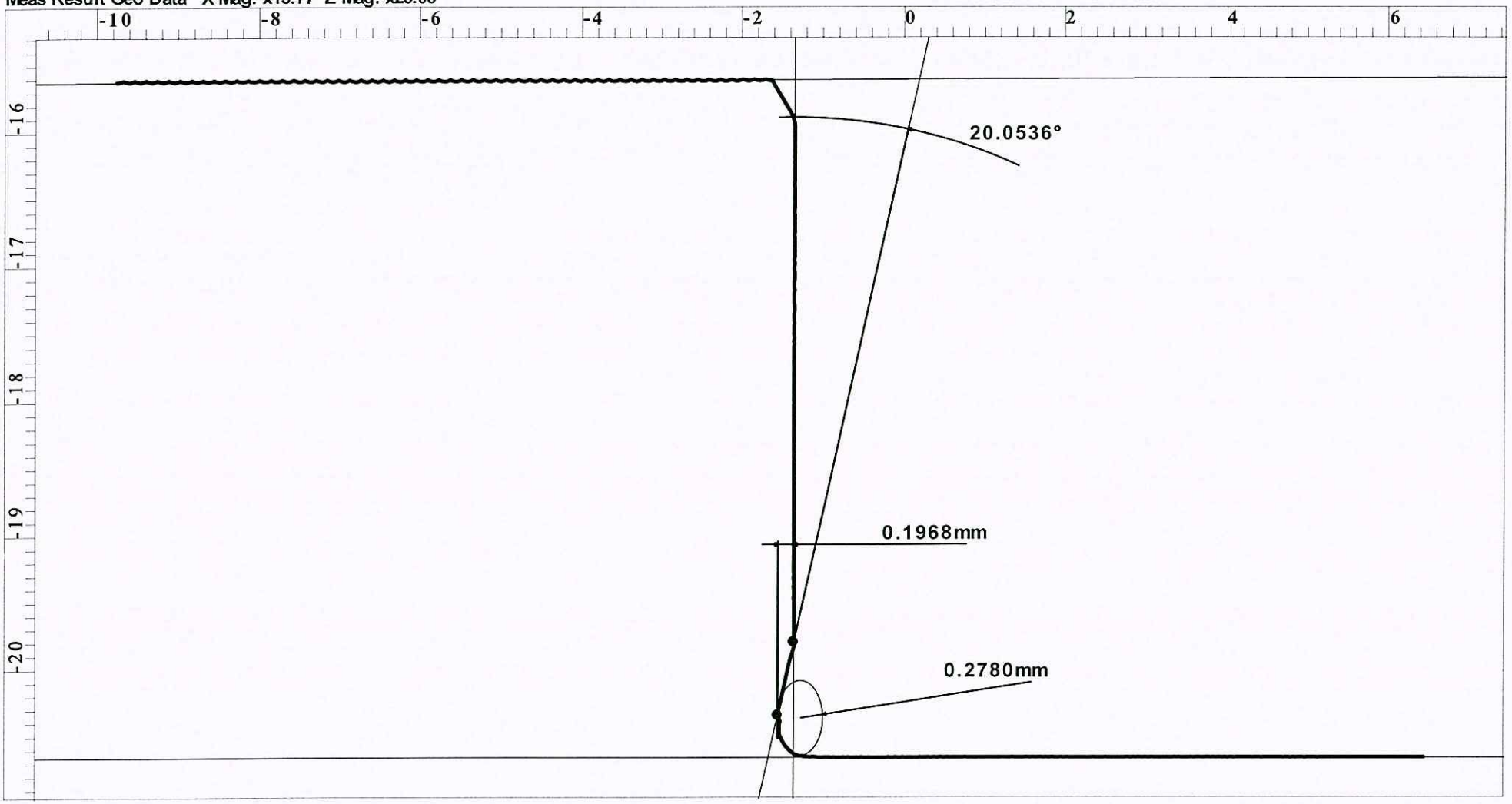
23/11/17 11:24:37



PART F1

23/11/17 11:47:47

Meas Result Geo Data X Mag: x13.77 Z Mag: x23.08

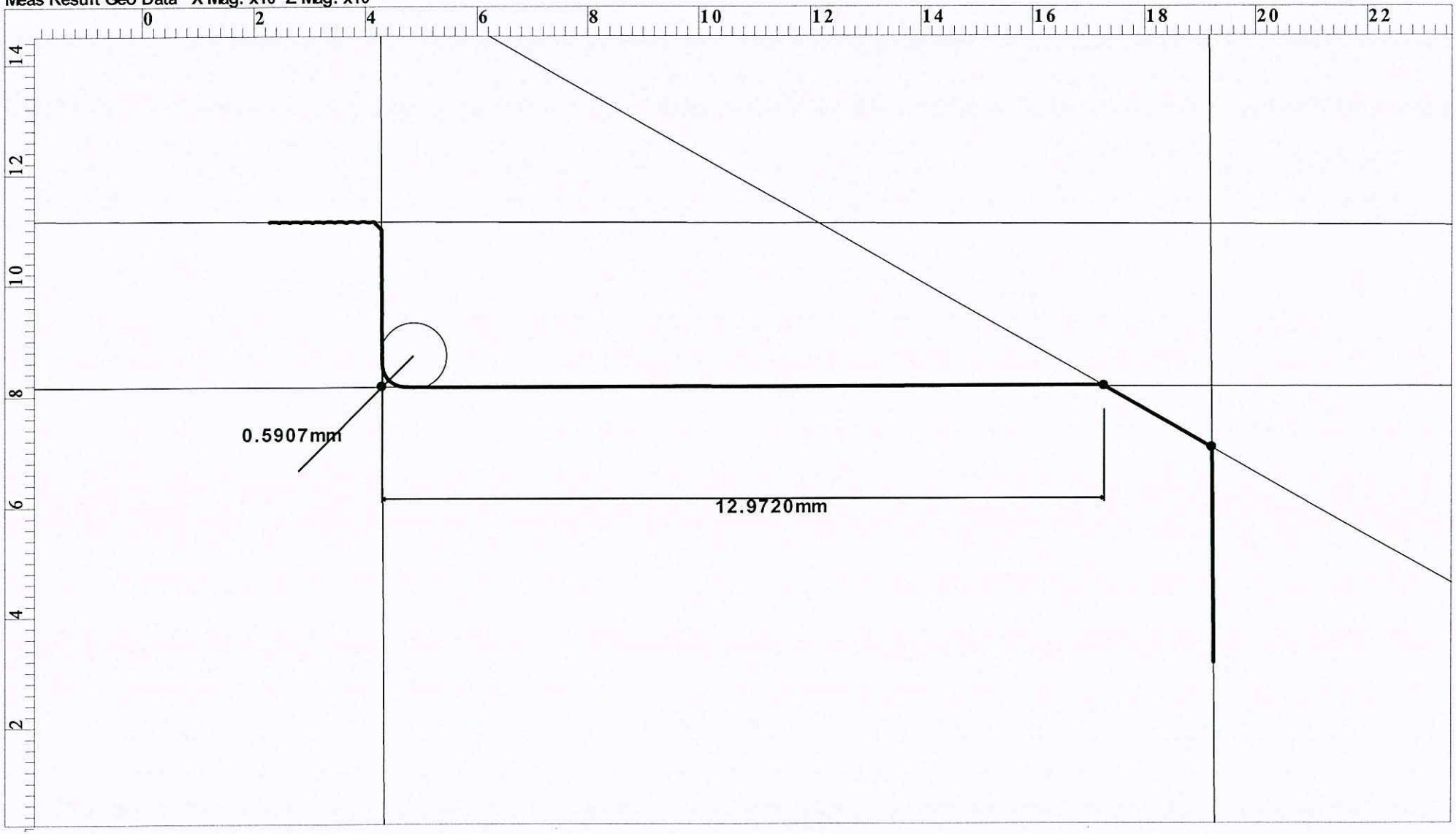


FORO D LATO FLANGIA H

1MS

23/11/17 12:03:11

Meas Result Geo Data X Mag: x10 Z Mag: x10

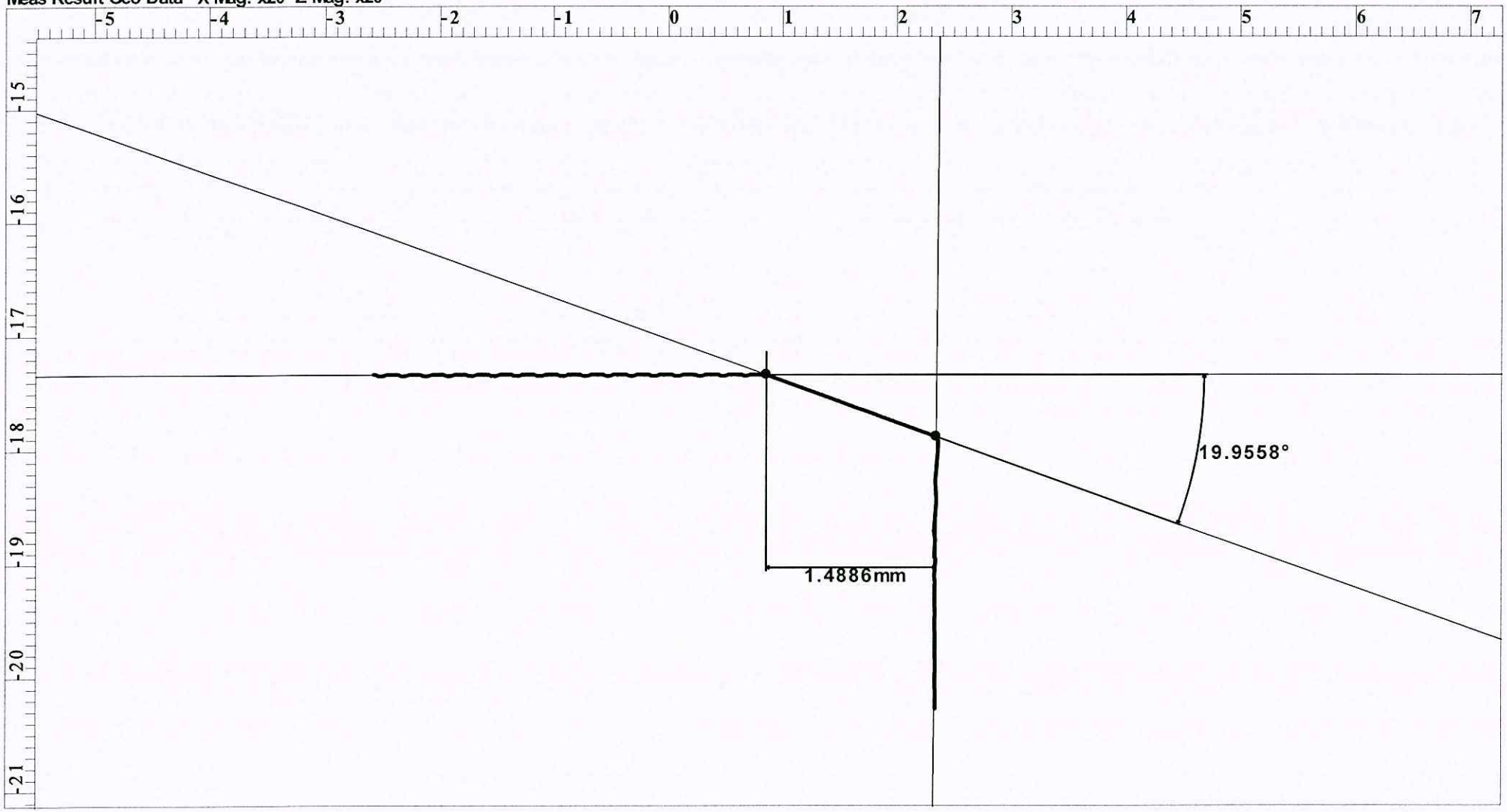


INS

SMUSSO FORO D LATO FLANGIA G

23/11/17 12:11:17

Meas Result Geo Data X Mag: x20 Z Mag: x20

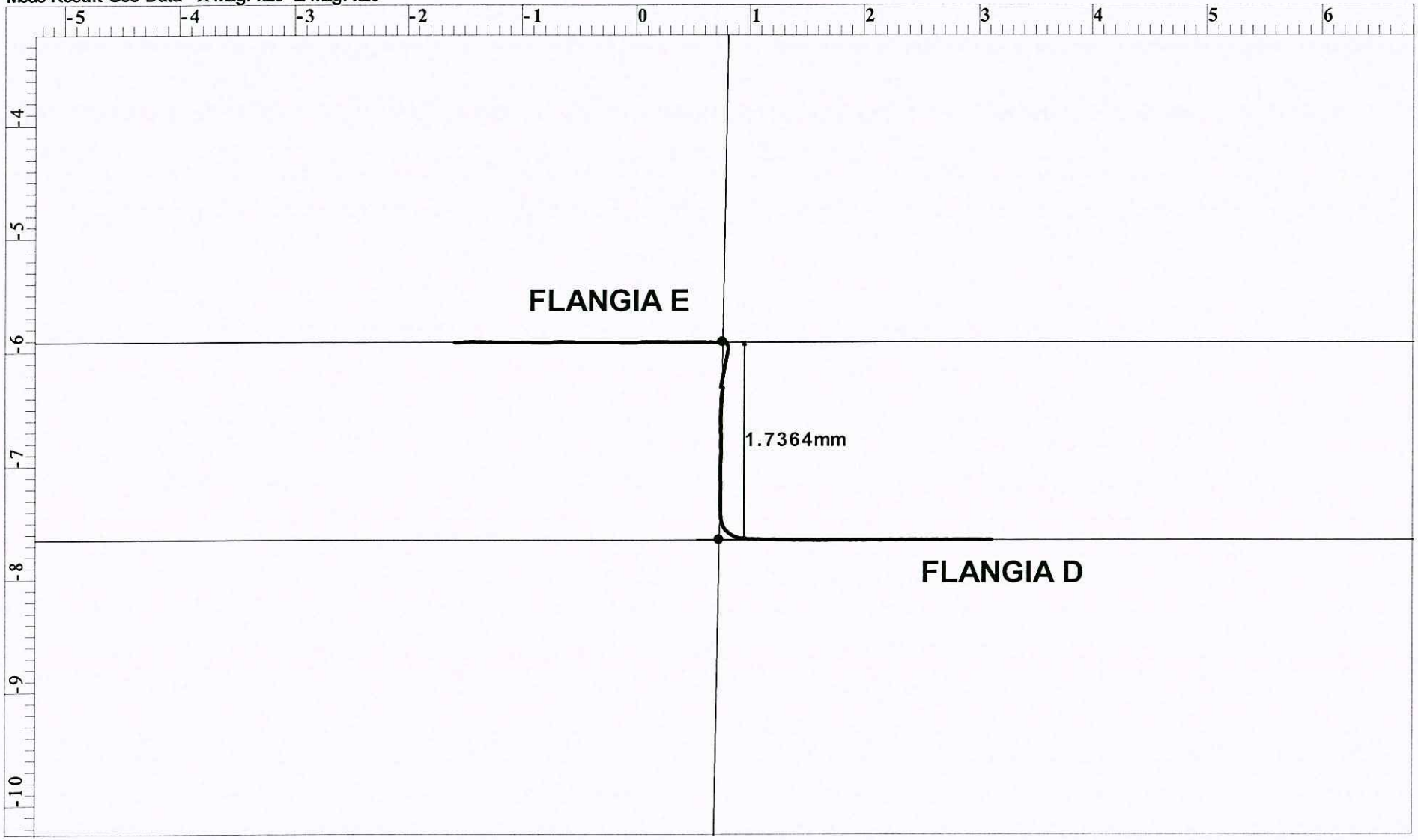


23/11/17 12:26:33

GRADINO E-D

INS

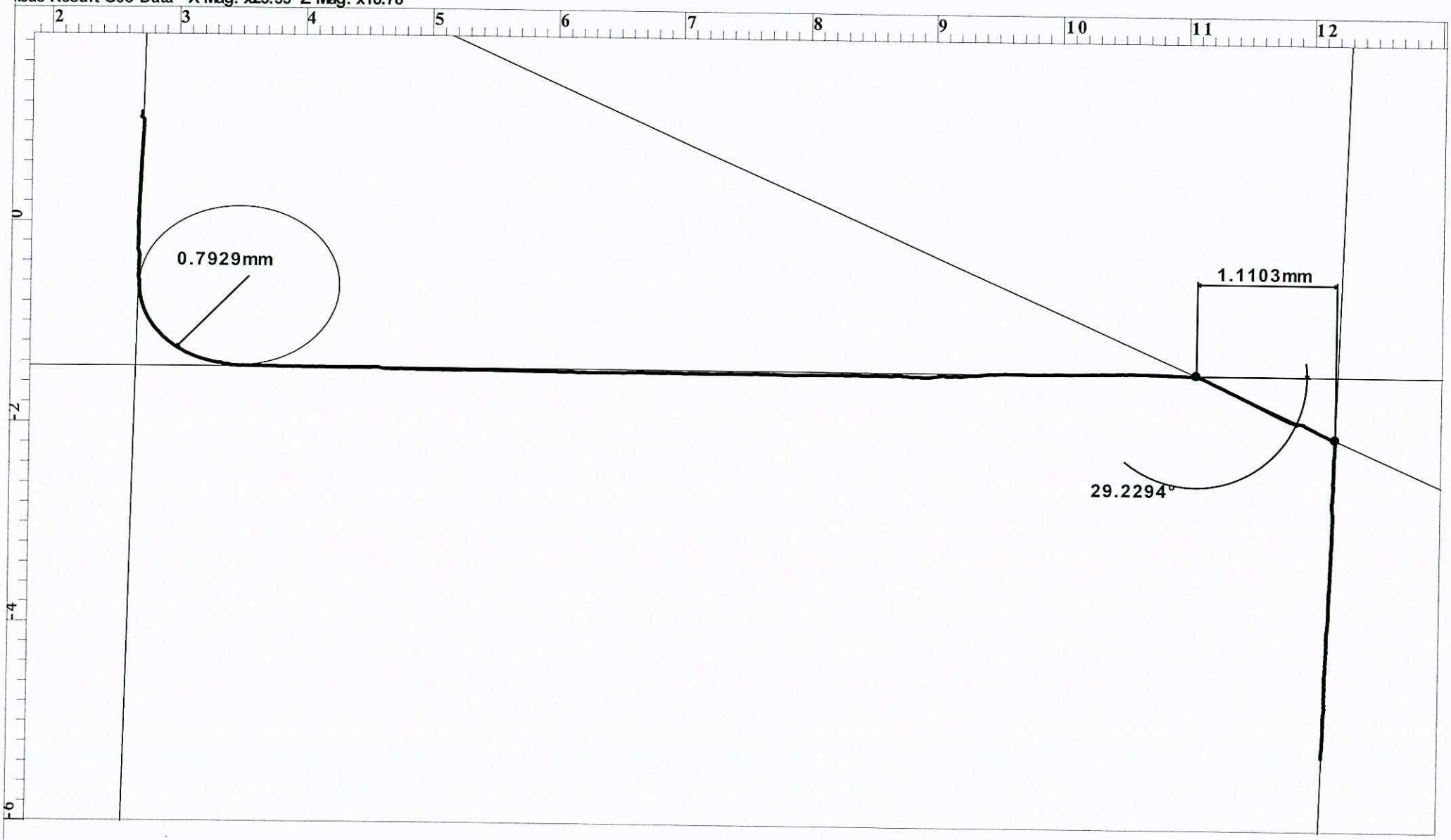
Meas Result Geo Data X Mag: x20 Z Mag: x20



FORO DG4

17/07/24 12:39:04

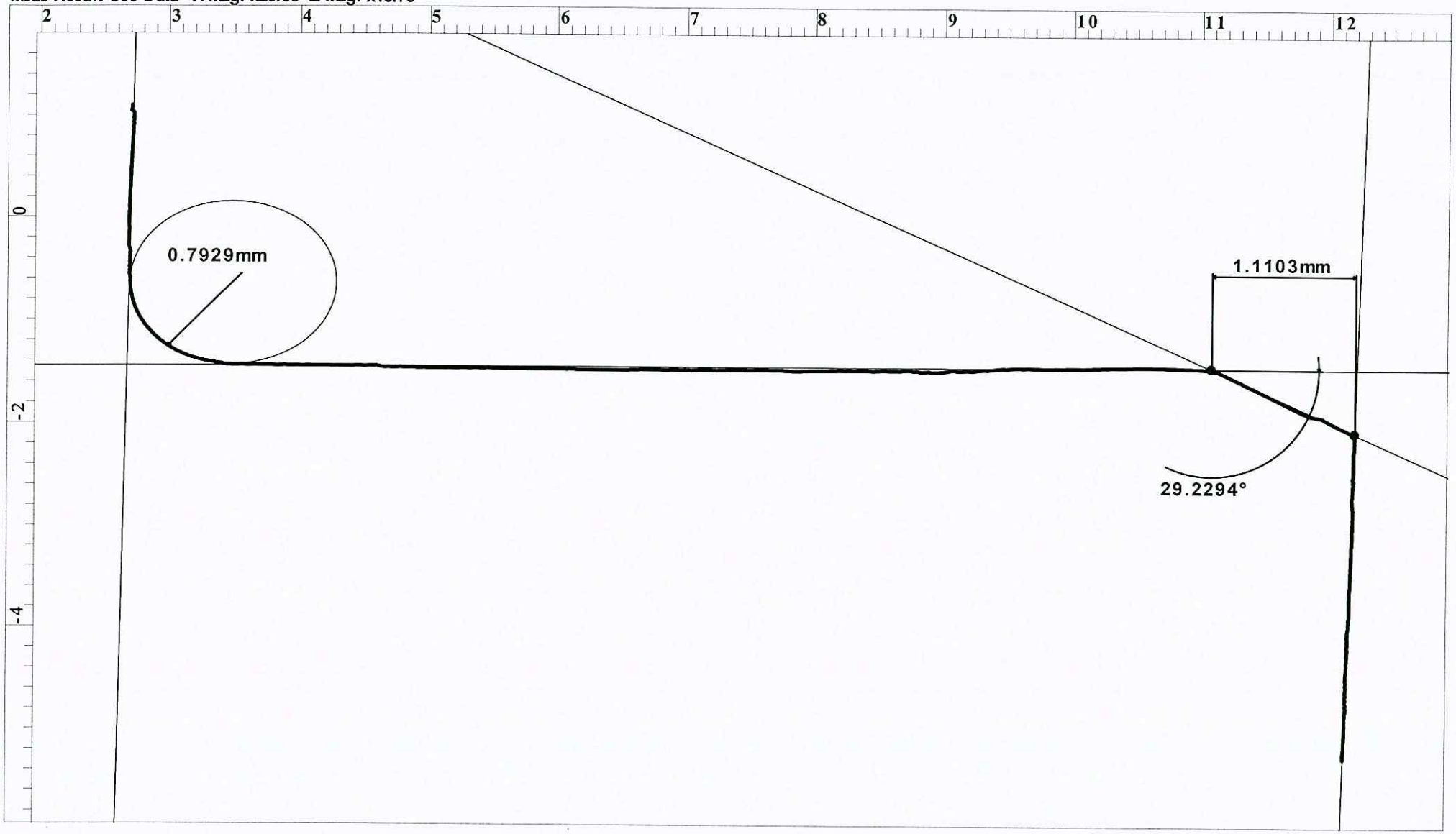
Meas Result Geo Data X Mag: x23.55 Z Mag: x18.78



FORO DG2

17/07/24 12:36:10

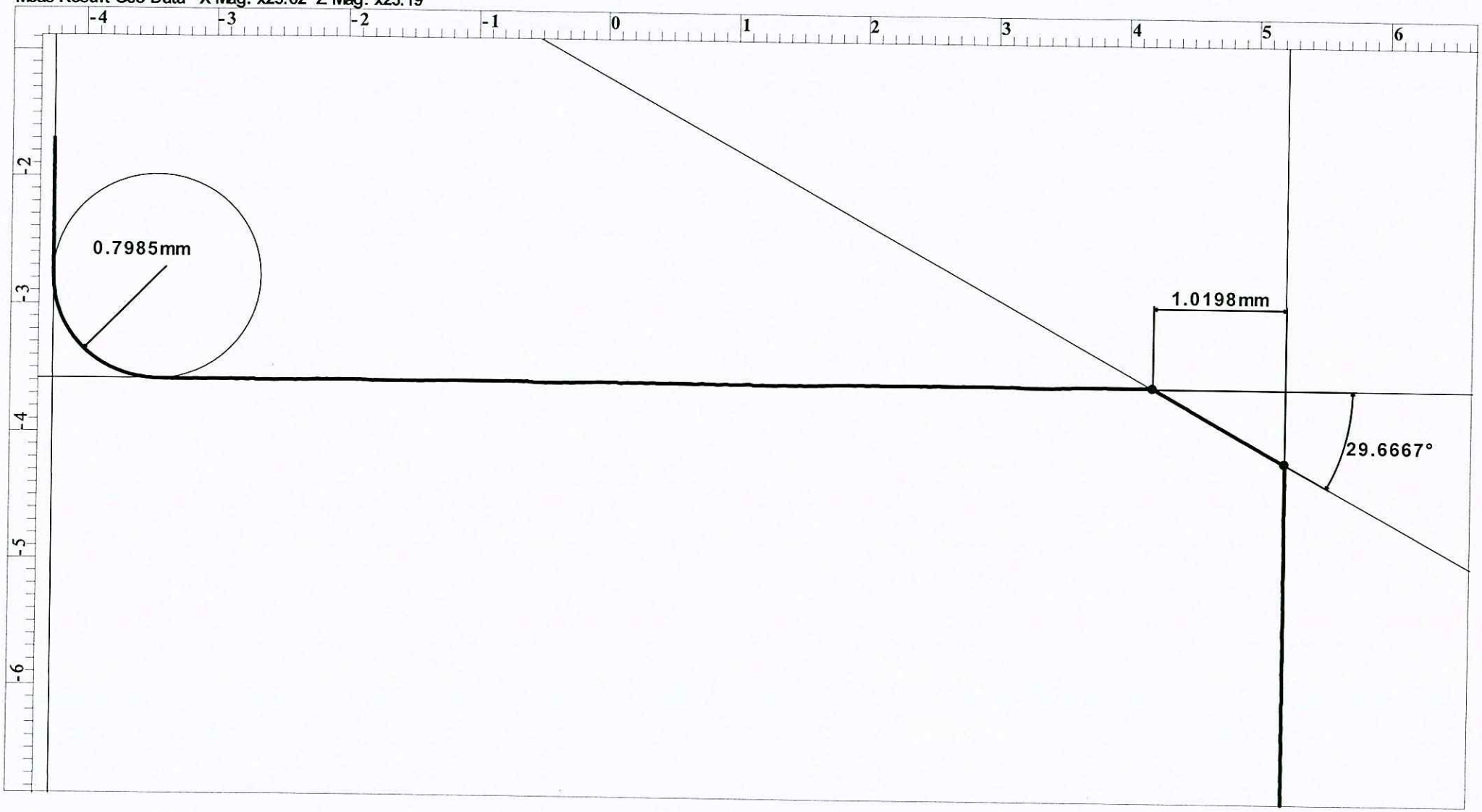
Meas Result Geo Data X Mag: x23.55 Z Mag: x18.78



FORO DG1

17/07/24 11:36:54

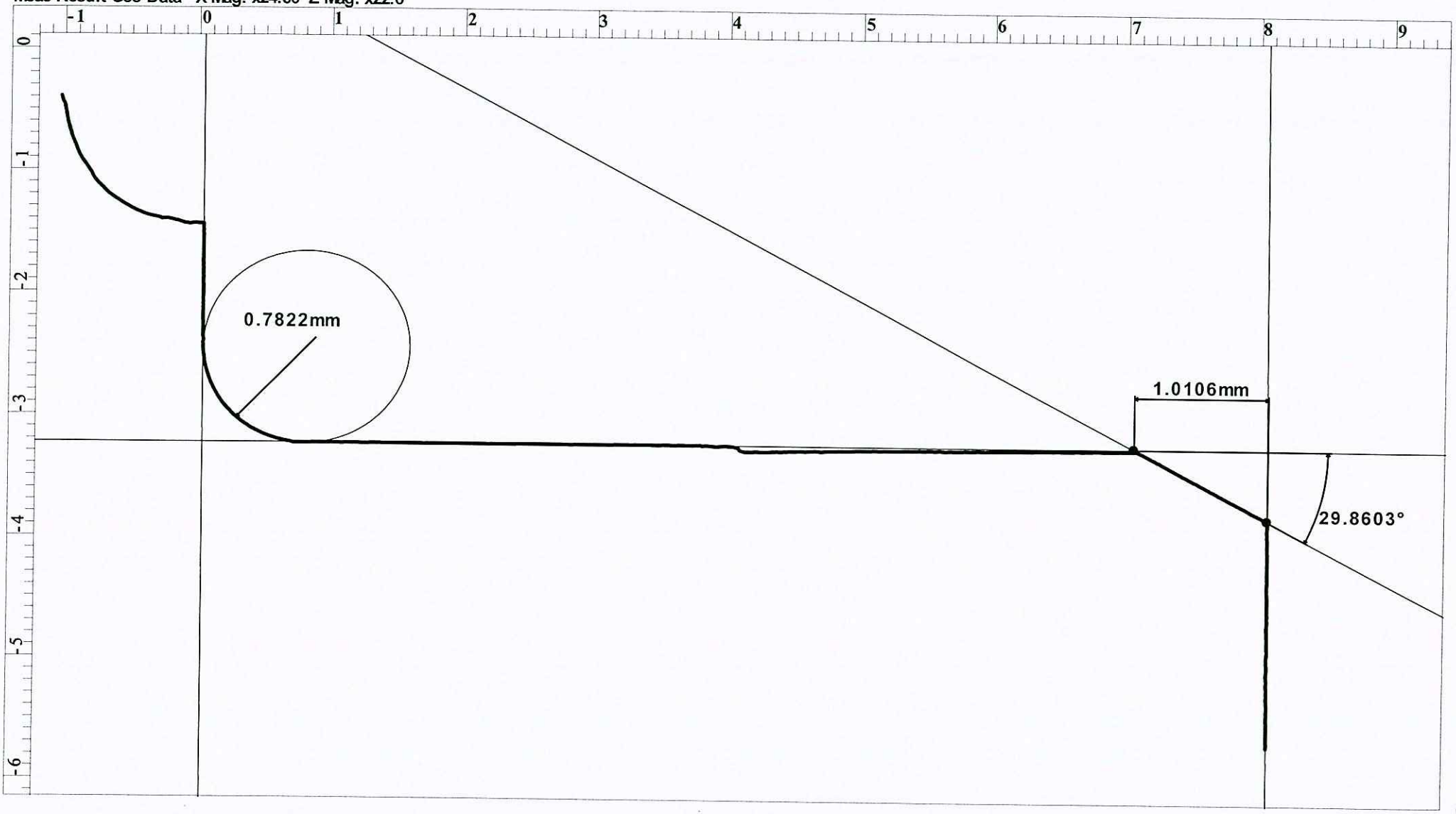
Meas Result Geo Data X Mag: x23.62 Z Mag: x23.19



FORO DG3

17/07/24 11:38:29

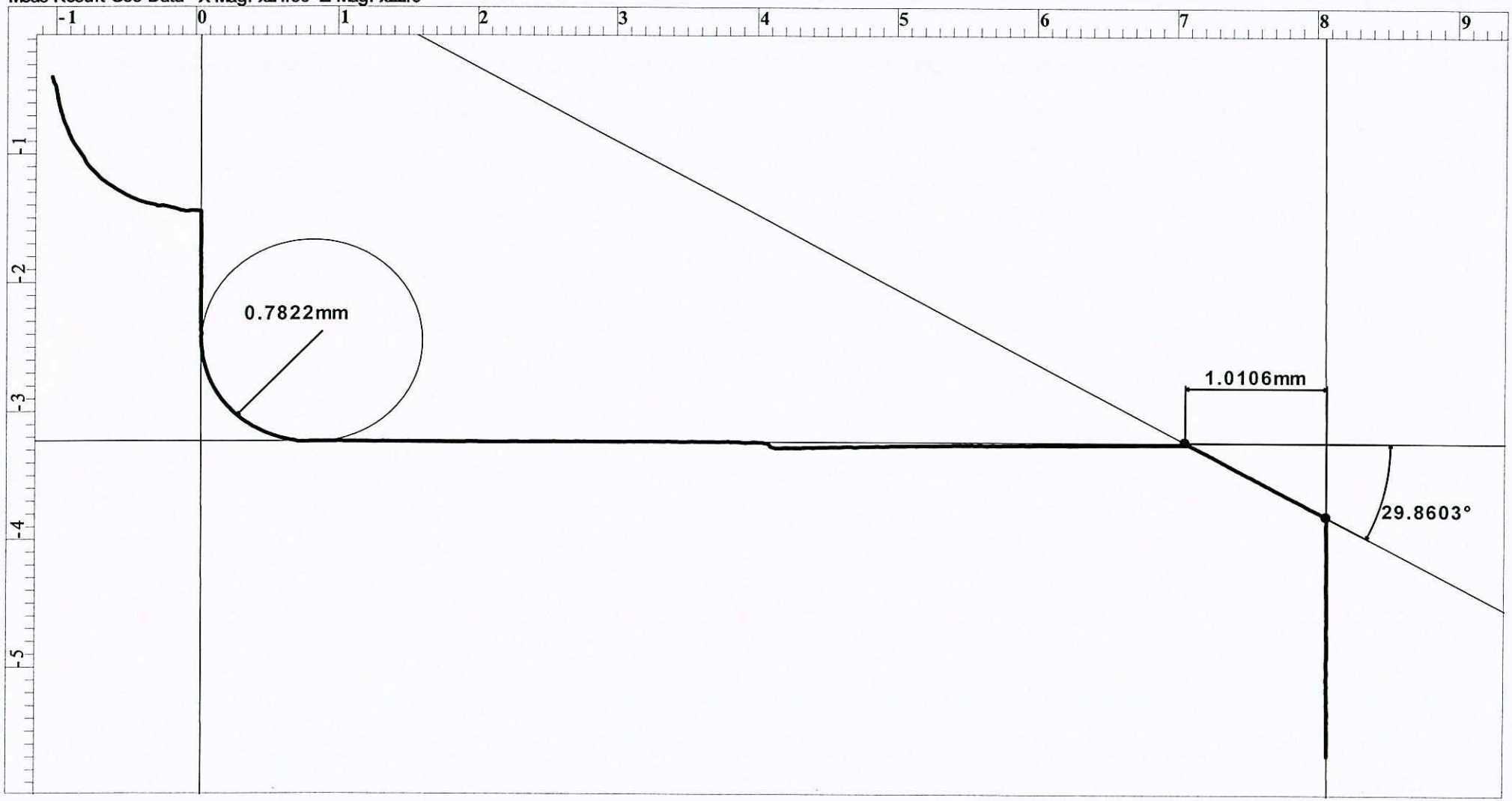
Meas Result Geo Data X Mag: x24.56 Z Mag: x22.6



FORO DG3

17/07/21 10:40:18

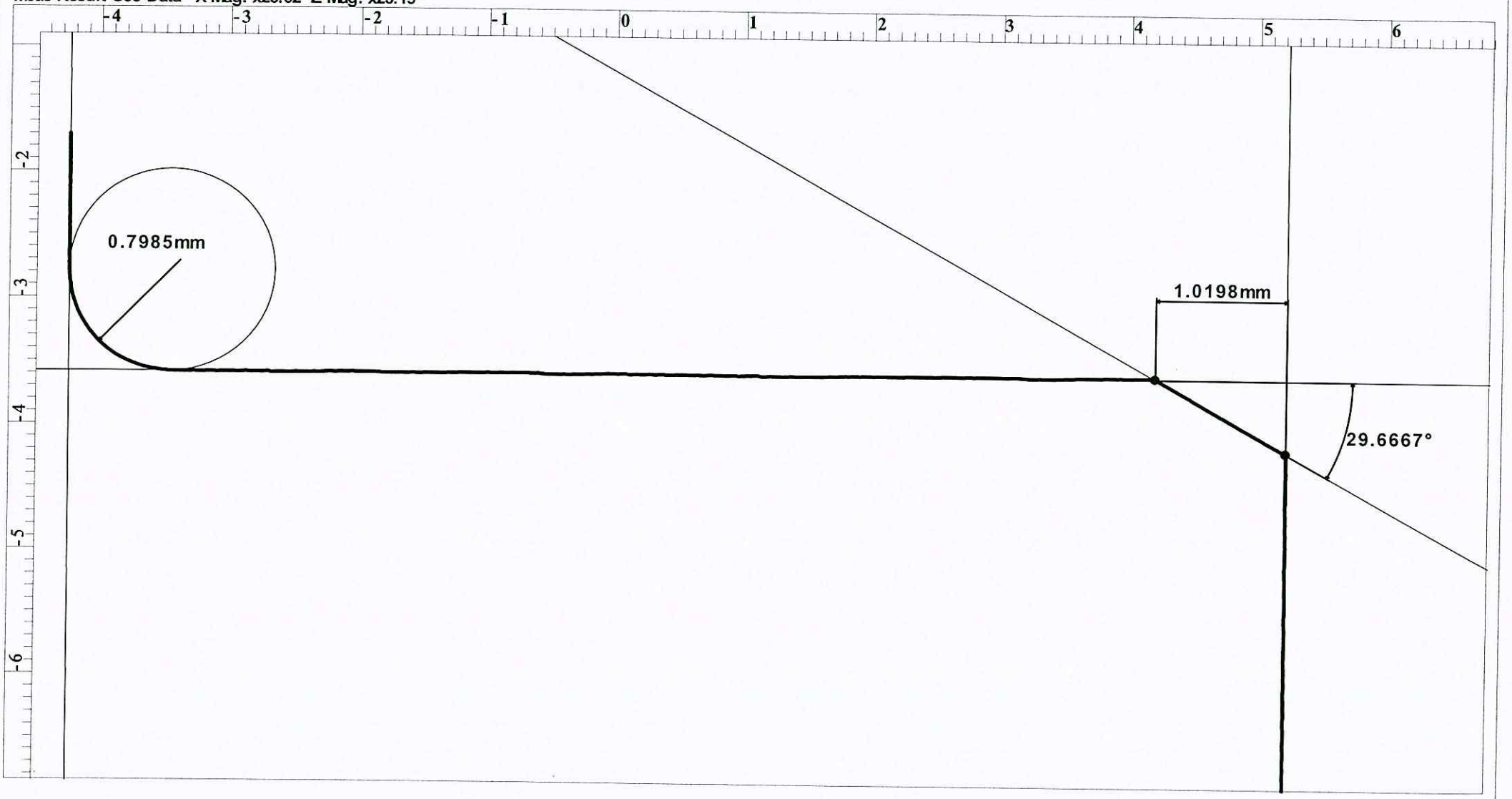
Meas Result Geo Data X Mag: x24.56 Z Mag: x22.6



FORO DG1

17/07/21 10:28:37

Meas Result Geo Data X Mag: x23.62 Z Mag: x23.19

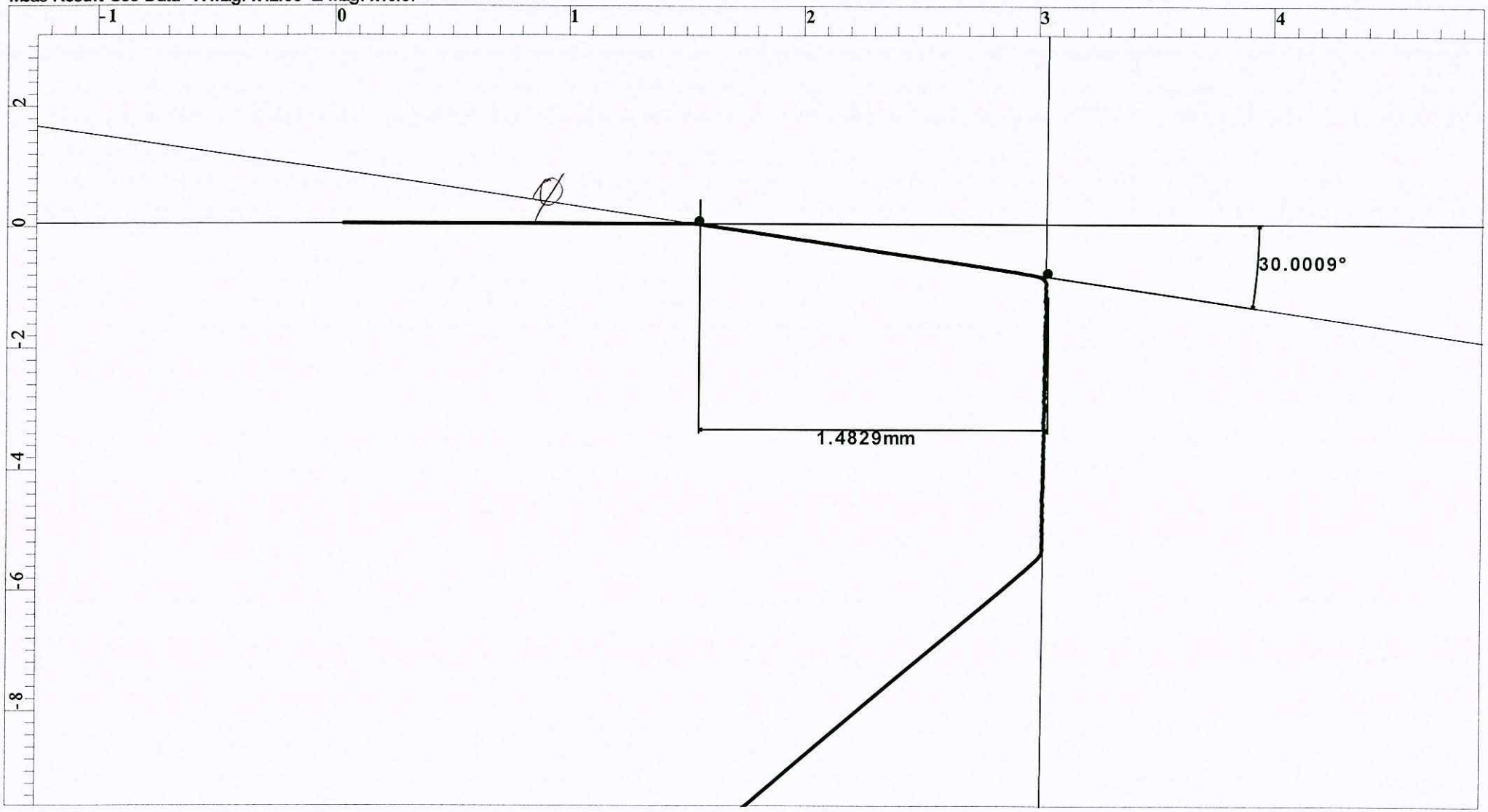


SMUSSO FORO CA2

INS

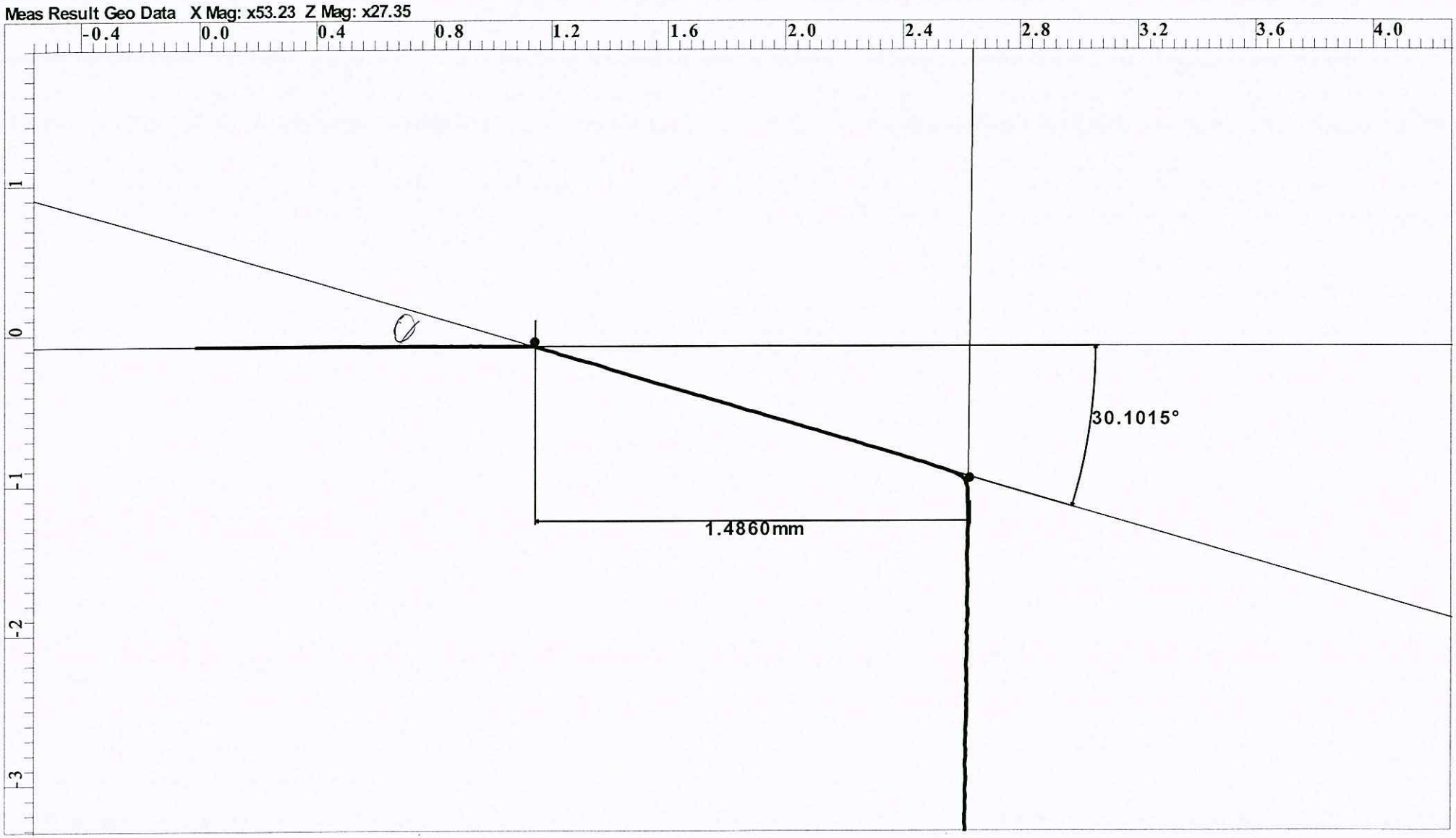
21/11/17 12:56:18

Meas Result Geo Data X Mag: x42.35 Z Mag: x10.97



SMUSSO FORO CA1

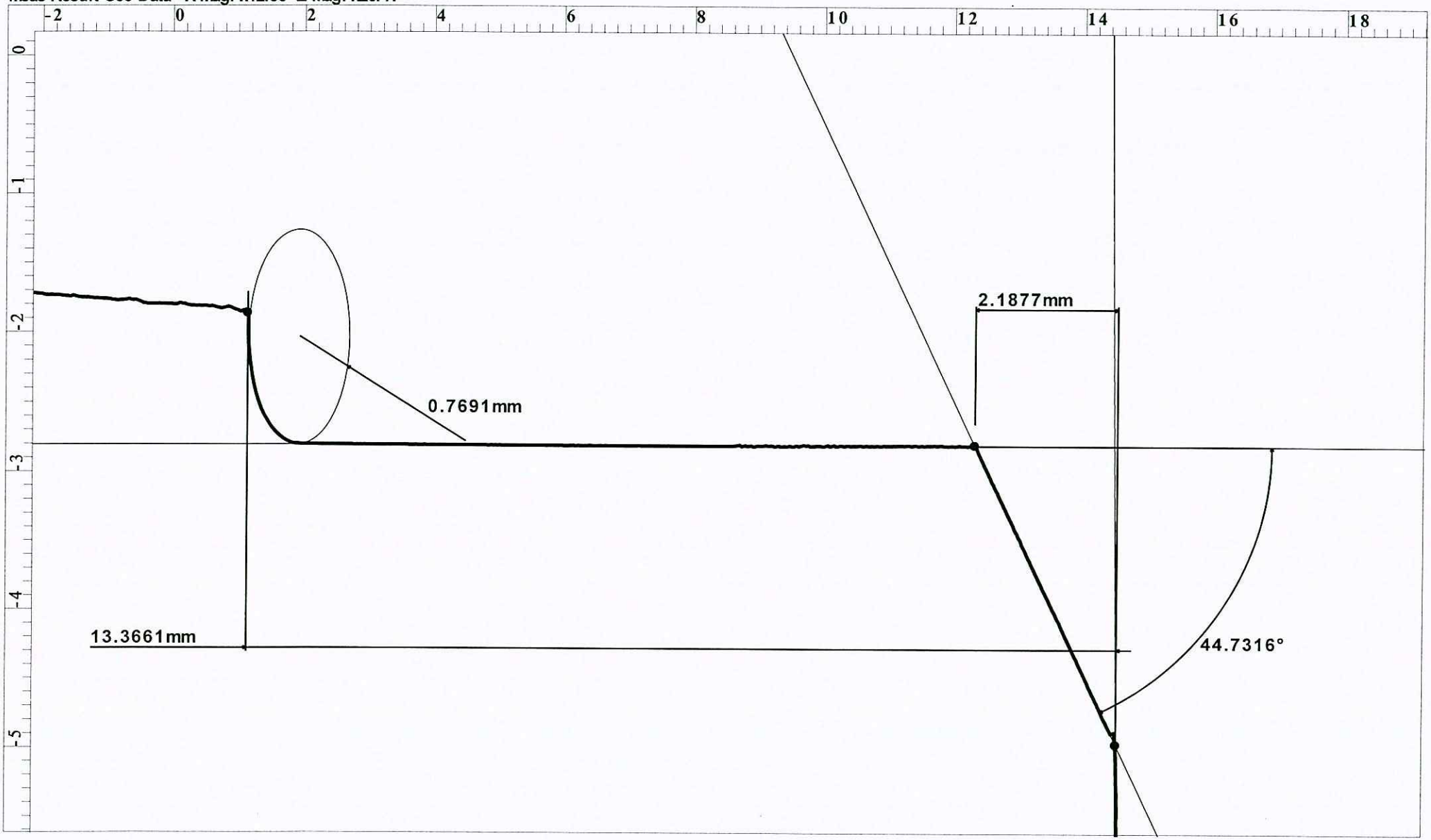
21/11/17 13:02:47



FORO SD1

17/07/21 08:57:53

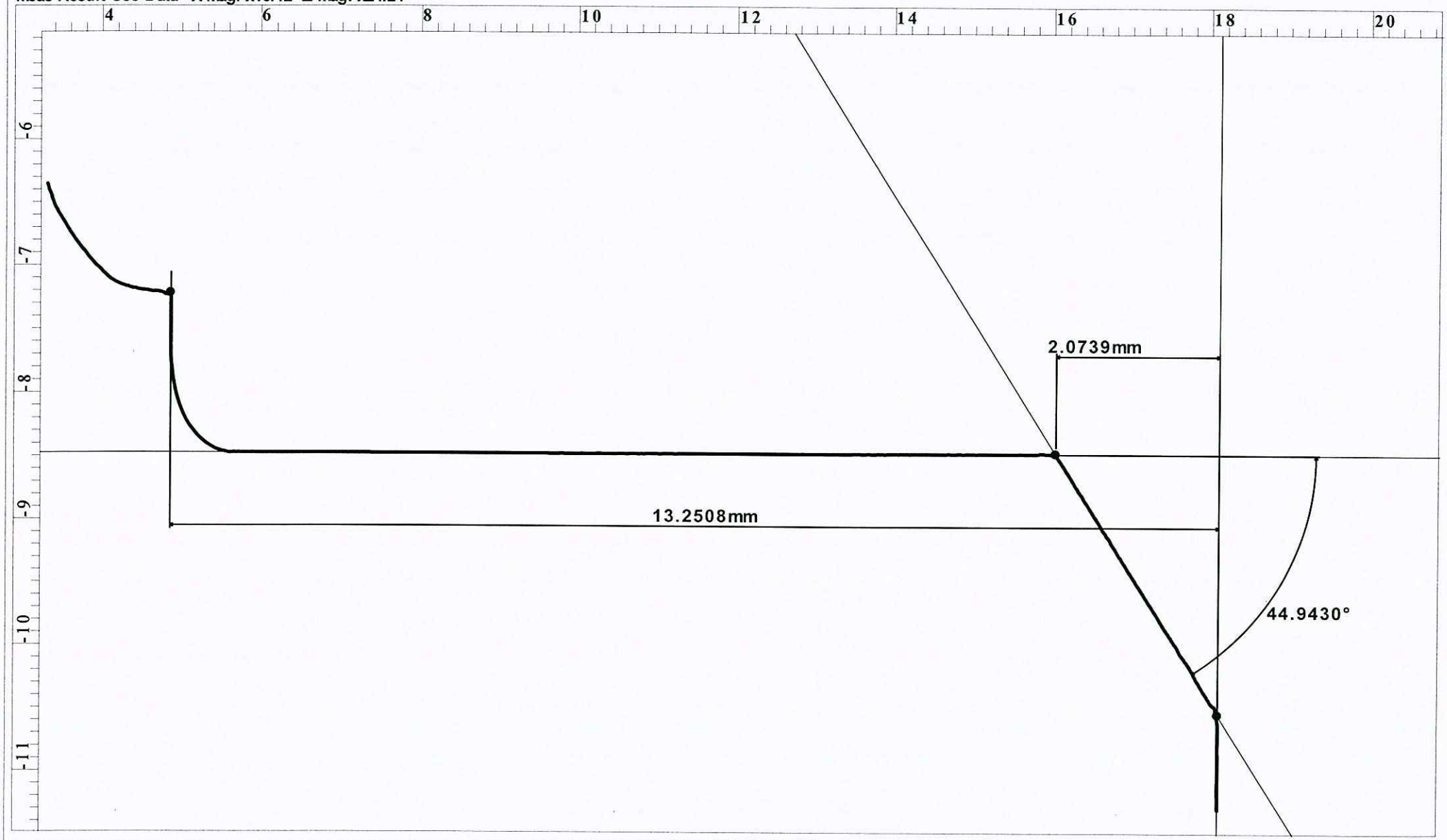
Meas Result Geo Data X Mag: x12.35 Z Mag: x26.41



FORO SD2

17/07/21 10:15:56

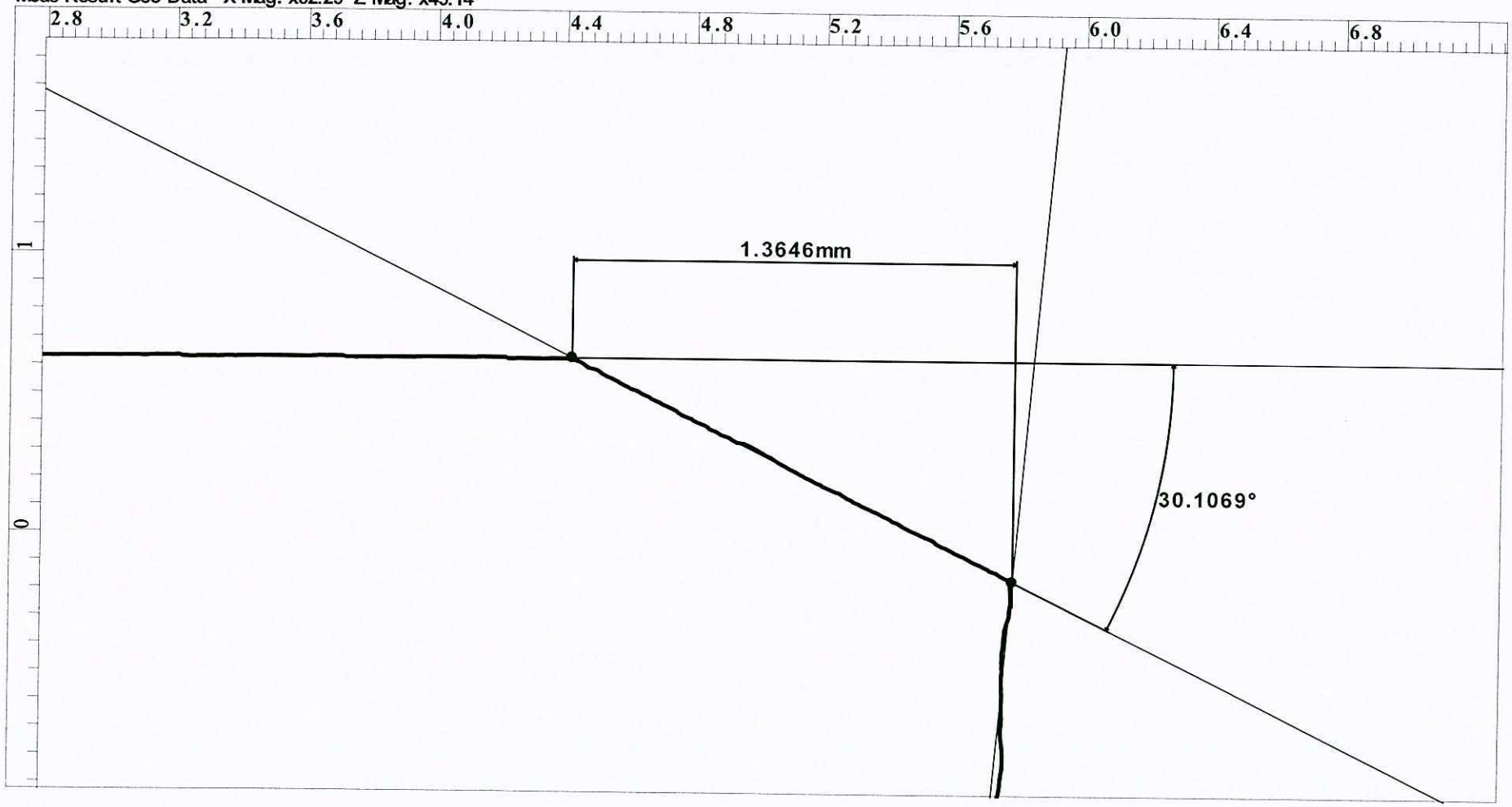
Meas Result Geo Data X Mag: x15.12 Z Mag: x24.24



FORO SR4

17/07/21 08:38:55

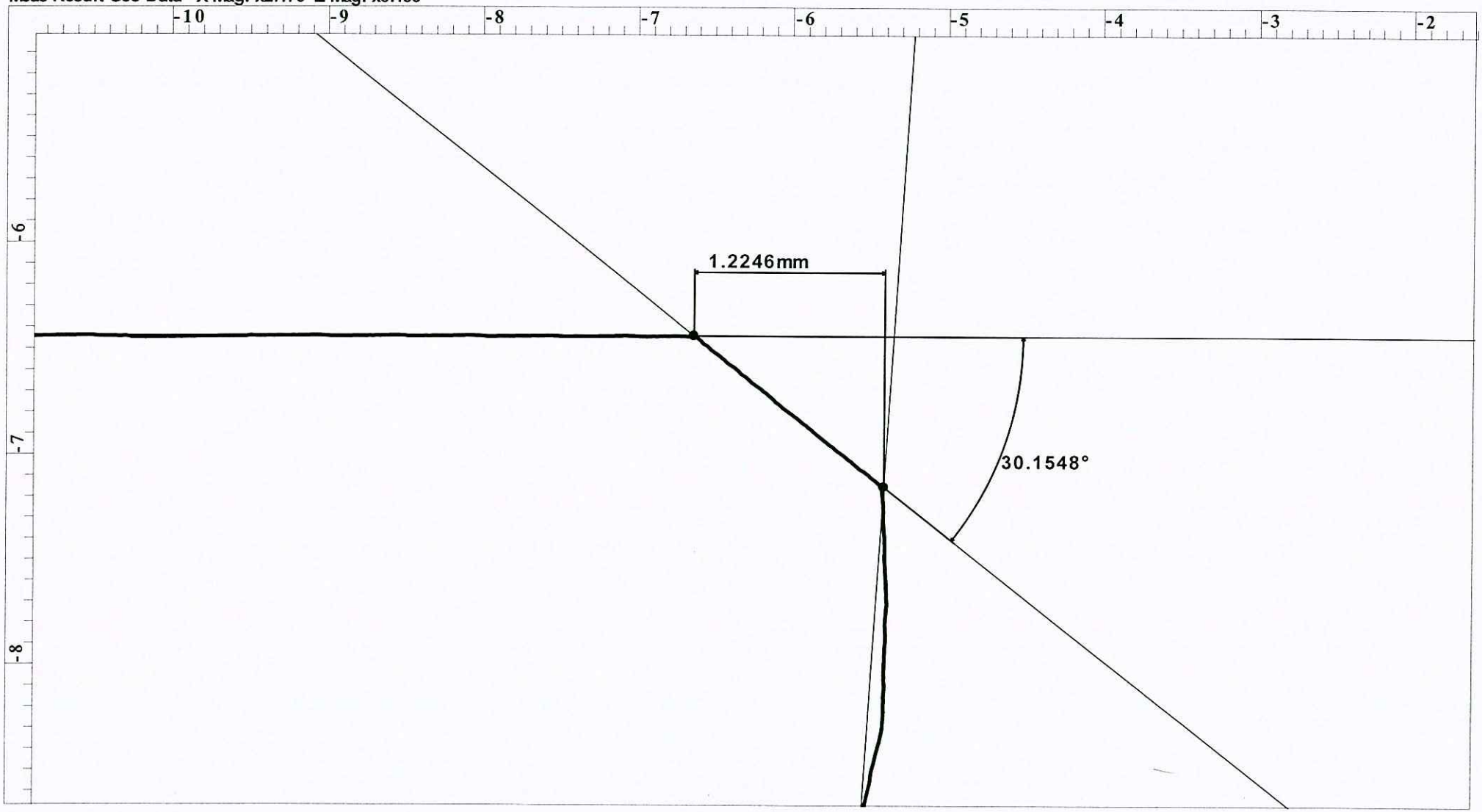
Meas Result Geo Data X Mag: x52.25 Z Mag: x45.14



FORO SR5

17/07/21 08:47:08

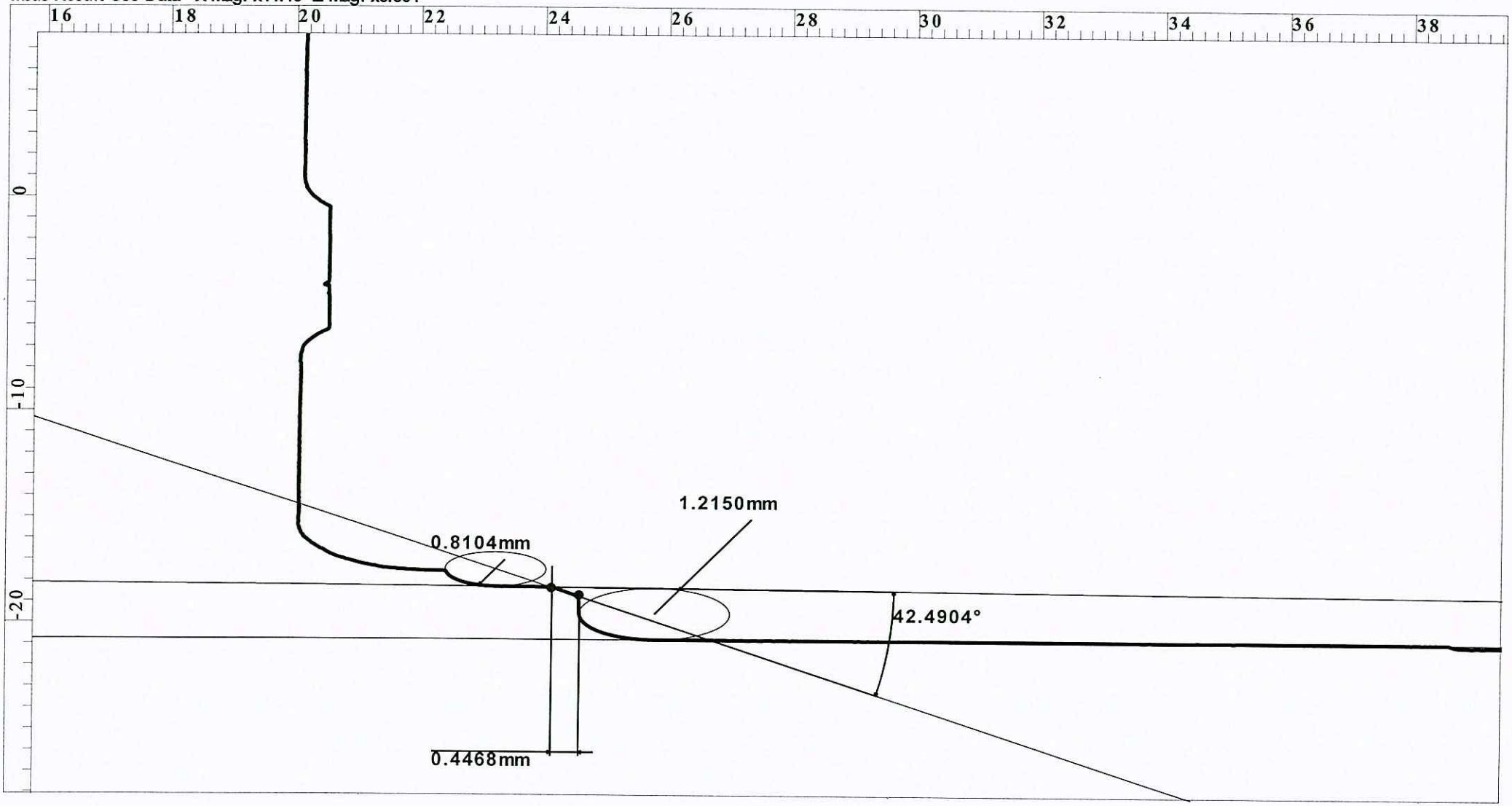
Meas Result Geo Data X Mag: x27.76 Z Mag: x37.93



FORO L1

17/07/21 11:20:16

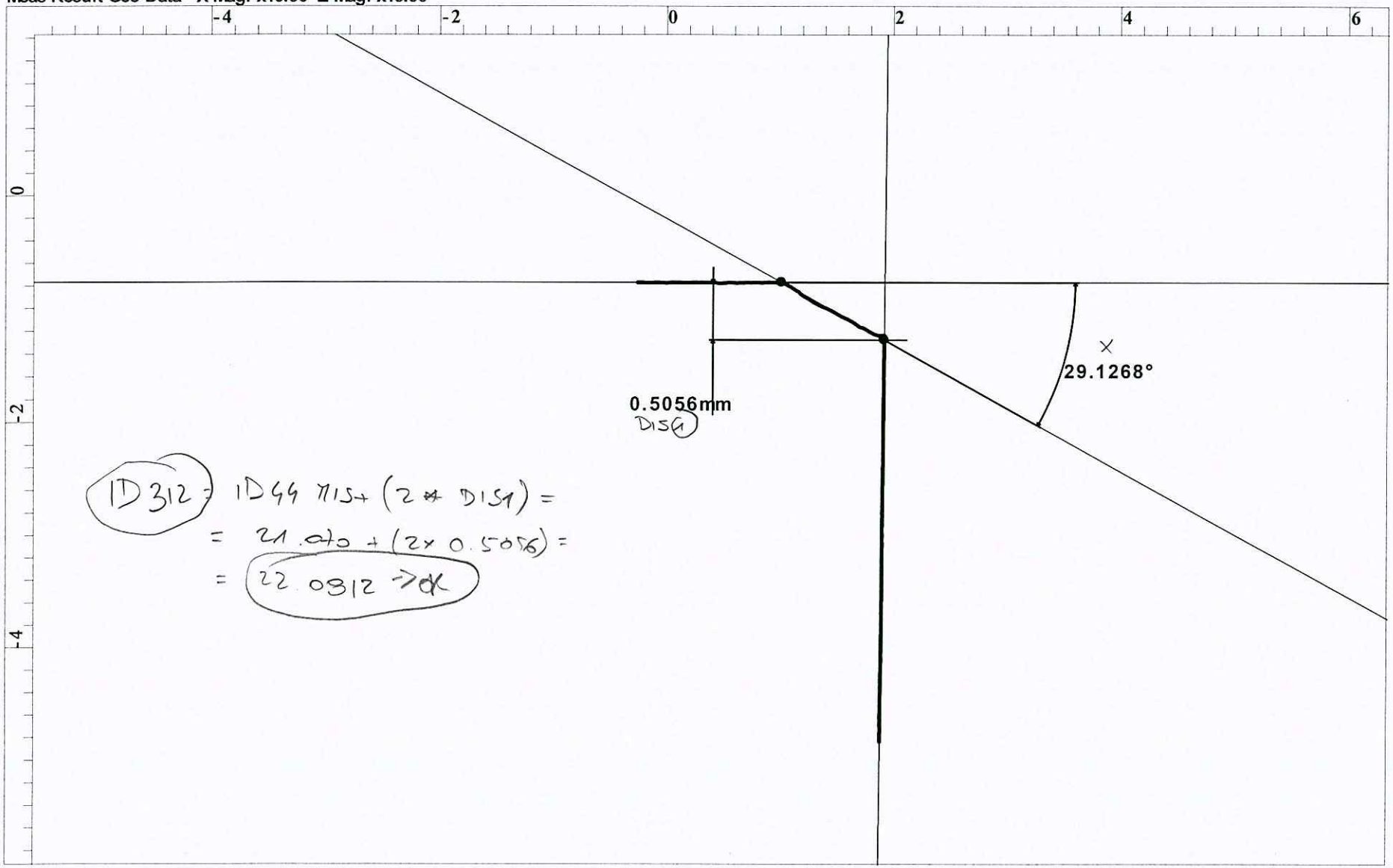
Meas Result Geo Data X Mag: x11.19 Z Mag: x3.854



FORO T1

17/07/18 10:37:00

Meas Result Geo Data X Mag: x19.96 Z Mag: x19.96



ID 312 = ID 44 MIS + (2 * DIS1) =

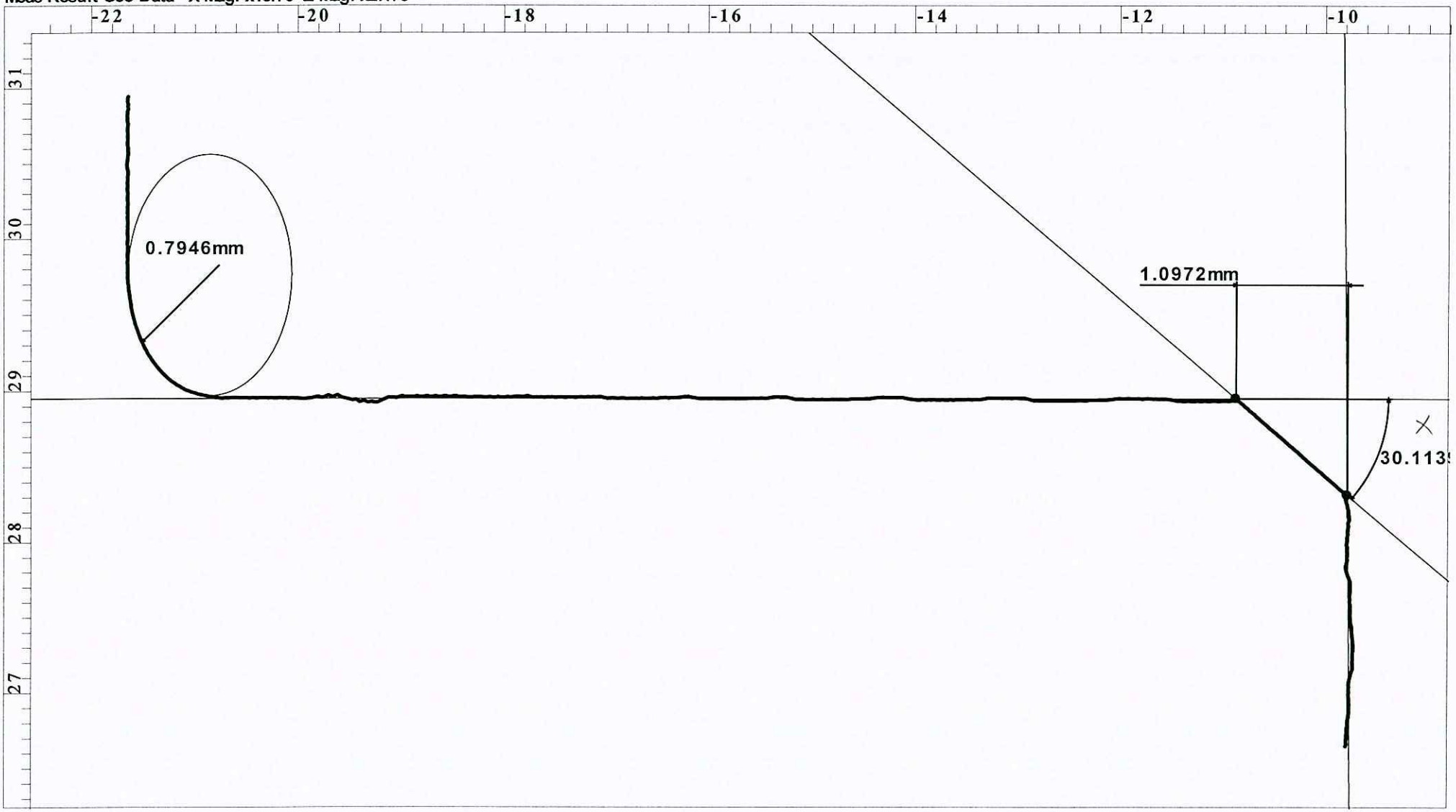
= 21.070 + (2 x 0.5056) =

= 22.0812 → OK

FORO SR2

17/07/18 12:40:20

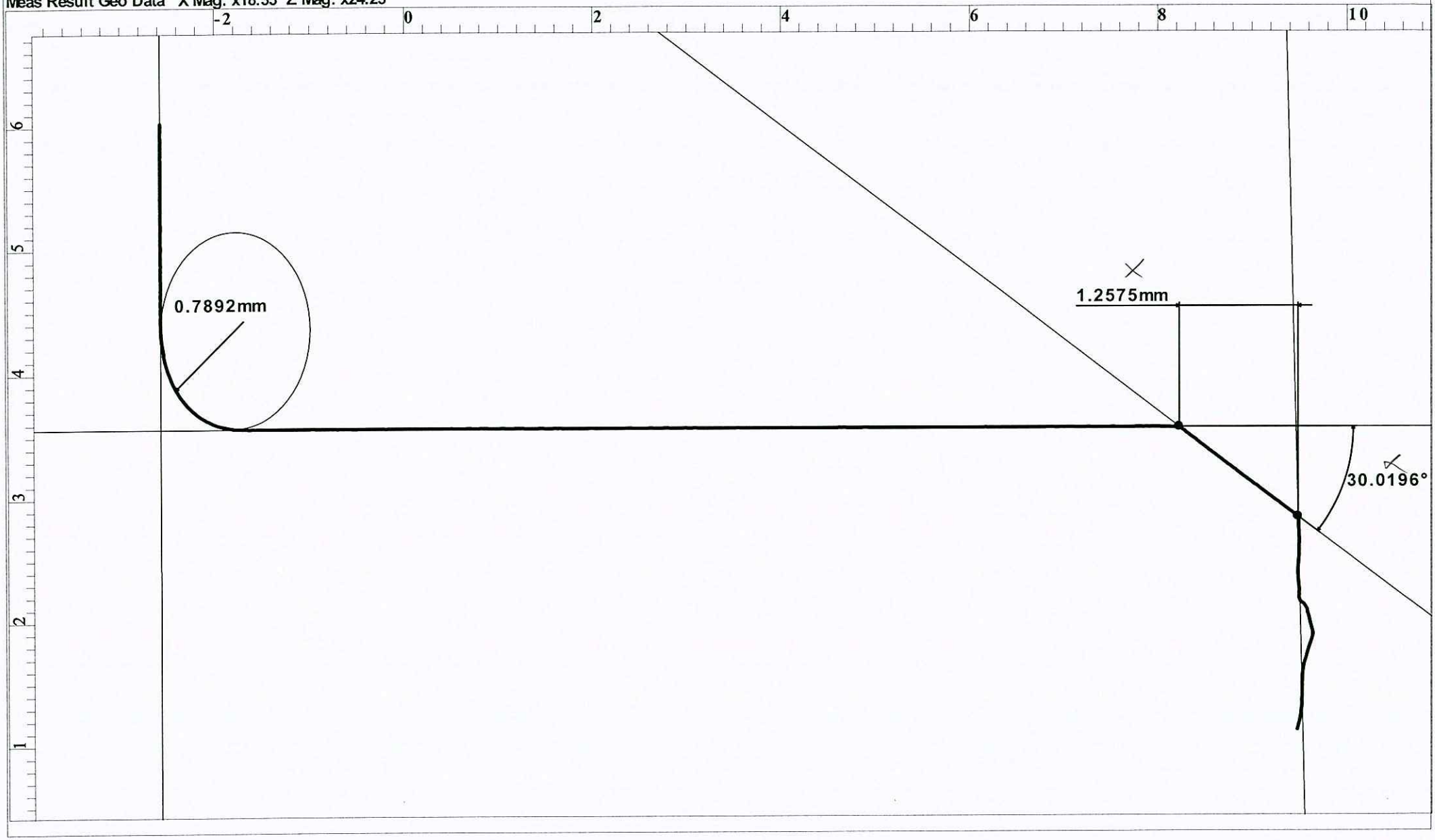
Meas Result Geo Data X Mag: x18.76 Z Mag: x27.76



FORO SR3

17/07/18 12:58:48

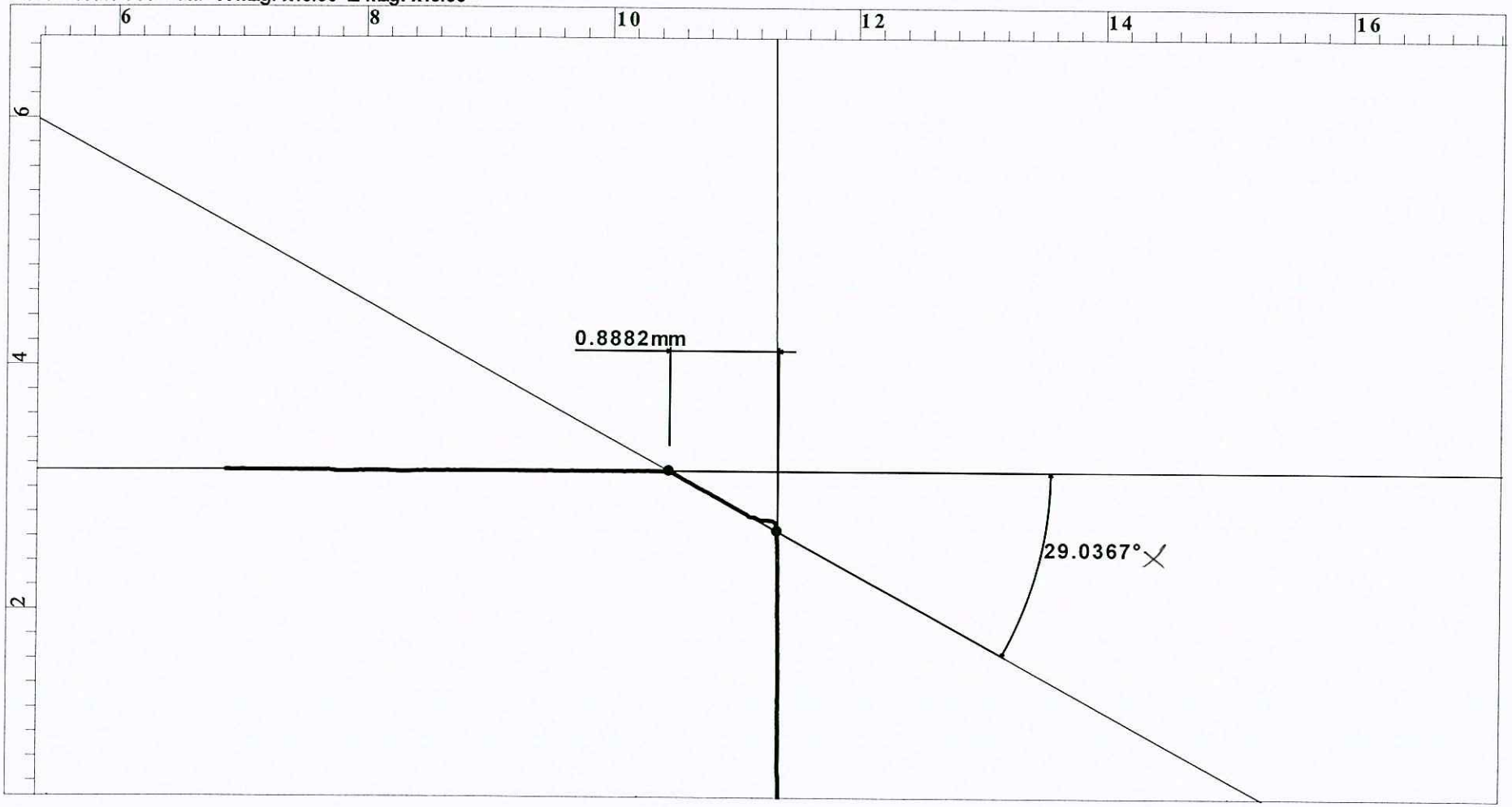
Meas Result Geo Data X Mag: x18.33 Z Mag: x24.23



FORO M

17/07/18 12:02:17

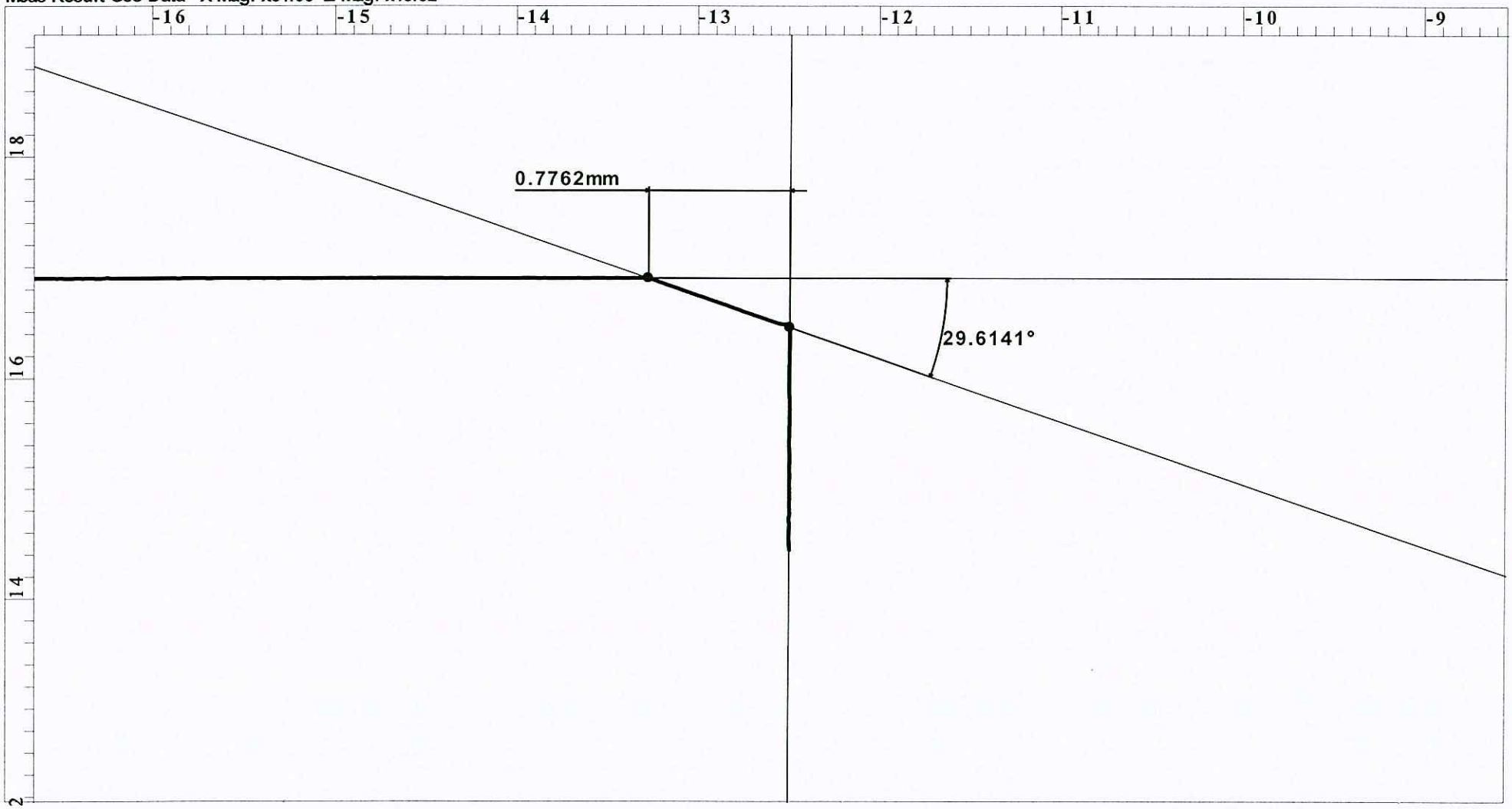
Meas Result Geo Data X Mag: x19.96 Z Mag: x19.96



17/07/18 12:20:33

FORO K

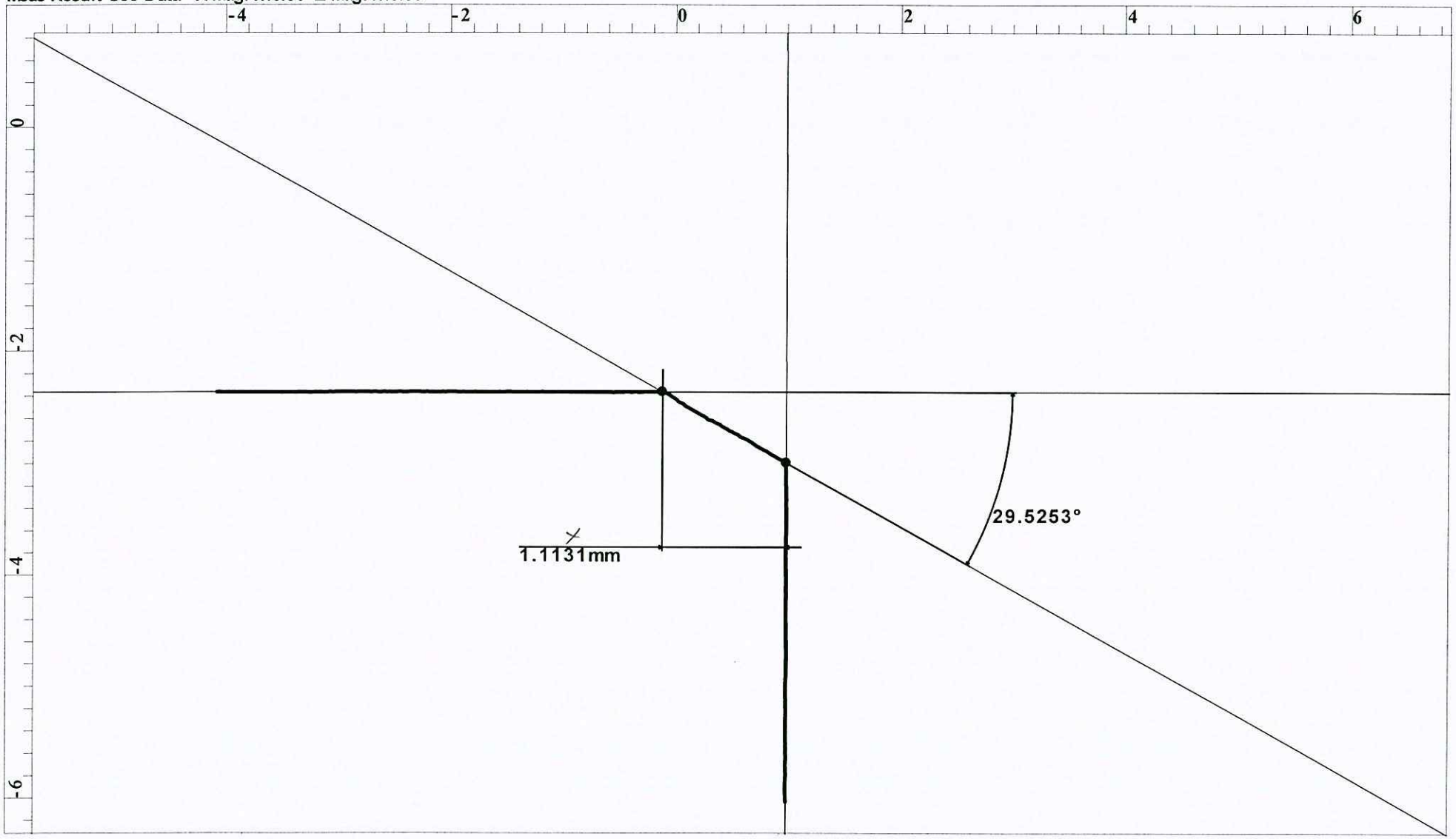
Meas Result Geo Data X Mag: x31.06 Z Mag: x19.02



FORO R

17/07/18 11:30:43

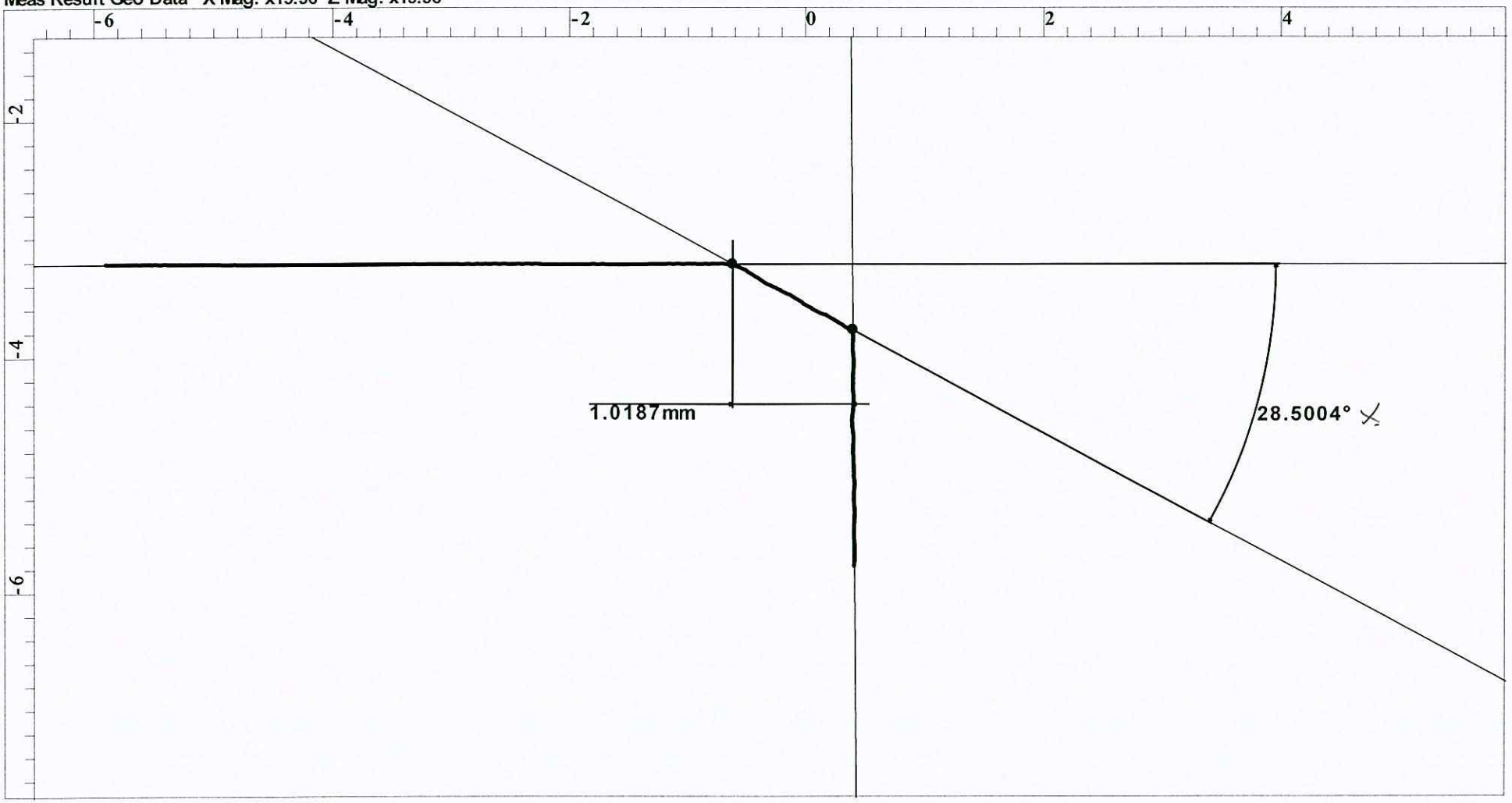
Meas Result Geo Data X Mag: x19.96 Z Mag: x19.96



FORO J

17/07/18 11:33:20

Meas Result Geo Data X Mag: x19.96 Z Mag: x19.96



Sbarro 2 | Produzione Grotto 27/06/2017 ZEISS

RICHIESTA DI CONTROLLO

DATA	ORA INGRESSO IN SALA METROLOGICA	OPERATORE

MACH BAZ 10363/10538 PAL. 4/1 VAR 6667 N° _____

MOTIVO CONTROLLO: C. PERIODICO ☐ TEST VARI ☐ PRIMO PEZZO ☐ **FASE:** 1 ☐ 2 ☐

TIPO CONTROLLO ALL ☐ MAIN ☐ FOCUS ☐

STATO MACCHINA: MACH FERMA ☐ MACH IN PRODUZIONE ☐

MISURE SPECIFICHE:

ELEMENTI NON CONFORMI:

ESITO FINALE OK NOK Visto Coordinatore / ATG	OPERATORE ZEISS	ORA